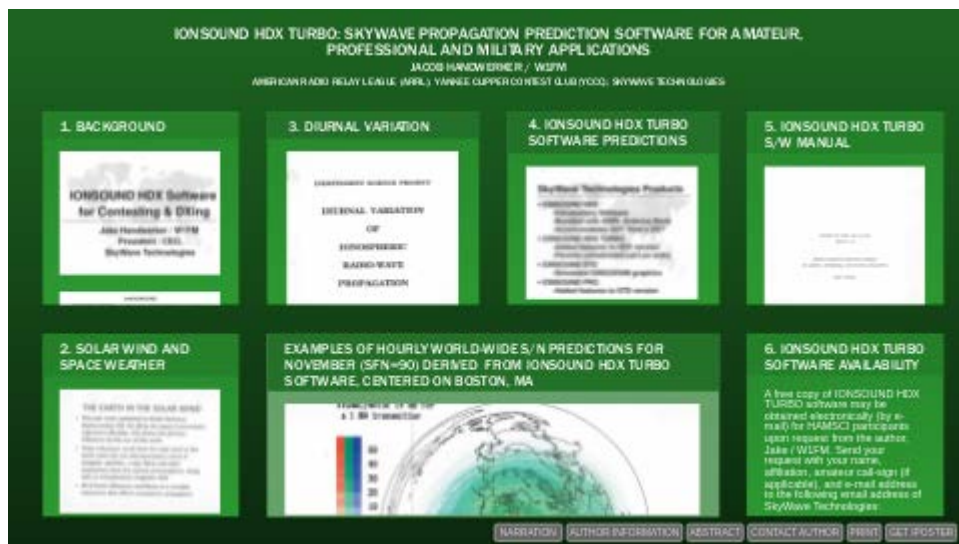


IONSOUND HDX TURBO: SKYWAVE PROPAGATION PREDICTION SOFTWARE FOR AMATEUR, PROFESSIONAL AND MILITARY APPLICATIONS



JACOB HANDWERKER / W1FM

AMERICAN RADIO RELAY LEAGUE (ARRL); YANKEE CLIPPER CONTEST CLUB (YCCC); SKYWAVE
TECHNOLOGIES

PRESENTED AT:



1. BACKGROUND



IONSOUND HDX Software for Contesting & DXing

Jake Handwerker / W1FM
President / CEO,
SkyWave Technologies

BACKGROUND

- IONSOUND HDX TURBO is a software propagation prediction program for use in the 1.8-30 MHz MF/HF range that evolved over a number of years and was primarily marketed in the 1990's by its author, W1FM, for use with IBM or IBM-compatible personal computers using DOS. It was intended to produce easy-to-interpret tabular predictions of radio frequency link performance between any two locations on the earth's surface.
- Menu selections within IONSOUND made it possible to compute predictions for comparison with Highest Possible Frequency (HPF), Maximum Possible Frequency (MUF) and Frequency of Optimum Transmission (FOT) predictions derived from U.S. Department of Commerce, National Telecommunications and Information Administration (NTIA) IONCAP program as found in ARRL's monthly QST Magazine "How's DX" Column.
- Parameters used in predictions included: Transmit and Receive Location, Short or Long Path, Local Receiver Noise Condition, Transmit and Receive Antenna/Gain, Receiver Bandwidth, Required Signal-to-Noise Ratio, Transmitter Power, Sunspot Number (SSN) or Solar Flux Number (SFN) Minimum Elevation Angle from the horizon, Prediction Frequencies, Prediction Months, Prediction Times, and Prediction Modes involving E and F Layer Propagation.

BACKGROUND (CONTINUED)

- The receive reliability prediction estimates include Total Receive Reliability which is composed of the product of Path Reliability and Signal-to-Noise (S/N) Availability.
- Path Reliability deals with the physics of the communication path specified by user-supplied transmitter/receiver latitude/longitude or location choices whereas the S/N Availability deals with the effects of absorption on the actual signal levels and local noise conditions relative to the minimum required S/N specified by the user.
- Takeoff radiation angle dependency on E, F, or multimode E/F hops along with antenna elevation angle gain, E and F layer ionospheric absorption, polarization loss, and ground reflection losses are also taken into account.
- The IONSOUND HDX TURBO program operates with or without a math coprocessor but will automatically take advantage of the 8087, 80287, or 80387 coprocessor if it finds it. A coprocessor is recommended due to the mathematically intensive nature of the calculations performed.
- A personal computer with 640 kilobytes of Random Access Memory (RAM) is desirable, along with DOS 2.11 or greater. For hard copy printout, a printer supporting IBM Graphics is recommended.

Presentation Highlights

- **Propagation Overview**
- **IONSOUND Software Features**
 - Overall Summary
 - SkyWave Technologies Product List
 - Additional Contesting/DXing Attributes
- **IONSOUND TURBO Detailed Screens**
- **Prediction Comparisons**
 - 3Y0PI Peter Island Band Open-WA0PUJ
 - CQWW 1994 IONCAP Predictions-N6BV
- **Software Give-a-Way**

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IONTSOUND Software by W1FM
Propagation Prediction Software for Amateur, Professional, Marine and Military Applications
 SkyWave Technologies, 17 Pine Knoll Road
 Lexington, MA 02173 U.S.A.
 Tel: 617-862-6742

The IONSOUND family of copyrighted programs (HDX, HDX TURBO, STD, and PRO) represent state-of-the-art software tools for predicting MF/HF/VHF ionospheric (skywave) propagation to any part of the world. They are ready-to-run programs designed to be fast and user-friendly through its menu-driven screens. As a minimum, all versions are supplied with an on-disk printable manual. Support is provided for color and graphics for PCs or compatibles for DOS. Use of a coprocessor is recommended but not required. IONSOUND programs can be stored on a hard drive and require up to approximately 520 Kbytes of RAM memory for execution.

IONSOUND provides prediction of skywave propagation by using sunspot number or solar flux number solar indices, along with a host of other variables. Calculations take into account actual operating conditions which can affect performance, such as antenna types or antenna gain, minimum elevation angle, transmitter power, receiver bandwidth, minimum required signal-to-noise (S/N) ratio, and local receive noise conditions. The programs provide automatic propagation mode searching and predict E-layer, F-layer, and mixed E/F layer propagating modes and path delays, received signal (dBuV) level, receiver S/N level, total antenna gain at each radiated takeoff angle, and receive reliability estimates. Calculated distances and bearings from transmitter to receiver are also provided. The receive reliability estimates include the Total Receive Reliability which is composed of the product of Path Reliability and S/N Availability. The Path Reliability deals with the physics of the path specified by user-supplied transmitter/receiver latitude/longitude or location choices whereas the S/N Availability deals with the effects of absorption on the actual signal levels and local noise conditions relative to the minimum required S/N specified by the user. Takeoff radiation angle dependency on E, F, or multimode E/F hops along with antenna elevation angle gain, E and F layer ionospheric absorption, polarization loss, and ground reflection losses are also taken into account. Seasonal, monthly, and diurnal (daily) hourly affects are also considered on a global basis.

All of the IONSOUND programs provide comprehensive tabular hourly output display containing the quantitative predicted results at each time of interest. The HDX and HDX TURBO versions accommodate up to 9 simultaneous frequencies in the range 1.8-30 MHz and provide a single-screen 24 hour tabular summary for up to eight parameters of interest. Pre-stored station variables make the HDX and HDX TURBO versions easy-to-use for first-time users. The PRO version also offers a more comprehensive 24 hour tabular summary which can be readily displayed, printed or stored to an ASCII file. The STD and PRO versions can accommodate up to 128 frequencies over an extended range from 1.8-54 MHz and also provide three unique simulated ionospheric chirpsounder graphic outputs depicting an ionogram display which conveys a great deal of information to the user. These plots show the predicted propagation modes, their relative delays, their bandwidth extents (frequency ranges of each propagating mode) and the mode propagation reliability/availability as indicated by display dot density and plot color code. Ionograms with selectable 0-30 MHz and 0-60 MHz display viewport windows are provided for Total Link Reliability, S/N Availability, and Path Availability, with each plot depicting the possibilities for multipath as well as the predicted reliability or availability for each propagating mode and frequency. The ionogram chirp plot, in conjunction with the more traditional tabular summary, provides a user with a more detailed and intelligent assessment of propagation with respect to actual operating conditions by providing visualization of the Maximum Usable Frequency (MUF) and Lowest Usable Frequency (LUF) for each propagating mode and is widely recognized by military and commercial users. Finally, all IONSOUND versions provide the capability for printing a distance and bearing table from its on-disk, user-modifiable, ASCII data base containing DXCC country/call-sign prefix location listing and analyzing antenna height above ground versus E and F-Layer hop distances as a function of solar indices.

SKYWAVE PROPAGATION PREDICTION

Shown below, from data provided by the National Geophysical Data Center in Boulder, Colorado, is a table of smoothed running sunspot numbers for the present solar cycle along with predicted values of activity expected for 1995-1996.

| | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 |
|------|------|------|------|------|------|------|------|------|------|------|------|
| Jan | | 18 | 58 | 142 | 151 | 148 | 124 | 71 | 37 | 24 | 14* |
| Feb | | 20 | 65 | 145 | 151 | 148 | 116 | 69 | 35 | 23 | 13* |
| Mar | | 22 | 71 | 150 | 152 | 147 | 108 | 67 | 34 | 22 | 13* |
| Apr | | 24 | 78 | 154 | 149 | 146 | 103 | 64 | 34 | 21* | 12* |
| May | | 26 | 84 | 157 | 147 | 146 | 100 | 60 | 33 | 20* | 12* |
| June | | 28 | 94 | 158 | 144 | 145 | 97 | 56 | 31 | 19* | 11* |
| July | | 31 | 104 | 159 | 141 | 146 | 91 | 55 | 29 | 19* | 11* |
| Aug | | 35 | 114 | 158 | 141 | 147 | 84 | 52 | 27 | 18* | 10* |
| Sept | 12 | 39 | 121 | 157 | 142 | 145 | 80 | 49 | 27 | 18* | 9* |
| Oct | 13 | 44 | 125 | 157 | 142 | 142 | 76 | 45 | 27 | 17* | 9* |
| Nov | 15 | 47 | 130 | 158 | 142 | 138 | 74 | 41 | 26 | 16* | 8* |
| Dec | 16 | 51 | 138 | 154 | 144 | 132 | 73 | 39 | 26 | 15* | 8* |

Smoothed Sunspot Numbers for Cycle 22 and Forecasts for 1995-96.
(Predicted Values shown with an *)

IONSOUND™ Software from SkyWave Technologies

Skywave Propagation Prediction PC Software by W1FM

State-of-the-Art Forecasting for Amateur, Marine, Professional & Military users

IONSOUND HDX: \$5.00 (A great value for the beginner)

• For use with QST "How's DX?" column + additional locations

• Same propagation software bundled with the recently published 17th edition of the ARRL

Antenna Book—Sept. 1994 QST article describing the Antenna Book software

• Utilizes pre-stored parameters; provides 24 hr predictions

IONSOUND HDX TURBO: \$20.00 (\$15.00 for registered IONSOUND users)

• Low-cost upgrade to the HDX version found in The Antenna Book

• Provides world-wide latitude/longitude or DXCC database entry

IONSOUND STD: \$35.00 (\$25.00 for registered IONSOUND users)

• Provides unique color-coded IONOGRAM LUF/MUF graphics

IONSOUND PRO: \$75.00 (\$60.00 for registered IONSOUND users)

• Includes STD capabilities + comprehensive 24 hr summary table

• See April 1992 IEEE Antenna & Propagation Magazine Product Review

SPECIFY DISK SIZE. MA residents add 5% sales tax. Overseas add \$5 shipping.

Tel 617-862-6742, evenings for tech info. Send US Check/Int'l Money Order to:

SkyWave Technologies, 17 Pine Knoll Rd., Lexington, MA 02173, USA

IONSOUND SOFTWARE by W1FM

3. DIURNAL VARIATION

INDEPENDENT SCIENCE PROJECT

**DIURNAL VARIATION
OF
IONOSPHERIC
RADIO-WAVE
PROPAGATION**

**JASON HANDWERKER
LEXINGTON HIGH SCHOOL
LEXINGTON, MA
MARCH 17, 1992**

ABSTRACT

Ionized particles found in the earth's ionosphere are capable of providing support for long-distance communications in the High Frequency (HF) broadcast frequency range of 2-30 MHz. Values of signal-to-noise ratio are predicted and measured for two skywave communication paths from radio stations WWV (Fort Collins, CO) and CHU (Ottawa, Canada) to Lexington, MA. These paths are supported by refraction effects from the E and F ionized layer regions within the ionosphere. The Ionospheric Communications Analysis and Prediction (IONCAP) Program is used on an IBM-PC compatible computer to provide an assessment of the predicted receive performance levels. Shortwave receiving equipment, in conjunction with the predicted assessments, are used to monitor and track the diurnal (daily) variation of the received signal and noise levels on the five frequencies transmitted by WWV and the three frequencies transmitted by CHU. Analysis of the measurement results obtained indicate close correlation with performance predictions such that diurnal variations caused by daily ionospheric changes exhibit predictable patterns. These changes are shown to be closely related to the daily solar cycle. It is concluded that diurnal variation effects need to be considered for a wide range of frequencies when reliable HF reception is desired.

ccc

2.0

METHODOLOGY

2.1

Primary Objective

It is the object of this investigation to focus on the diurnal (or daily) variations of shortwave reception from two particular radio stations, over a range of frequencies, in order to gain insight regarding this phenomena. For this purpose, I have chosen to monitor two radio stations. WWV in Ft. Collins, CO broadcasts continuously on 2.5, 5, 10, 15, and 20 MHz. CHU in Ottawa, Canada broadcasts continuously on 3.330, 7.335, and 14.670 MHz.

WWV is a standard time and frequency radio station operated by the U.S. National Institute of Standards and Technology (NIST). Part of it's broadcast service involves dissemination of solar information and propagation at 18 minutes after each hour. It is intended that periodic monitoring of propagation information broadcast by WWV could conceivably result in additional insight into the observed propagation monitoring.

CHU is operated by the government of Canada in order to disseminate standard time information. By comparing observed reception of these ionospherically propagated frequencies with theoretical predictions for their reception, it is hoped that an understanding of this diurnal variation will be obtained.

On an hourly basis, a shortwave receiver will be tuned to each of the WWV and CHU transmitted frequencies. Indications of the received signal and noise levels (in signal strength or S-units) will be manually recorded in a table for subsequent conversion to standard power levels measured in decibels below one watt (dBW). In addition, a computation for signal-to-noise ratio will also be performed and recorded. At selected times, solar activity levels will also be recorded from the WWV geomagnetic alert transmissions at 18 minutes past the hour. The tabular data will then be plotted in a graphical form along with predicted signal and noise levels for subsequent comparison and evaluation.

2.2

Procedures and Materials

To accommodate this procedure, the following major components have been identified. These components are:

Major Project Components

1. Yaesu model FT-757GX-II Transceiver
2. Yaesu model FP-757HD Power Supply
3. Wm.M. Nye Directional Coupler
4. E.F. Johnson Directional Coupler VSWR Indicator
5. Drake TV-1000-LP Low Pass Filter
6. Radio Shack Coaxial Lightning Arrestor
7. Heathkit 5-position Coaxial Switch
8. Cushcraft model AP-8 Vertical Groundplane Antenna
9. ITT RG-214/U 50 Ohm Coaxial Cable, part no. 90484
10. Flat Braided Wire for grounding purposes
11. Amdek model System/286A Personal Computer
12. Ionospheric Communications Analysis and Prediction (IONCAP) computer software program.

Components 1-10 are utilized for radio frequency (RF) measurements and are physically part of an amateur radio station; components 11-12 are utilized for propagation prediction and analysis of data.

2.3

Safety Features

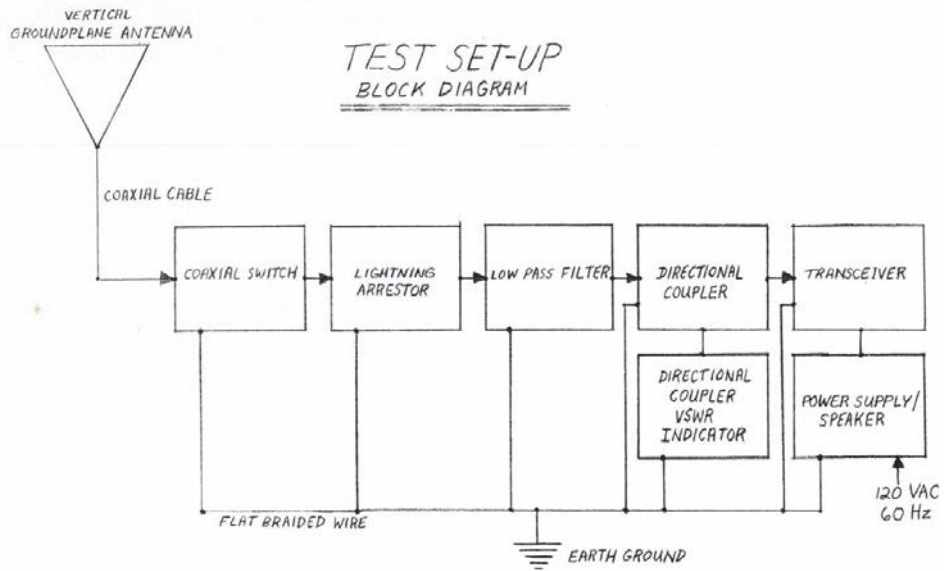
Incorporated into the materials, set-up, and procedure are several safety features in order to insure my protection and the protection of the equipment. These features are as follows:

a. To protect against electrical static build-up on the antenna when not in use, a shorting coaxial switch is used to ground the antenna.

b. A coaxial lightning arrestor with a built-in spark gap is used against high voltage induced by potential lightning hits on the antenna.

c. A braided wire ground strap is connected to all chassis grounds of all the equipment used in the test set-up. The ground strap is then connected to a cold water pipe which runs to an outside Earth ground.

d. All measurements were conducted in fair weather to minimize the possibility of lightning strikes.



3.0

DATA

Data was manually recorded from S-meter readings taken on the Yaesu FT-757 transceiver for February 22, 1992 and February 29, 1992. The data consisted of various signal and noise readings from WWV (transmitting at 2.5, 5.0, 10, 15 and 20 MHz) and CHU (transmitting at 3.330, 7.335 and 14.670 MHz) taken at one hour intervals for a 24-hour period for each day. The data collected was then inputted to a spreadsheet program on the computer where it was later tabulated and graphed. See Appendix I for additional tables and graphs.

[Note: WWV and CHU are standard frequency and time stations which are broadcast 24 hours a day, continuously, by the governments of the United States and Canada, respectively.]

WWV Solar Activity Reports monitored during the days that data was taken is summarized below:

WWV Solar Activity Reports for February 22 and 29, 1992

| <u>Local Time</u> | <u>Solar Flux Number</u> | <u>A Index</u> | <u>K Index</u> | <u>Conditions</u> |
|-------------------|--------------------------|----------------|----------------|---|
| 0018 (2/22) | 217 | 62 | 4 | Last 24 Hours Solar: Moderate Geomagnetic: Quiet-to-Storm Next 24 Hours Solar: Moderate Geomag: Unsettled-to-Storm |
| 1318 (2/22) | 217 | 62 | 3 | Last 24 Hours Solar: Moderate Geomag: Quiet-to-Minor Storm Next 24 Hours: Moderate Geomag: Unsettled-to-Active |
| 2218 (2/22) | 235 | 20 | 3 | Last 24 Hours: Low Geomagnetic: Flat Next 24: Quiet-to-Minor Storm Geomag: Unsettled-to-Active |
| 0118 (2/29) | 233 | 3 | 2 | Last 24 Hours: Low Geomagnetic: Quiet Next 24 Hours: Mid-to-High Geomag: Minor-to-Major Storm |
| 0818 (2/29) | 233 | 3 | 4 | Last 24 Hours Solar: Low Geomagnetic: Quiet Next 24 Hours: Moderate Geomag: Quiet-to-Minor Storm |
| 1718 (2/29) | 218 | 28 | 4 | Last 24 Hours Solar: Moderate Geomag: Quiet-to-Minor Storm Next 24 Hours Solar: Moderate Geomag: Moderately Active |
| 2318 (2/29) | 218 | 26 | 3 | Last 24 Hours Solar: Moderate Geomag: Quiet-to-Minor Storm Next 24 Hours Solar: Moderate Geomag: Mostly Active |

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4.0

CALCULATIONS

4.1 Calculation of Predicted Values using IONCAP

Computer generated calculations have been made using the IONCAP program in order to obtain predictions of radio wave propagation from WWV to Lexington, MA and from CHU to Lexington, MA. These calculations involved the current solar activity level (sunspot number) and have been printed out for comparison with experimental data that I have collected. The IONCAP calculations are carried out as follows:

1. An input data file describing IONCAP parameters is created using a word processor. Each line of this data file corresponds to the system requirements of IONCAP.

2. A blank output data file is created for use by the IONCAP program to store prediction results.

3. A typical set of input and output files, along with all prediction results, are shown in Appendix II.

4.2 Calculation of Power (DBW) from S-Meter Readings

In order to obtain receive power measurements from S-Meter readings, the following procedures and calculations are used:

1. S-Meter readings range from S1 to S9+60 on the FT-757 receiver. The lower S-Meter readings are from calibrated from S1 to S9 in steps of 1 S unit. Above S9 the meter is calibrated in DB above S9 (i.e. S9+10 DB). Due to received signal and noise fluctuations, the S-meter reading was read to the nearest whole S-unit and to the nearest multiple of 5 DB for readings above S9.

2. Since the input impedance of most receivers is $R=50$ Ohms, the power received at the receiver can be calculated from the received voltage level using:

$$\text{Power} = \text{Voltage} * \text{Current}$$

$$\text{Current} = \text{Voltage}/\text{Resistance}$$

$$\text{Power} = \text{Voltage}^2/\text{Resistance}$$

$$\text{Power for 1 uV} = (1\text{E-}6)^2/50 \text{ watts}$$

4.4 Conversion of Predicted-to-Actual Transmit Power Levels

All IONCAP predictions used a constant power level for the transmitter power at WWV or CHU. Not all transmit frequencies, however, employed the same transmit power level. Therefore, a correction factor has to be applied for each individual frequency which differs from that level used in the prediction.

1. IONCAP predictions for WWV utilized 10 kW for all frequencies. However, 2.5 and 20 MHz transmit at 2.5 kW.

2. IONCAP predictions for CHU utilized 3 kW for all frequencies. However, 3.330 and 14.670 transmit at 0.3 and 5.0 kW, respectively.

3. Therefore IONCAP signal-to-noise ratios need to be modified according to the following conversion:

$$DB = 10 \cdot \log(\text{Actual Power} / \text{Predicted Power})$$

4.5 Relationship between DB S/N and DB (S+N)/N vs. S/N

Measurements of received signals over an RF link result in readings of the receiver's S-Meter which yield an estimate of the combined received signal and noise power and the received noise power (in the absence of any signals). The figure showing Signal Power (measured in DBW) vs. S-Meter Reading provides an easy-to-use mechanism for converting the measured signal and noise reading into a power reading.

Since readings on the S-Meter can only be read down to the point where signal and noise levels are approximately equal (for any bandwidth selected), a potential problem arises when trying to estimate the signal-to-noise ratio from a reading which is in actuality a signal-plus-noise-to-noise ratio. The governing equation for measuring a received signal along with noise is given by:

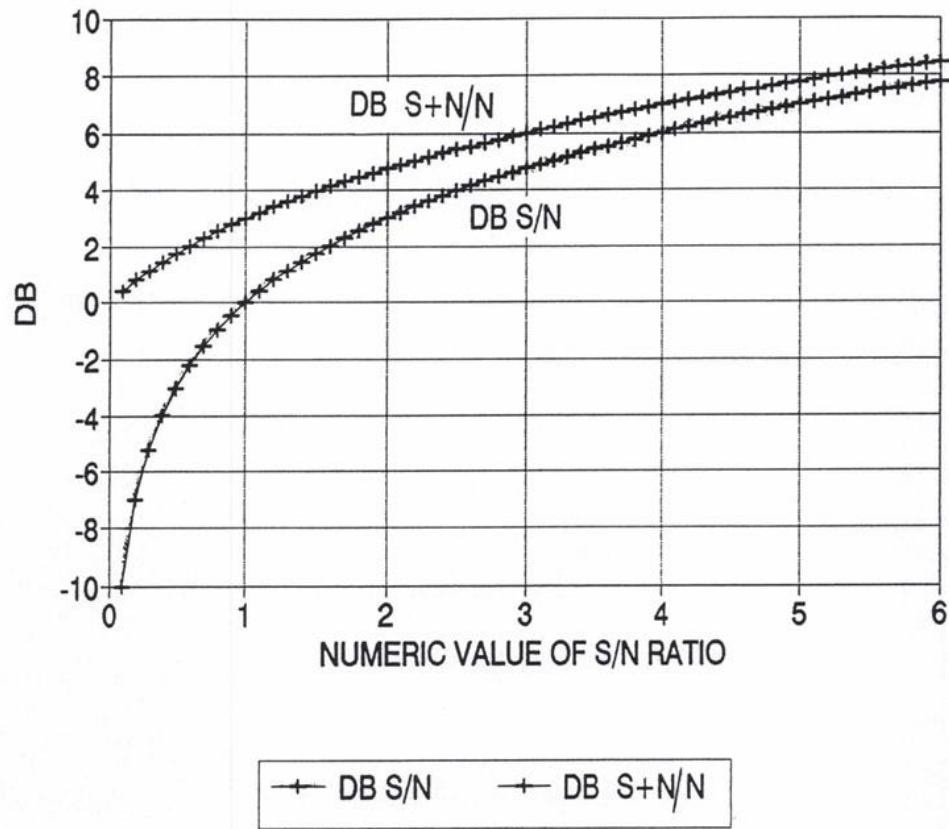
$$(\text{Signal} + \text{Noise}) / \text{Noise} = (S + N) / N = S / N + N / N = S / N + 1$$

It can therefore be seen for very large values of signal level relative to noise, the (S+N)/N ratio is going to be approximately equal to the signal-to-noise ratio. For very small signal levels relative to noise, the (S+N)/N ratio will be equal to 1 (or 0 DB). Thus, the best that can be measured for very negative signal-to-noise ratios is a (S+N)/N ratio of 0 DB since the measurement is limited by the actual noise power being observed.

It can also be seen from the chart that when the measured value of $(S+N)/N$ is approximately 6 DB, the actual value of S/N is approximately 5 DB and is only a small fraction of an S-Meter unit difference. Below the 6 DB $(S+N)/N$ reading, corresponding to a numeric S/N value of less than 3, the difference between $(S+N)/N$ and S/N diverges very rapidly; above the value of 6 DB $(S+N)/N$, the difference converges very rapidly and can be neglected. Therefore, for $(S+N)/N$ above 6 DB, there is negligible difference between the actual reading and a true measurement of S/N in DB.

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DB S/N & DB (S+N)/N VS. S/N



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Since DB is defined as:

$$DB = 10 \cdot \log(\text{Power2/Power1}) = 20 \cdot \log(\text{Voltage2/Voltage1})$$

The DBW power of 1 microvolt (across 50 Ohms) is given by:

$$\begin{aligned} \text{DBW (due to 1 uV)} &= 10 \cdot \log[(1\text{E-}6)^2/(50/1)] \\ &= 10 \cdot \log[(1\text{E-}12)/50] \\ &= -137 \text{ DBW} \end{aligned}$$

3. The calibration level of the FT-757 receiver is such that an S-Meter reading of S9 is approximately 50 microvolts (uV). This can be converted to a DB value with respect to a reference of 1uV by taking the ratio of 50uV to 1uV. This is given by:

$$\text{DBuV value of 50 uV (S9 Reading)} = 20 \cdot \log(50/1) = 34 \text{ DBuV}$$

4. Since the power for 1 uV is calculated above to be -137 DBW, the power level for 50 uV is obtained by simply adding the DB ratio of 50 uV to 1 uV (i.e., 34 DBuV) and the DBW power due to 1 uV (i.e., -137 DBW). This S9 (50 uV) power is therefore given by:

$$\text{S9 DBW Power (due to 50 uV)} = -137 + 34 = -103 \text{ DBW}$$

5. Knowing that each S-unit step is 6 DB for each S-unit and above S9 the steps are just DB values, all of the values of DBW can be calculated from the S9 S-Meter reading. (See table for S-meter Reading Conversions to DBW and DBuV. Also see chart for DBW vs. S-meter Reading.)

4.3 Conversion of 1 Hz Noise Bandwidth to 6000 Hz Noise Bandwidth

IONCAP computes signal-to-noise ratios in a normalized 1 Hz noise bandwidth. Since the FT-757 measurement receiver has a 6000 Hz (6 KHz) bandwidth for receiving Amplitude Modulation (AM) signals such as WWV and CHU, a conversion calculation is necessary. This DB ratio conversion adjusts the amount of noise from the 1 Hz prediction to the 6 KHz noise prediction and is given by:

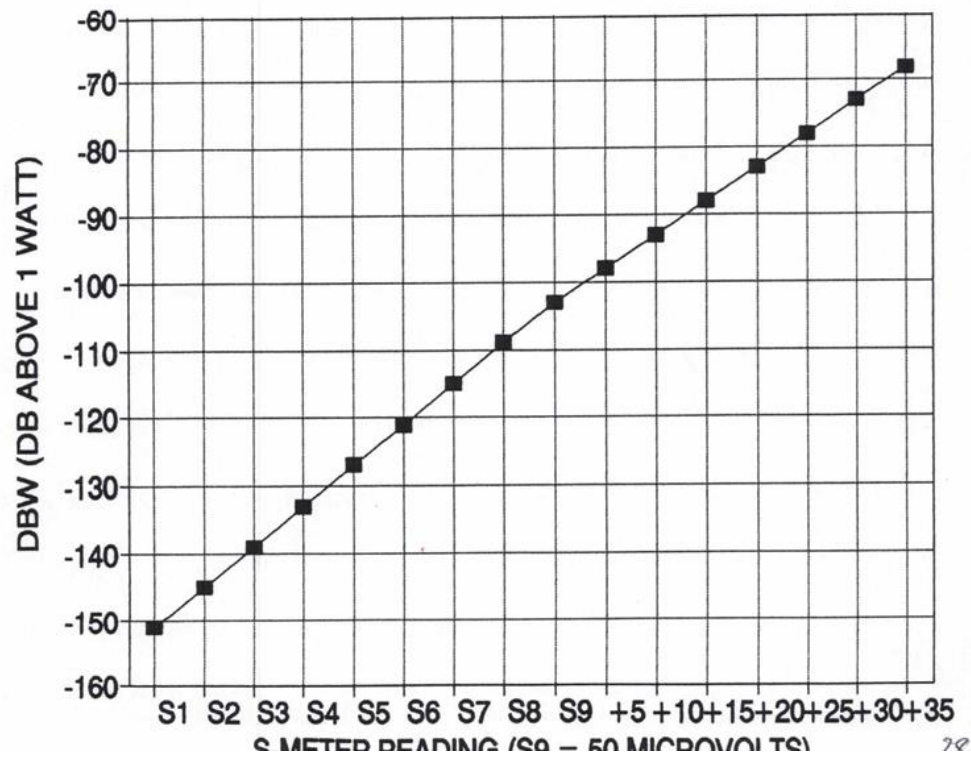
$$\text{DB Ratio of 1 Hz to 6000 Hz} = 10 \cdot \log(1/6000) = -38 \text{ DB}$$

Therefore IONCAP signal-to-noise ratios need to be reduced by 38 DB in order compare them to the measurement bandwidth of 6 KHz used in the FT-757 receiver for AM reception.

S-METER READING CONVERSIONS TO DBW AND DBUV

| S-METER READING | DBW (DB ABOVE 1 WATT) | DBUV (DB ABOVE 1UV) |
|-----------------|--------------------------|------------------------|
| S1 | -151 | -14 |
| S2 | -145 | -8 |
| S3 | -139 | -2 |
| S4 | -133 | 4 |
| S5 | -127 | 10 |
| S6 | -121 | 16 |
| S7 | -115 | 22 |
| S8 | -109 | 28 |
| S9 | -103 | 34 |
| S9+5 | -98 | 39 |
| S9+10 | -93 | 44 |
| S9+15 | -88 | 49 |
| S9+20 | -83 | 54 |
| S9+25 | -78 | 59 |
| S9+30 | -73 | 64 |

■ S-METER READING



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LABEL      CHU - OTTAWA, CANADA TO LEXINGTON, MA
CIRCUIT    45.30N  75.75W  41.40N  72.25W      0
SYSTEM     3.0  -4.  .001  90 5500 1000  85
MONTH      1992   2
SUNSPOT    157.
COMMENT    TIME      0   24   2

COMMENT    FPROB      1.0  1.0  1.0  1.0

COMMENT    METHOD      1

COMMENT    EXECUTE

COMMENT    CHANGE CRITICAL FREQUENCY MULTIPLIER FOR ES BACK TO PROGRAM DEFAULT
FPROB      OFF
COMMENT    ES CRITICAL FREQUENCY NOW IS MULTIPLIED BY .7 TO ALLOW FOR MEDIAN LOSS
COMMENT    METHOD      2

COMMENT    TIME      12   12   1  -1

COMMENT    EXECUTE

COMMENT    *****
COMMENT    METHODS 3 THROUGH 11 ARE MUF CALCULATIONS (METHOD 12 NOT IMPLEMENTED)
COMMENT    METHODS 3,4,5 AND 6 ARE MUF USING NOMOGRAM AND AREN'T PRESENTED HERE
COMMENT    TIME      1   24   1

COMMENT    METHOD      7

COMMENT    OUTPUT METHODS 8 THROUGH 11 WITHOUT RECOMPUTATION USING "OUTGRAPH"
COMMENT    OUTGRAPH   8   9  10  11

COMMENT    EXECUTE

OUTGRAPH    OFF
COMMENT    *****
COMMENT    METHODS 13 THROUGH 15 ARE ANTENNA PATTERN CALCULATIONS
COMMENT    METHODS 13 AND 14 ARE ANTENNAS ONE AT A TIME AND AREN'T PRESENTED HERE
COMMENT    ANTOUT      ANTFIL.BIN
COMMENT    METHOD      15

COMMENT    ANTENNA     1   2      .001 4.      -0.5

COMMENT    ANTENNA     2   2      .001 4.      -0.25

COMMENT    ANTENNA     1  18 ANTFIL.BIN
COMMENT    ANTENNA     2  18 ANTFIL.BIN
COMMENT    EXECUTE

COMMENT    ANTOUT      OFF
COMMENT    *****
COMMENT    METHODS 16 THROUGH 23 ARE SYSTEM PERFORMANCE PREDICTIONS
FREQUENCY   2.5  3.3  5.0  7.3  10.0 14.7 15.0 20.0
TIME        1   24   1
COMMENT    METHOD      16

COMMENT    EXECUTE

COMMENT    METHOD      17

COMMENT    EXECUTE

COMMENT    METHOD      18

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COMMENT      METHOD      19
COMMENT      EXECUTE

COMMENT      METHOD      20
COMMENT      EXECUTE

COMMENT      METHOD 21 FORCES THE PROGRAM TO EXERCISE THE "LONG" PATH MODEL
COMMENT      METHOD      21
COMMENT      EXECUTE

COMMENT      METHOD 22 FORCES THE PROGRAM TO EXERCISE THE "SHORT" PATH MODEL
METHOD      22
EXECUTE

COMMENT      METHOD 23 ALLOWS THE USER TO SELECT THE DESIRED OUTPUT BY SPECIFYING
COMMENT      PREDEFINED LINE NUMBERS ON THE "TOPLINES" AND "BOTLINES" CARDS
COMMENT      LINES ARE NUMBERED IN ORDER AS IN METHOD 20 (SEE TABLES 8 AND 9)
COMMENT      METHOD      23

COMMENT      TOPLINES      1      2      3      4      5      6      7
COMMENT      BOTLINES      1      2      4      10     11     12

COMMENT      EXECUTE

COMMENT      *****
COMMENT      METHOD 24 IS THE MUF-RELIABILITY TABLE
COMMENT      *****
METHOD      24
TIME      1      24      1
EXECUTE

COMMENT      *****
COMMENT      METHOD 25 IS THE ALL MODES TABLE
COMMENT      METHOD      25

COMMENT      NOTE THAT THE MUF ALL MODES TABLE IS ALSO PRINTED
COMMENT      FREQUENCY      2.5      5.0      10.0      15.0      20.0

COMMENT      TIME      1      24      1

COMMENT      EXECUTE

COMMENT      *****
COMMENT      METHODS 26 THROUGH 29 ARE LUF PREDICTIONS
METHOD      26
COMMENT      OUTPUT METHODS 27, 28 AND 29 WITHOUT RECOMPUTATION USING "OUTGRAPH"
COMMENT      OUTGRAPH      27      28      29

COMMENT      TIME      2      24      2

COMMENT      EXECUTE

COMMENT      OUTGRAPH      OFF

COMMENT      *****
COMMENT      *****

```

METHOD 22 IONCAP PC.20 PAGE 1

FEB 1992 SSN = 157.
 CHU - OTTAWA, CANADA TO LEXINGTON, MA AZIMUTHS N. MI. KM
 45.30 N 75.75 W - 41.40 N 72.25 W 145.66 328.06 279.5 517.6
 MINIMUM ANGLE .0 DEGREES
 TS- 1 ANTENNA PACKAGE
 XMTR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 RCVR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 POWER = 3.000 KW 3 MHZ NOISE = -163.6 DBW REQ. REL = .90 REQ. SNR = 55.0
 MULTIPATH POWER TOLERANCE = 10.0 DB MULTIPATH DELAY TOLERANCE = .850 MS

UT MUF

| | | | | | | | | | | | | | |
|-----|------|------|------|------|------|------|------|------|------|----|----|----|--------|
| 1.0 | 9.4 | 2.5 | 3.3 | 5.0 | 7.3 | 10.0 | 14.7 | 15.0 | 20.0 | .0 | .0 | .0 | FREQ |
| | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | - | - | - | MODE |
| | 55.9 | 45.4 | 44.7 | 45.1 | 47.8 | 55.9 | 55.9 | 55.9 | 55.9 | - | - | - | ANGLE |
| | 3.3 | 2.6 | 2.5 | 2.6 | 2.7 | 3.3 | 3.3 | 3.3 | 3.3 | - | - | - | DELAY |
| | 412. | 279. | 273. | 277. | 305. | 412. | 412. | 412. | 412. | - | - | - | V HITE |
| | .50 | 1.00 | 1.00 | 1.00 | .99 | .27 | .00 | .00 | .00 | - | - | - | F DAYS |
| | 121. | 108. | 109. | 111. | 114. | 125. | 183. | 183. | 186. | - | - | - | LOSS |
| | 40. | 43. | 44. | 45. | 46. | 37. | -18. | -18. | -18. | - | - | - | DBU |
| | -86 | -71 | -72 | -75 | -78 | -89 | -148 | -148 | -150 | - | - | - | S DBW |
| | -162 | -150 | -152 | -155 | -159 | -164 | -172 | -172 | -180 | - | - | - | N DBW |
| | 77. | 78. | 79. | 80. | 81. | 74. | 24. | 24. | 30. | - | - | - | SNR |
| | -6. | -13. | -13. | -15. | -16. | -1. | 40. | 39. | 33. | - | - | - | RPWRG |
| | .96 | 1.00 | 1.00 | 1.00 | 1.00 | .91 | .02 | .01 | .00 | - | - | - | REL |
| | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | - | - | - | MPROB |
| | .60 | .70 | .73 | .76 | .79 | .51 | .01 | .01 | .02 | - | - | - | S PRB |
| | 14. | 6. | 6. | 7. | 7. | 17. | 7. | 7. | 7. | - | - | - | SIG LW |
| | 6. | 3. | 3. | 4. | 3. | 8. | 18. | 14. | 3. | - | - | - | SIG UP |
| 2.0 | 8.3 | 2.5 | 3.3 | 5.0 | 7.3 | 10.0 | 14.7 | 15.0 | 20.0 | .0 | .0 | .0 | FREQ |
| | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | 1F2 | - | - | - | MODE |
| | 56.5 | 46.2 | 46.0 | 47.0 | 51.2 | 56.5 | 56.5 | 56.5 | 56.5 | - | - | - | ANGLE |
| | 3.3 | 2.6 | 2.6 | 2.6 | 2.9 | 3.3 | 3.3 | 3.3 | 3.3 | - | - | - | DELAY |
| | 423. | 287. | 285. | 296. | 344. | 423. | 423. | 423. | 423. | - | - | - | V HITE |
| | .50 | 1.00 | 1.00 | 1.00 | .87 | .03 | .00 | .00 | .00 | - | - | - | F DAYS |
| | 116. | 103. | 104. | 106. | 110. | 132. | 178. | 178. | 181. | - | - | - | LOSS |
| | 45. | 48. | 49. | 50. | 49. | 30. | -13. | -13. | -13. | - | - | - | DBU |
| | -80 | -66 | -68 | -70 | -74 | -97 | -143 | -143 | -146 | - | - | - | S DBW |
| | -160 | -147 | -150 | -154 | -158 | -163 | -173 | -173 | -181 | - | - | - | N DBW |
| | 79. | 80. | 81. | 83. | 83. | 66. | 30. | 30. | 35. | - | - | - | SNR |
| | -5. | -13. | -13. | -14. | -13. | 14. | 37. | 37. | 31. | - | - | - | RPWRG |
| | .95 | .99 | 1.00 | 1.00 | .99 | .72 | .00 | .00 | .00 | - | - | - | REL |
| | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | - | - | - | MPROB |
| | .57 | .69 | .71 | .73 | .72 | .33 | .02 | .02 | .05 | - | - | - | S PRB |
| | 18. | 10. | 10. | 11. | 13. | 25. | 11. | 11. | 11. | - | - | - | SIG LW |
| | 6. | 4. | 4. | 4. | 4. | 15. | 3. | 3. | 3. | - | - | - | SIG UP |

METHOD 24 IONCAP PC.20 PAGE 13

FEB 1992 SSN = 157.

CHU - OTTAWA, CANADA TO LEXINGTON, MA AZIMUTHS N. MI. KM
 45.30 N 75.75 W - 41.40 N 72.25 W 145.66 328.06 279.5 517.6

MINIMUM ANGLE .0 DEGREES

TS- 1 ANTENNA PACKAGE

XMTR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 RCVR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 POWER = 3.000 KW 3 MHZ NOISE = -163.6 DBW REQ. REL = .90 REQ. SNR = 55.0

FREQUENCY / RELIABILITY

| UT | MUF | 2.5 | 3.3 | 5.0 | 7.3 | 10.0 | 14.7 | 15.0 | 20.0 | - | - | - | MUF |
|----|------|------|------|------|------|------|------|------|------|---|---|---|-----|
| 1 | 9.4 | 1.00 | 1.00 | 1.00 | 1.00 | .91 | .02 | .01 | .00 | - | - | - | .96 |
| 2 | 8.3 | .99 | 1.00 | 1.00 | .99 | .72 | .00 | .00 | .00 | - | - | - | .95 |
| 3 | 7.6 | .99 | .99 | .99 | .97 | .54 | .00 | .00 | .01 | - | - | - | .94 |
| 4 | 7.1 | .99 | .99 | .99 | .92 | .34 | .00 | .00 | .01 | - | - | - | .94 |
| 5 | 6.7 | .99 | .99 | .99 | .87 | .20 | .00 | .00 | .01 | - | - | - | .93 |
| 6 | 6.6 | .99 | .99 | .99 | .85 | .16 | .01 | .01 | .01 | - | - | - | .94 |
| 7 | 6.5 | .99 | .99 | .99 | .82 | .09 | .01 | .01 | .01 | - | - | - | .89 |
| 8 | 6.0 | .99 | .99 | .98 | .68 | .00 | .01 | .01 | .01 | - | - | - | .88 |
| 9 | 5.1 | .99 | .99 | .87 | .18 | .00 | .01 | .01 | .01 | - | - | - | .85 |
| 10 | 4.5 | .99 | .99 | .81 | .01 | .00 | .00 | .00 | .01 | - | - | - | .87 |
| 11 | 5.3 | .99 | .99 | .97 | .23 | .00 | .00 | .00 | .01 | - | - | - | .92 |
| 12 | 7.4 | .99 | .99 | .99 | .95 | .33 | .00 | .00 | .01 | - | - | - | .91 |
| 13 | 10.1 | .86 | .99 | 1.00 | 1.00 | .96 | .07 | .05 | .00 | - | - | - | .93 |
| 14 | 12.4 | .09 | .59 | .96 | .98 | .98 | .59 | .54 | .00 | - | - | - | .82 |
| 15 | 13.7 | .00 | .15 | .94 | .99 | .99 | .75 | .71 | .00 | - | - | - | .86 |
| 16 | 14.3 | .00 | .01 | .48 | .97 | .98 | .80 | .76 | .00 | - | - | - | .86 |
| 17 | 14.5 | .00 | .00 | .36 | .96 | .98 | .81 | .77 | .02 | - | - | - | .86 |
| 18 | 14.6 | .00 | .01 | .49 | .98 | .99 | .82 | .78 | .01 | - | - | - | .88 |
| 19 | 14.5 | .00 | .17 | .97 | 1.00 | .99 | .77 | .74 | .01 | - | - | - | .79 |
| 20 | 14.3 | .18 | .76 | 1.00 | 1.00 | 1.00 | .78 | .76 | .00 | - | - | - | .82 |
| 21 | 14.0 | .77 | .95 | .98 | .99 | .99 | .75 | .72 | .00 | - | - | - | .79 |
| 22 | 13.3 | .96 | .98 | .98 | .99 | .99 | .68 | .62 | .00 | - | - | - | .80 |
| 23 | 12.3 | .97 | .97 | .98 | .99 | .99 | .64 | .60 | .00 | - | - | - | .87 |
| 24 | 10.9 | .98 | .99 | .99 | 1.00 | .99 | .28 | .23 | .00 | - | - | - | .92 |

METHOD 22 IONCAP PC.20 PAGE 1

FEB 1992 SSN = 157.
 WWV - FT. COLLINS, CO TO LEXINGTON, MA AZIMUTHS N. MI. KM
 40.67 N 105.00 W - 41.40 N 72.25 W 77.43 279.27 1474.9 2731.2
 MINIMUM ANGLE .0 DEGREES
 1TS- 1 ANTENNA PACKAGE
 XMTR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 RCVR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 POWER = 10.000 KW 3 MHZ NOISE = -163.6 DBW REQ. REL = .90 REQ. SNR = 55.0
 MULTIPATH POWER TOLERANCE = 10.0 DB MULTIPATH DELAY TOLERANCE = .850 MS

UT MUF

| | | | | | | | | | | | | | |
|-----|------|------|------|------|------|------|----|----|----|----|----|----|--------|
| 1.0 | 26.4 | 2.5 | 5.0 | 10.0 | 15.0 | 20.0 | .0 | .0 | .0 | .0 | .0 | .0 | FREQ |
| | 1F2 | 2 E | 1F2 | 1F2 | 1F2 | 1F2 | - | - | - | - | - | - | MODE |
| | 9.8 | 4.9 | 7.6 | 4.1 | 4.3 | 5.1 | - | - | - | - | - | - | ANGLE |
| | 9.8 | 9.3 | 9.6 | 9.4 | 9.4 | 9.5 | - | - | - | - | - | - | DELAY |
| | 403. | 96. | 344. | 254. | 259. | 278. | - | - | - | - | - | - | V HITE |
| | .50 | 1.00 | 1.00 | 1.00 | 1.00 | .99 | - | - | - | - | - | - | F DAYS |
| | 147. | 146. | 142. | 135. | 136. | 138. | - | - | - | - | - | - | LOSS |
| | 33. | 10. | 22. | 33. | 35. | 35. | - | - | - | - | - | - | DBU |
| | -102 | -104 | -98 | -93 | -95 | -98 | - | - | - | - | - | - | S DBW |
| | -185 | -150 | -155 | -164 | -172 | -180 | - | - | - | - | - | - | N DBW |
| | 83. | 45. | 56. | 70. | 77. | 82. | - | - | - | - | - | - | SNR |
| | -9. | 19. | 7. | -9. | -17. | -24. | - | - | - | - | - | - | RPWRG |
| | .97 | .15 | .59 | 1.00 | 1.00 | 1.00 | - | - | - | - | - | - | REL |
| | .00 | .00 | .17 | .00 | .00 | .00 | - | - | - | - | - | - | MPROB |
| | .60 | .10 | .25 | .70 | .91 | .96 | - | - | - | - | - | - | S PRB |
| | 18. | 2. | 1. | 1. | 2. | 2. | - | - | - | - | - | - | SIG LW |
| | 13. | 7. | 8. | 6. | 6. | 6. | - | - | - | - | - | - | SIG UP |
| 2.0 | 22.6 | 2.5 | 5.0 | 10.0 | 15.0 | 20.0 | .0 | .0 | .0 | .0 | .0 | .0 | FREQ |
| | 1F2 | 2 E | 1F2 | 1F2 | 1F2 | 1F2 | - | - | - | - | - | - | MODE |
| | 10.0 | 5.1 | 5.2 | 4.5 | 5.0 | 6.5 | - | - | - | - | - | - | ANGLE |
| | 9.8 | 9.3 | 9.5 | 9.4 | 9.5 | 9.6 | - | - | - | - | - | - | DELAY |
| | 409. | 99. | 282. | 264. | 277. | 316. | - | - | - | - | - | - | V HITE |
| | .50 | 1.00 | 1.00 | 1.00 | 1.00 | .88 | - | - | - | - | - | - | F DAYS |
| | 146. | 140. | 141. | 135. | 136. | 138. | - | - | - | - | - | - | LOSS |
| | 34. | 16. | 24. | 34. | 35. | 35. | - | - | - | - | - | - | DBU |
| | -100 | -99 | -96 | -92 | -94 | -98 | - | - | - | - | - | - | S DBW |
| | -183 | -147 | -154 | -163 | -173 | -181 | - | - | - | - | - | - | N DBW |
| | 82. | 48. | 57. | 71. | 78. | 83. | - | - | - | - | - | - | SNR |
| | -9. | 15. | 5. | -10. | -18. | -23. | - | - | - | - | - | - | RPWRG |
| | .97 | .24 | .63 | 1.00 | 1.00 | 1.00 | - | - | - | - | - | - | REL |
| | .00 | .00 | .20 | .00 | .00 | .00 | - | - | - | - | - | - | MPROB |
| | .59 | .16 | .27 | .71 | .90 | .91 | - | - | - | - | - | - | S PRB |
| | 18. | 2. | 1. | 1. | 2. | 4. | - | - | - | - | - | - | SIG LW |
| | 13. | 7. | 10. | 7. | 7. | 7. | - | - | - | - | - | - | SIG UP |

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METHOD 24 IONCAP PC.20 PAGE 13

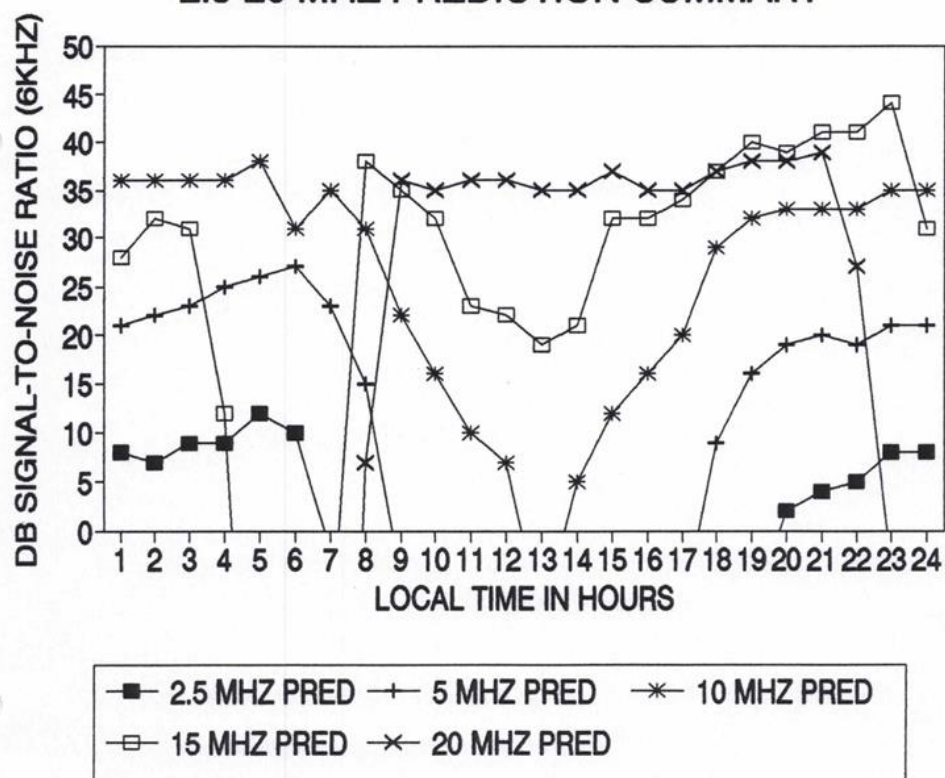
FEB 1992 SSN = 157
 WWV - FT. COLLINS, CO TO LEXINGTON, MA AZIMUTHS N. MI. KM
 40.67 N 105.00 W - 41.40 N 72.25 W 77.43 279.27 1474.9 2731.2
 MINIMUM ANGLE .0 DEGREES
 TS- 1 ANTENNA PACKAGE
 XMTR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 RCVR 2.0 TO 30.0 CONST. GAIN H .00 L .00 A .0 OFF AZ .0
 POWER = 10.000 KW 3 MHZ NOISE = -163.6 DBW REQ. REL = .90 REQ. SNR = 55.0

FREQUENCY / RELIABILITY

| UT | MUF | 2.5 | 5.0 | 10.0 | 15.0 | 20.0 | - | - | - | - | - | - | MUF |
|----|------|-----|-----|------|------|------|---|---|---|---|---|---|-----|
| 1 | 26.4 | .15 | .59 | 1.00 | 1.00 | 1.00 | - | - | - | - | - | - | .97 |
| 2 | 22.6 | .24 | .63 | 1.00 | 1.00 | 1.00 | - | - | - | - | - | - | .97 |
| 3 | 19.2 | .26 | .63 | 1.00 | 1.00 | .81 | - | - | - | - | - | - | .90 |
| 4 | 16.2 | .34 | .77 | 1.00 | 1.00 | .22 | - | - | - | - | - | - | .89 |
| 5 | 14.2 | .36 | .79 | 1.00 | .76 | .00 | - | - | - | - | - | - | .88 |
| 6 | 13.8 | .34 | .79 | 1.00 | .71 | .00 | - | - | - | - | - | - | .89 |
| 7 | 14.2 | .33 | .81 | 1.00 | .78 | .00 | - | - | - | - | - | - | .90 |
| 8 | 14.1 | .38 | .85 | 1.00 | .77 | .00 | - | - | - | - | - | - | .90 |
| 9 | 12.7 | .43 | .90 | 1.00 | .39 | .00 | - | - | - | - | - | - | .88 |
| 10 | 10.8 | .47 | .92 | .99 | .00 | .00 | - | - | - | - | - | - | .85 |
| 11 | 9.9 | .42 | .94 | .75 | .00 | .00 | - | - | - | - | - | - | .84 |
| 12 | 11.9 | .05 | .83 | 1.00 | .07 | .00 | - | - | - | - | - | - | .75 |
| 13 | 17.5 | .00 | .39 | .99 | 1.00 | .42 | - | - | - | - | - | - | .89 |
| 14 | 24.9 | .00 | .00 | .73 | 1.00 | 1.00 | - | - | - | - | - | - | .90 |
| 15 | 30.9 | .00 | .00 | .42 | .98 | 1.00 | - | - | - | - | - | - | .96 |
| 16 | 34.2 | .00 | .00 | .14 | .79 | 1.00 | - | - | - | - | - | - | .97 |
| 17 | 35.4 | .00 | .00 | .04 | .66 | 1.00 | - | - | - | - | - | - | .99 |
| 18 | 35.6 | .00 | .00 | .00 | .58 | .99 | - | - | - | - | - | - | .93 |
| 19 | 35.5 | .00 | .00 | .03 | .62 | 1.00 | - | - | - | - | - | - | .93 |
| 20 | 35.0 | .00 | .00 | .19 | .97 | 1.00 | - | - | - | - | - | - | .97 |
| 21 | 35.0 | .00 | .00 | .40 | 1.00 | 1.00 | - | - | - | - | - | - | .96 |
| 22 | 34.9 | .00 | .00 | .61 | .99 | 1.00 | - | - | - | - | - | - | .93 |
| 23 | 33.5 | .00 | .18 | .96 | 1.00 | 1.00 | - | - | - | - | - | - | .92 |
| 24 | 30.4 | .02 | .44 | .99 | 1.00 | 1.00 | - | - | - | - | - | - | .96 |

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WWV-LEXINGTON, MA SSN=157 FEB 2.5-20 MHZ PREDICTION SUMMARY



Comparison of Predictions With Measured Data
 CHU-Ottawa, Canada to Lexington, MA
 22 February 1992 SSN=157 F=3.330 MHz

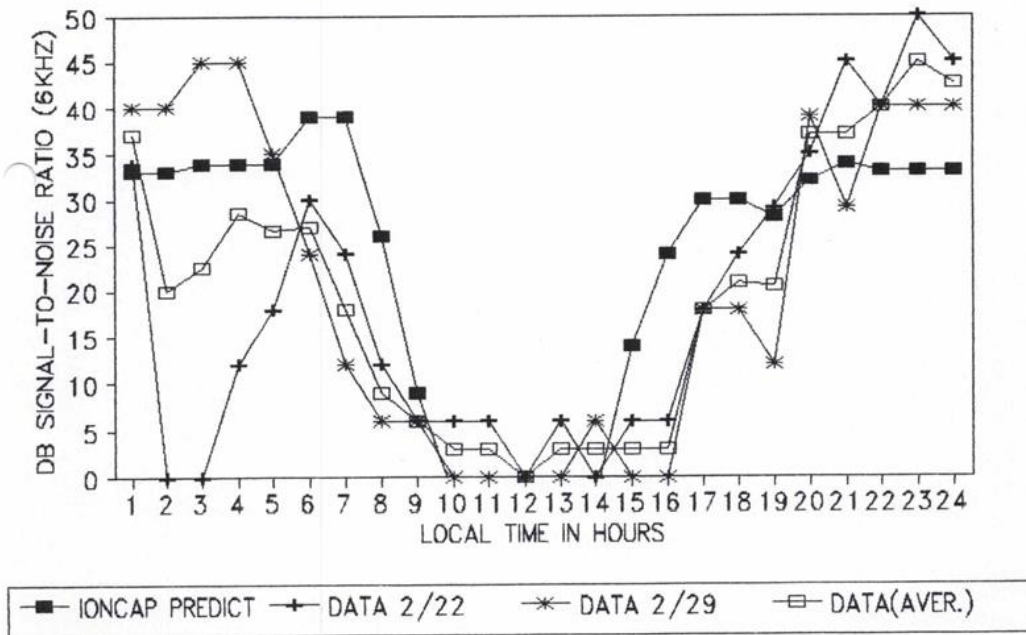
IONCAP PREDICTED DATA

| Loc. Time | 3KW Sig(DBW) | 0.3KW Sig(DBW) | 1HZ N (DBW) | 6KHZ N (DBW) | 6KHZ S/N(DB) |
|-----------|-----------------|-------------------|----------------|-----------------|-----------------|
| 1 | -67 | -77 | -148 | -110 | 33 |
| 2 | -67 | -77 | -148 | -110 | 33 |
| 3 | -67 | -77 | -149 | -111 | 34 |
| 4 | -68 | -78 | -150 | -112 | 34 |
| 5 | -69 | -79 | -151 | -113 | 34 |
| 6 | -67 | -77 | -154 | -116 | 39 |
| 7 | -72 | -82 | -159 | -121 | 39 |
| 8 | -88 | -98 | -162 | -124 | 26 |
| 9 | -107 | -117 | -164 | -126 | 9 |
| 10 | -119 | -129 | -165 | -127 | -2 |
| 11 | -131 | -141 | -165 | -127 | -14 |
| 12 | -136 | -146 | -165 | -127 | -19 |
| 13 | -131 | -141 | -165 | -127 | -14 |
| 14 | -118 | -128 | -164 | -126 | -2 |
| 15 | -102 | -112 | -164 | -126 | 14 |
| 16 | -89 | -99 | -161 | -123 | 24 |
| 17 | -81 | -91 | -159 | -121 | 30 |
| 18 | -78 | -88 | -156 | -118 | 30 |
| 19 | -78 | -88 | -154 | -116 | 28 |
| 20 | -72 | -82 | -152 | -114 | 32 |
| 21 | -68 | -78 | -150 | -112 | 34 |
| 22 | -67 | -77 | -148 | -110 | 33 |
| 23 | -67 | -77 | -148 | -110 | 33 |
| 24 | -67 | -77 | -148 | -110 | 33 |

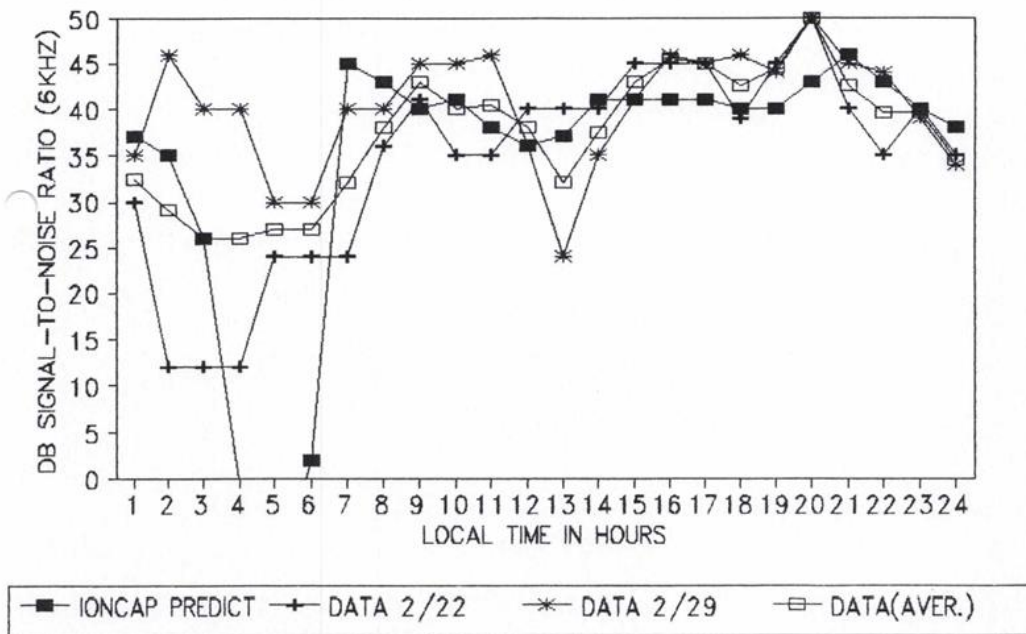
MEASURED DATA

| Loc. Time | 0.3KW Sig(DBW) | 6KHZ N (DBW) | 6KHZ S/N(DB) |
|-----------|-------------------|-----------------|-----------------|
| 1 | -93 | -127 | 34 |
| 2 | -133 | -133 | 0 |
| 3 | -133 | -133 | 0 |
| 4 | -115 | -127 | 12 |
| 5 | -109 | -127 | 18 |
| 6 | -103 | -133 | 30 |
| 7 | -109 | -133 | 24 |
| 8 | -127 | -139 | 12 |
| 9 | -133 | -139 | 6 |
| 10 | -133 | -139 | 6 |
| 11 | -127 | -133 | 6 |
| 12 | -127 | -127 | 0 |
| 13 | -127 | -133 | 6 |
| 14 | -133 | -133 | 0 |
| 15 | -133 | -139 | 6 |
| 16 | -127 | -133 | 6 |
| 17 | -115 | -133 | 18 |
| 18 | -109 | -133 | 24 |
| 19 | -98 | -127 | 29 |
| 20 | -98 | -133 | 35 |
| 21 | -88 | -133 | 45 |
| 22 | -93 | -133 | 40 |
| 23 | -83 | -133 | 50 |
| 24 | -88 | -133 | 45 |

CHU-LEXINGTON, MA SSN=157 3.330 MHZ PRED. VS. MEASURED SUMMARY

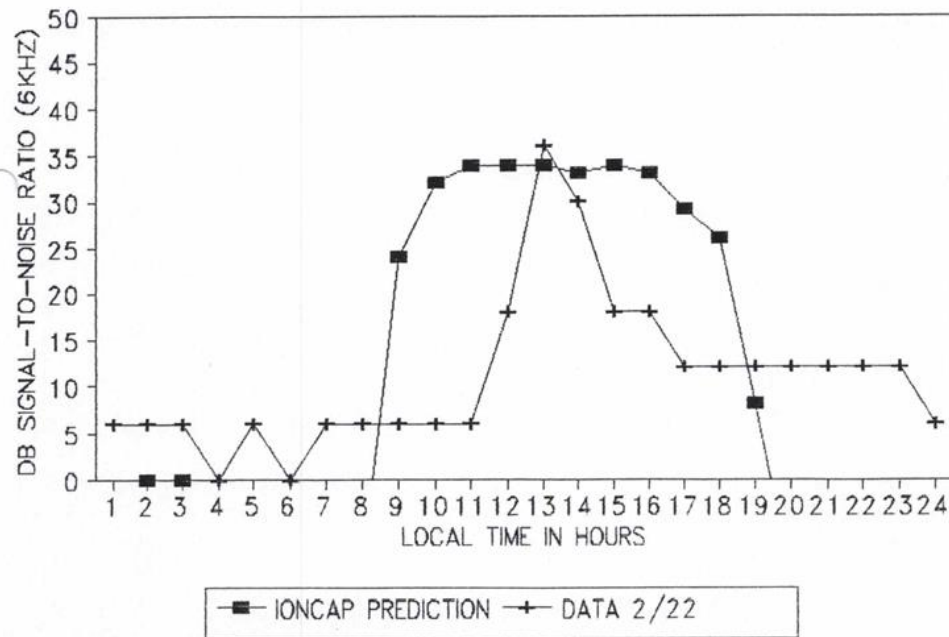


CHU-LEXINGTON, MA SSN=157 7.335 MHZ PRED. VS. MEASURED SUMMARY

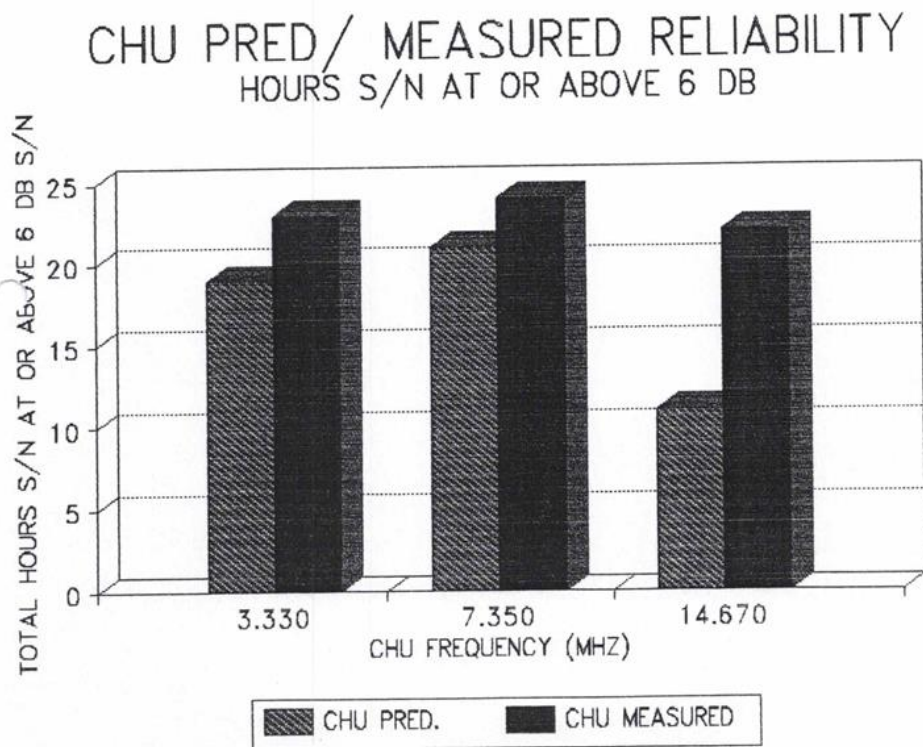


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CHU-LEXINGTON, MA SSN=157 14.670 MHZ PRED. VS. MEASURED SUMMARY



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Comparison of Predictions With Measured Data
 WWV-Ft. Collins, CO to Lexington, MA
 22 February 1992 SSN=157 F=10Mhz

IONCAP PREDICTED DATA

| Loc. Time | 10KW Sig(DBW) | 10KW Sig(DBW) | 1HZ N (DBW) | 6KHZ N (DBW) | 6KHZ S/N(DB) |
|-----------|------------------|------------------|----------------|-----------------|-----------------|
| 1 | -92 | -92 | -166 | -128 | 36 |
| 2 | -93 | -93 | -167 | -129 | 36 |
| 3 | -93 | -93 | -167 | -129 | 36 |
| 4 | -93 | -93 | -167 | -129 | 36 |
| 5 | -91 | -91 | -167 | -129 | 38 |
| 6 | -98 | -98 | -167 | -129 | 31 |
| 7 | -94 | -94 | -167 | -129 | 35 |
| 8 | -98 | -98 | -167 | -129 | 31 |
| 9 | -108 | -108 | -168 | -130 | 22 |
| 10 | -115 | -115 | -169 | -131 | 16 |
| 11 | -120 | -120 | -168 | -130 | 10 |
| 12 | -123 | -123 | -168 | -130 | 7 |
| 13 | -139 | -139 | -167 | -129 | -10 |
| 14 | -124 | -124 | -167 | -129 | 5 |
| 15 | -116 | -116 | -166 | -128 | 12 |
| 16 | -112 | -112 | -166 | -128 | 16 |
| 17 | -107 | -107 | -165 | -127 | 20 |
| 18 | -97 | -97 | -164 | -126 | 29 |
| 19 | -94 | -94 | -164 | -126 | 32 |
| 20 | -93 | -93 | -164 | -126 | 33 |
| 21 | -92 | -92 | -163 | -125 | 33 |
| 22 | -92 | -92 | -163 | -125 | 33 |
| 23 | -91 | -91 | -164 | -126 | 35 |
| 24 | -92 | -92 | -165 | -127 | 35 |

MEASURED DATA

| Loc. Time | 10KW Sig(DBW) | 6KHZ N (DBW) | 6KHZ S/N(DB) |
|-----------|------------------|-----------------|-----------------|
| 1 | -103 | -145 | 42 |
| 2 | -109 | -145 | 36 |
| 3 | -109 | -145 | 36 |
| 4 | -109 | -145 | 36 |
| 5 | -98 | -145 | 47 |
| 6 | -93 | -145 | 52 |
| 7 | -109 | -145 | 36 |
| 8 | -121 | -145 | 24 |
| 9 | -121 | -145 | 24 |
| 10 | -127 | -145 | 18 |
| 11 | -139 | -145 | 6 |
| 12 | -139 | -139 | 0 |
| 13 | -139 | -145 | 6 |
| 14 | -139 | -145 | 6 |
| 15 | -139 | -145 | 6 |
| 16 | -133 | -145 | 12 |
| 17 | -127 | -145 | 18 |
| 18 | -127 | -145 | 18 |
| 19 | -109 | -145 | 36 |
| 20 | -109 | -145 | 36 |
| 21 | -103 | -145 | 42 |
| 22 | -103 | -145 | 42 |
| 23 | -93 | -145 | 52 |
| 24 | -98 | -145 | 47 |

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Comparison of Predictions With Measured Data
 WWV-Ft. Collins, CO to Lexington, MA
 29 February 1992 SSN=157 F=5.0Mhz

IONCAP PREDICTED DATA

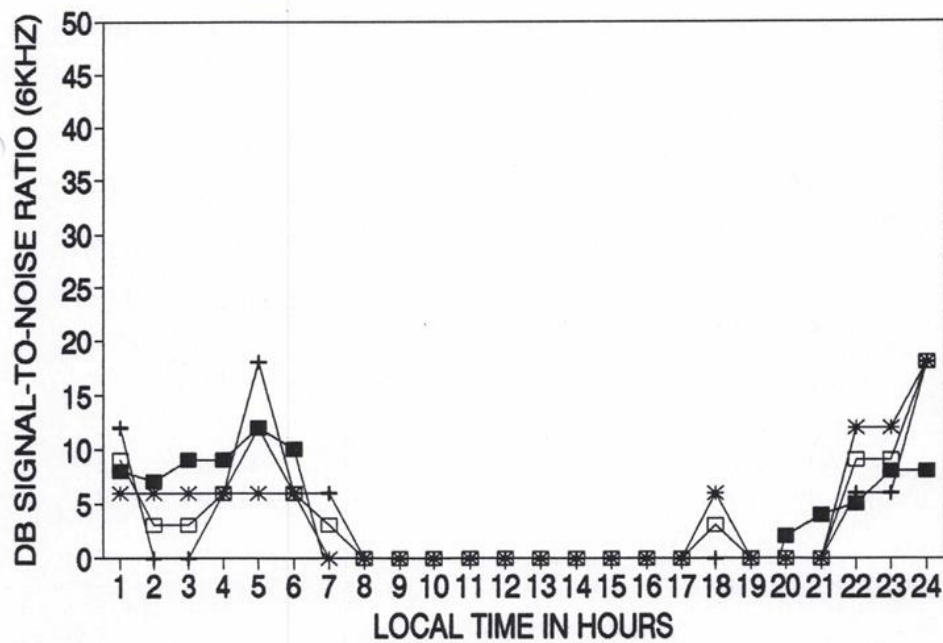
| Loc. Time | 10KW Sig(DBW) | 10KW Sig(DBW) | 1HZ N (DBW) | 6KHZ N (DBW) | 6KHZ S/N(DB) |
|-----------|------------------|------------------|----------------|-----------------|-----------------|
| 1 | -93 | -93 | -152 | -114 | 21 |
| 2 | -93 | -93 | -153 | -115 | 22 |
| 3 | -92 | -92 | -153 | -115 | 23 |
| 4 | -91 | -91 | -154 | -116 | 25 |
| 5 | -91 | -91 | -155 | -117 | 26 |
| 6 | -91 | -91 | -156 | -118 | 27 |
| 7 | -100 | -100 | -161 | -123 | 23 |
| 8 | -112 | -112 | -165 | -127 | 15 |
| 9 | -135 | -135 | -168 | -130 | -5 |
| 10 | -167 | -167 | -169 | -131 | -36 |
| 11 | -198 | -198 | -169 | -131 | -67 |
| 12 | -226 | -226 | -169 | -131 | -95 |
| 13 | -241 | -241 | -169 | -131 | -110 |
| 14 | -230 | -230 | -169 | -131 | -99 |
| 15 | -193 | -193 | -167 | -129 | -64 |
| 16 | -157 | -157 | -164 | -126 | -31 |
| 17 | -133 | -133 | -162 | -124 | -9 |
| 18 | -112 | -112 | -159 | -121 | 9 |
| 19 | -103 | -103 | -157 | -119 | 16 |
| 20 | -98 | -98 | -155 | -117 | 19 |
| 21 | -96 | -96 | -154 | -116 | 20 |
| 22 | -95 | -95 | -152 | -114 | 19 |
| 23 | -93 | -93 | -152 | -114 | 21 |
| 24 | -93 | -93 | -152 | -114 | 21 |

MEASURED DATA

| Loc. Time | 10KW Sig(DBW) | 6KHZ N (DBW) | 6KHZ S/N(DB) |
|-----------|------------------|-----------------|-----------------|
| 1 | -115 | -145 | 30 |
| 2 | -121 | -145 | 24 |
| 3 | -115 | -139 | 24 |
| 4 | -115 | -139 | 24 |
| 5 | -121 | -139 | 18 |
| 6 | -115 | -139 | 24 |
| 7 | -133 | -139 | 6 |
| 8 | -139 | -139 | 0 |
| 9 | -139 | -139 | 0 |
| 10 | -139 | -139 | 0 |
| 11 | -139 | -139 | 0 |
| 12 | -139 | -139 | 0 |
| 13 | -139 | -139 | 0 |
| 14 | -139 | -139 | 0 |
| 15 | -139 | -139 | 0 |
| 16 | -139 | -139 | 0 |
| 17 | -139 | -139 | 0 |
| 18 | -139 | -139 | 0 |
| 19 | -139 | -139 | 0 |
| 20 | -127 | -139 | 12 |
| 21 | -127 | -139 | 12 |
| 22 | -115 | -139 | 24 |
| 23 | -115 | -139 | 24 |
| 24 | -109 | -139 | 30 |

WWV-LEXINGTON,MA SSN=157

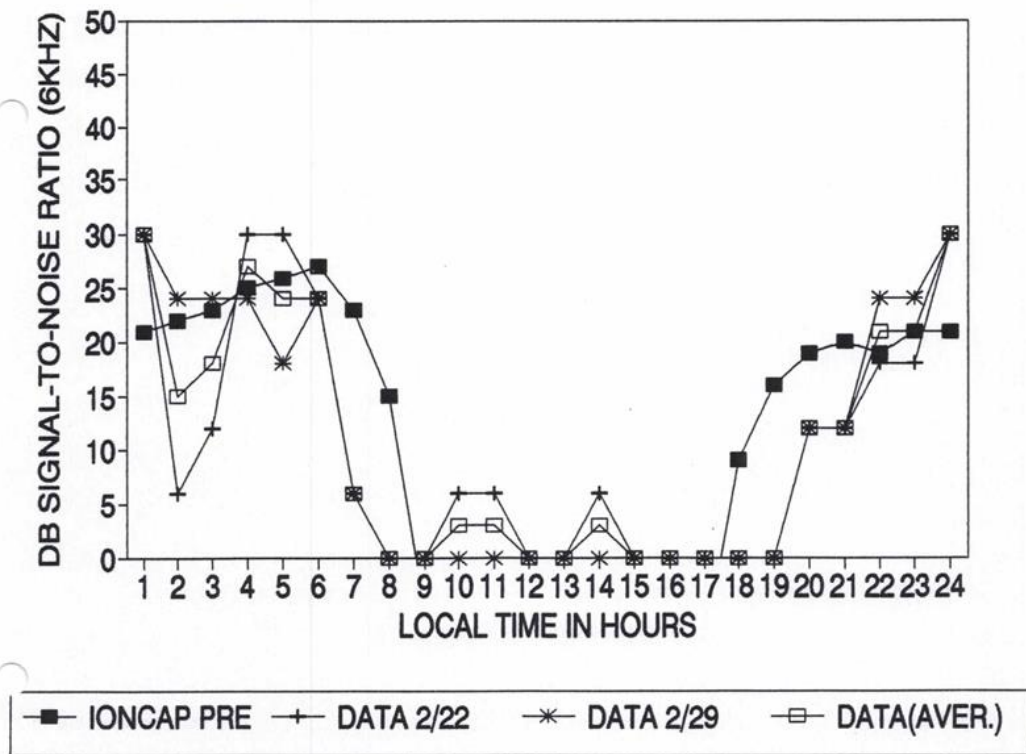
2.5 MHZ PRED. VS. MEASURED SUMMARY



■ IONCAP PRE + DATA 2/22 * DATA 2/29 □ DATA(AVER.)

WWV-LEXINGTON,MA SSN=157

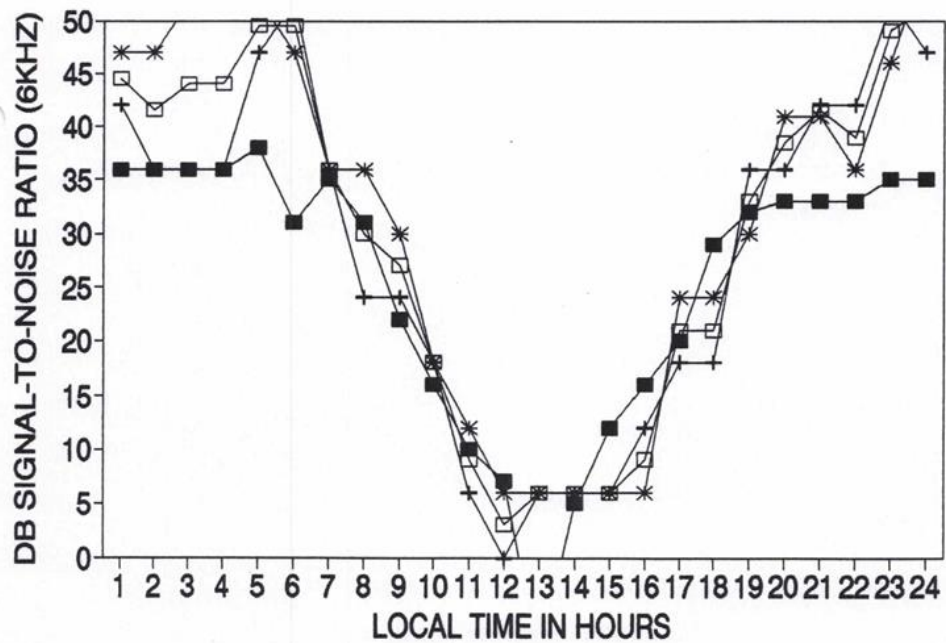
5.0 MHZ PRED. VS. MEASURED SUMMARY



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WWV-LEXINGTON,MA SSN=157

10.0 MHZ PRED. VS. MEASURED SUMMARY

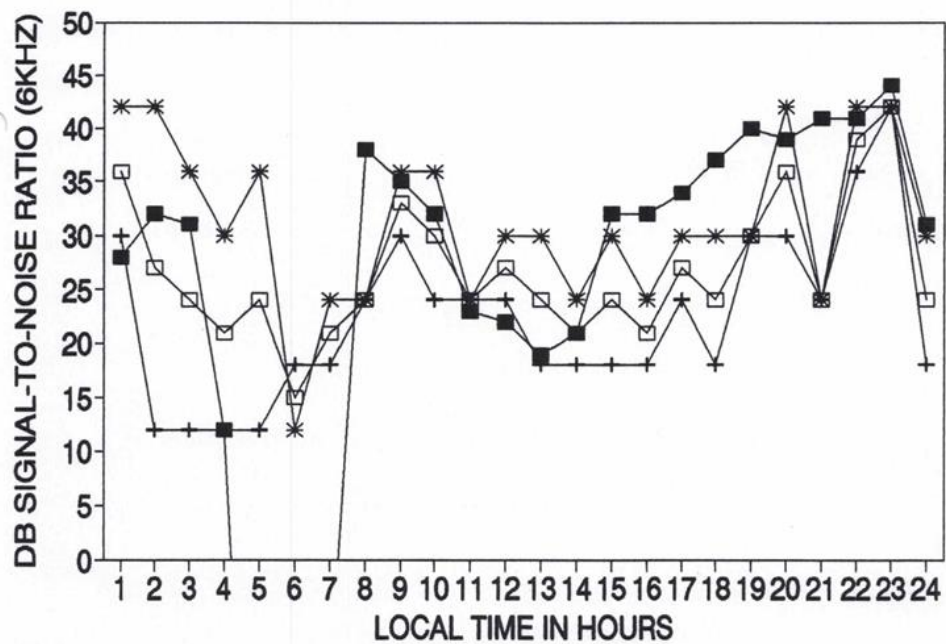


■ IONCAP PRE + DATA 2/22 * DATA 2/29 □ DATA(AVER.)

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WWV-LEXINGTON,MA SSN=157

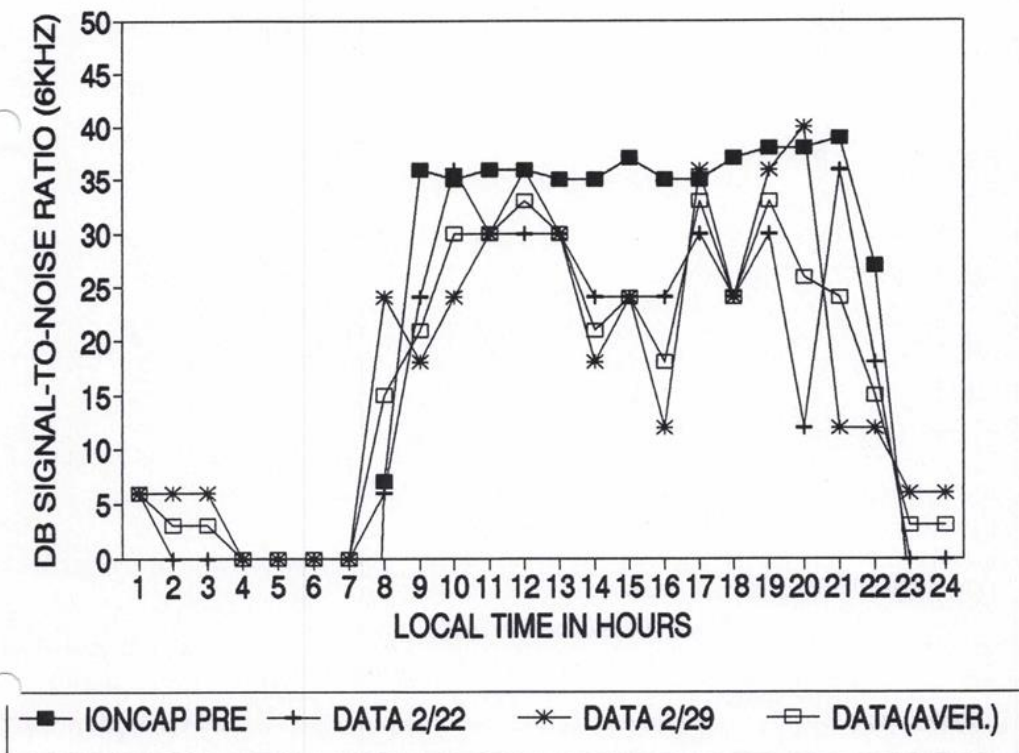
15.0 MHZ PRED. VS. MEASURED SUMMARY



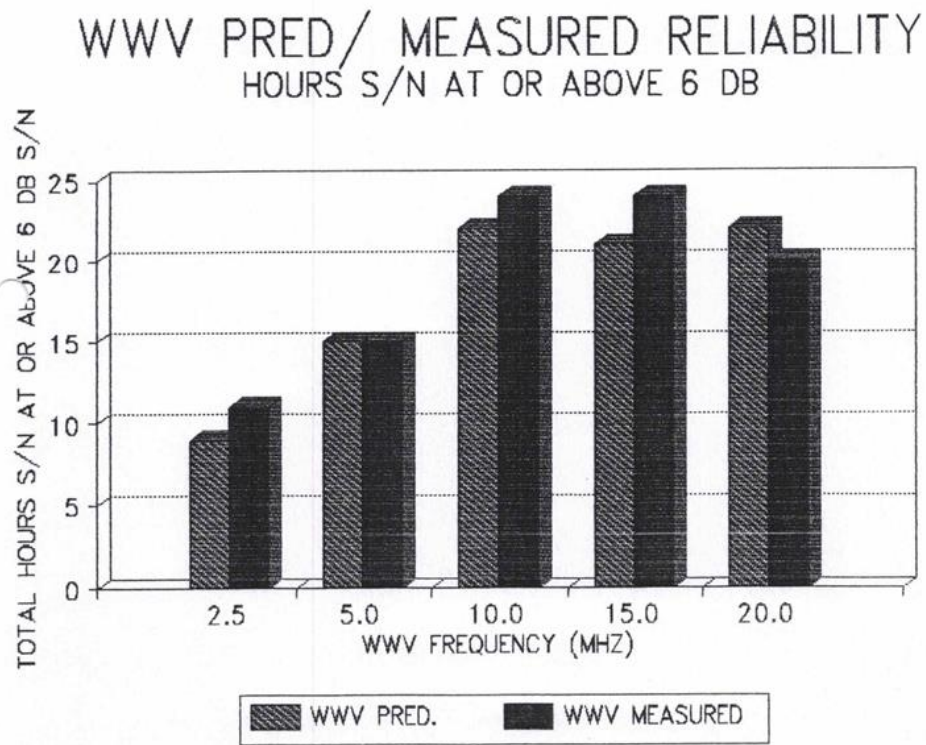
■ IONCAP PRE + DATA 2/22 * DATA 2/29 □ DATA(AVER.)

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WWV-LEXINGTON,MA SSN=157 20.0 MHZ PRED. VS. MEASURED SUMMARY



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SUMMARY OF MEASUREMENT TRENDS

TIME PERIODS VS. FREQUENCIES VS. SIGNAL CHARACTERISTICS

| | <u>MIDNIGHT</u> | <u>SUNRISE</u> | <u>NOON</u> | <u>EVENING</u> |
|---------------------------|--|-------------------------------|--|--|
| <u>GROUP #1</u> | | | | |
| <u>LOWER FREQUENCIES</u> | STRONG | STRONG | WEAK | MEDIUM |
| WWV 2.5 MHZ | LOW | LOW | HIGHEST | WEAKER |
| CHU 3.33 MHZ | ABSORP- TION | ABORP- TION | ION- IZATION | ION- IZATION |
| WWV 5.0 MHZ | | NO D- LAYER | STRONG D LAYER | D LAYER WEAKENS |
| WWV 10.0 MHZ | | | | LESS ABSORP- TION |
| <u>GROUP #2</u> | | | | |
| <u>MIDDLE FREQUENCIES</u> | STRONG | WEAK | MEDIUM | STRONG |
| CHU 7.335 MHZ | LOW | NOT | GOOD | STILL |
| WWV 15.0 MHZ | ABSORP- TION & ENOUGH ION- IZATION | ENOUGH ION- IZATION | ION- IZATION LOT OF ABSORP- TION | GOOD ION- LOWER ABSORP- TION |
| <u>GROUP #3</u> | | | | |
| <u>HIGHER FREQUENCIES</u> | WEAK | WEAK | STRONG | STRONG |
| CHU 14.67 MHZ | NOT ENOUGH | LOWEST ION- | GOOD ION- | GOOD ION- |
| WWV 20.00 MHZ | ION- IZATION | IZATION BUT ON THE RISE | IZATION | IZATION BUT WEAKENING |

NOTE: DURING THE MIDNIGHT-TO-EARLY MORNING PERIOD OF 22 FEB 1992 MEASUREMENTS, THERE WAS A PERIOD OF UNUSUALLY HIGH SOLAR AND GEOMAGNETIC ACTIVITY WHICH SEEMED TO HAVE AN EFFECT ON PROPAGATION.

5.0

ANALYSIS OF RESULTS

Certain observations concerning the measured and predicted data, located in Appendix I and II, can be derived from existing ionospheric theory and data analysis. These observations are as follows:

5.1 Analysis of CHU predicted and actual data

a. 3.330 MHz Data

The predicted data indicates that this frequency tends to propagate during nighttime hours. Shortly after sunrise the predicted signal-to-noise ratio drops off sharply such that recovery of the signal does not occur until late afternoon. The minimum signal-to-noise ratio tends to occur at noon local time. This pattern can be attributed to absorption due to the formation of the D-layer during daytime hours. The average measured data indicates somewhat lower signal-to-noise ratios for early morning hours and higher signal-to-noise ratios for late evening hours when compared to IONCAP predictions. In general the propagation tends to follow the pattern which was predicted, with minimum signal-to-noise ratios occurring during daylight hours.

b. 7.335 MHz Data

The predicted data indicates that this frequency tends to propagate best during daylight to late evening hours. Shortly before sunrise this frequency drops off very rapidly, but it recovers quickly with the onset of sunrise. This appears to be a very reliable frequency due to short outage time and high signal-to-noise ratio indicated. This pattern can be attributed to the formation and retention of the F-layer in support of propagation.

The average measured data indicates approximately the same signal-to-noise ratios, as predicted, throughout most of the measurement period. The lowest ratios occurred during the early pre-dawn time interval when IONCAP predicted outages for reception.

c. 14.670 MHz Data

The predicted data indicates that this frequency tends to propagate solely during daylight hours. Shortly after sunset to about an hour after sunrise this frequency suffers an outage. However, with the ionization of the F-Layer to sufficient states, the frequency once again has a favorable signal-to-noise ratio. Peak signal-to-noise ratios occur around noontime. This frequency is less reliable than previously mentioned frequencies.

The average measured data indicates increased signal-to-noise ratios during the nighttime hours and generally lower during daylight hours. However, the pattern established in the prediction is related to actual measurements in that peak performance occurs during daylight hours and minimum performance occurs during nighttime hours. Actual duration of peak performance, however, was small compared to the prediction but this could have been the result of intense geomagnetic activity resulting from solar storm disturbances. Such storms historically tend to affect propagation more severely in higher latitudes.

5.2 Analysis of WWV predicted and actual data

a. 2.5 MHz Data

The pattern established by predicted data indicates that this frequency primarily propagates well during nighttime hours, when the D-Layer has disappeared, resulting in lower absorption. Very shortly after sunrise, however, the signal-to-noise ratio drops off rapidly until it reaches an outage. Not until an hour after sunset does the signal-to-noise ratio-rebound. This frequency appears to have relatively low reliability because of its high overall outage period and its low signal-to-noise ratio when it is being received.

The average measured data closely follows the diurnal pattern established by the predicted data. Data minimum and maximum values occur at approximately the same time as the predicted levels. Furthermore, the frequency tended to only propagate during nighttime hours with the expected low signal-to-noise ratios.

b. 5.0 MHz Data

The pattern established by predicted data indicates that this frequency closely resembles that of 2.5 MHz. It primarily propagates well during nighttime hours and suffers outages during daylight hours. Also, the signal-to-noise ratio falls in response to sunrise and rises in response to sunset. However, this frequency is more reliable than 2.5 MHz and usually has better performance as exhibited by its higher signal-to-noise ratios. Furthermore, signal-to-noise ratio drops off slower in response to the advent of sunrise and rises more rapidly in response to the arrival of sunset. Its outage time is less than 2.5 MHz.

The average measured data is in general agreement with the pattern established by the predicted data. Both are similar in terms of performance levels, reliability, and response to daytime and nighttime hours although it did drop off slightly earlier than expected at sunrise and recovered slightly following sunset.

c. 10 MHz Data

The predicted data indicates that this frequency tends to propagate almost throughout the entire 24 hour period. However, peak propagation occurs during nighttime hours when there is minimal absorption. Performance drops during the daylight hours, reaching a minimum at approximately an hour following local noontime. This can be attributed to the effects of D-layer ionization and resulting absorption losses. As the sun starts to set, the signal-to-noise ratio levels return to their high levels. Unlike 2.5 MHz and 5.0 MHz, this frequency has the greatest reliability (i.e., least amount of predicted outage duration), very high signal-to-noise ratio performance, and is affected very gradually by sunrise and sunset.

The average measured data is in excellent agreement with the pattern established by the predicted data. The measured data also reflects similar reliability and performance. It also indicates that best performance occurs at night and that minimum performance occurs around noontime. Signal-to-noise ratios at night, however, were much higher than anticipated from the IONCAP prediction.

d. 15 MHz Data

The predicted data indicates that this frequency tends to propagate best from about an hour after sunrise to late evening hours. However, signal-to-noise ratios sharply drop off resulting in an outage just before sunrise. This can be accounted for by low F-layer ionization at this time period. Following the onset of sunrise, its performance quickly rebounds and is fairly constant throughout the day. This frequency appears to give good reliability and overall performance.

The average measured data is in good agreement with the pattern established by the predicted data. A drop off in signal-to-noise ratio occurs late in the night just before sunrise. It also reflects the same general level of reliability and performance of the predictions with the exception that no observable outage occurred during the measurement period. Additionally, the daytime dropoff in performance appeared following noontime which corresponded closely to the peak in absorption due to E layer ionization.

e. 20 MHz Data

The predicted data indicated that this frequency almost solely propagates during daylight hours, when the F-layer has a sufficient ionization level to support this type of propagation. Performance drops off in the evening and suffers an outage until an hour after sunrise. The frequency lacks some of the reliability and performance levels of 15 MHz since it is supported largely in the daytime hours only.

The average measured data is in very good agreement with the predicted data and follows a similar pattern. Peak performance occurs during daylight hours, and minimum performance occurs during nighttime hours. It also responds to arrival of sunrise and sunset at roughly the identical predicted time and in a similar manner in regard to rate of rise and fall of signal-to-noise ratio. The data recorded for the nighttime was slightly higher than predicted, and it was almost identical or slightly lower for daylight hours.

5.3 WWV and CHU Predicted vs. Measured Reliability

Each of the predictions and measurements for WWV and CHU were analyzed for the total number of hours (out of a 24 hour day) for which the signal-to-noise ratio was at or above 6 DB. In the case of the measured data, occurrences of 6 DB or higher were counted for any given hour, even if it occurred in only one day.

These findings are summarized in the WWV and CHU predicted and measured reliability bar chart showing the respective frequencies. For the CHU case, both the 7.350 MHz predicted and measured frequency had the greatest overall reliability. For the WWV case, 10 MHz had the greatest predicted reliability but 10 MHz and 15 MHz each had the greatest number of hours in which the signal-to-noise ratio was measured at 6 DB or higher.

PREDICTED AND MEASURED
HOURS ABOVE 6 DB S/N RATIO

WWV PREDICTED

| 2.5 | 5.0 | 10.0 | 15.0 | 20.0 |
|-----|-----|------|------|------|
| 9 | 15 | 22 | 21 | 22 |

WWV MEASURED

| 2.5 | 5.0 | 10.0 | 15.0 | 20.0 |
|-----|-----|------|------|------|
| 11 | 15 | 24 | 24 | 20 |

CHU PREDICTED

| 3.330 | 7.350 | 14.670 |
|-------|-------|--------|
| 19 | 21 | 11 |

CHU MEASURED

| 3.330 | 7.350 | 14.670 |
|-------|-------|--------|
| 23 | 24 | 22 |

25

6.0

CONCLUSIONS

1. The diurnal changes for radio frequency propagation from WWV and CHU exhibited very close correspondence to IONCAP predictions. Although a limited amount of data was collected, the resulting averages appeared to be closely correlated with predicted time outage durations and values of predicted signal-to-noise ratio. In general, measurements made on both the WWV and CHU paths to Lexington were very agreeable with IONCAP predictions.

2. Onset of sunrise and sunset, along with the noontime position of the sun, appear to identify the major time-related events affecting increases or decreases in observed signal-to-noise ratio performance. The physical processes in the ionosphere which affect the D, E, and F layers therefore appear to be closely correlated to these events. These processes thus appear to govern the structure of the ionized layers which determine the characteristics of each of the observed frequencies. Therefore, the diurnal variation of the received frequencies appear to be strongly correlated to the daily solar cycle.

3. Geomagnetic disturbances, monitored on WWV solar activity alert broadcasts, did appear to influence ionospheric behavior to some extent so that some measurements did not always achieve their expected values. As an example, this appeared to occur on the highest frequency (14.670 MHz) for the north-south path from CHU to Lexington, MA. This difference in behavior between predicted and measured results could be attributed to geomagnetic storm conditions which have a tendency to depress propagation performance in higher latitudes. As a result, the high levels of signal-to-noise ratio expected for this path did not materialize as often as had been expected.

4. IONCAP predictions can be used with great confidence to predict forecasts of propagation. Using this prediction technique, it is observed that close correlation exists between the propagation predictions and actual measurements when taken on an average basis. I believe that if more data was taken, the overall average measured performance would be even closer to the predictions. It should be noted that the IONCAP predictions correspond to quiet conditions for geomagnetic activity levels although these conditions don't always exist in nature. Additionally, the IONCAP predictions did not appear to be too sensitive to sunspot number variations since the actual equivalent sunspot number at times was much higher than used in the propagation forecasts.

5. When considering diurnal variation, HF signal reception can be improved when 2 or more widely separated frequencies are used.

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NOTE: JASON HANDWERKER IS NOW:

DR. JASON HANDWERKER / N1UEQ

4. IONSOUND HDX TURBO SOFTWARE PREDICTIONS

SkyWave Technologies Products

- **IONSOUND HDX**
 - Introductory Software
 - Bundled with ARRL Antenna Book
 - Accommodates QST 'How's DX?'
- **IONSOUND HDX TURBO**
 - Added features to HDX version
 - Permits unrestricted Lat/Lon entry
- **IONSOUND STD**
 - Simulated IONOGRAM graphics
- **IONSOUND PRO**
 - Added features to STD version

IONSOUND Software Features

- | | |
|------------------------------|-------------------------------|
| ▪ Menu Driven MMI | ▪ Prestored Tx/Rx |
| ▪ Prestored Variables | Locations/Freq List |
| ▪ Default Parameters | -User Modifiable |
| ▪ Tabular Summaries | ▪ Auto Co-Processor |
| - 24 Hour Total Rel, | Support |
| Path & Sig Avail, | ▪ Ant Gain Summary |
| S/N, Ang, dBuV, E/F | ▪ Antenna Height & |
| Hops, S-Meter Sig | Hop Dist. Analysis |
| Level; Indiv. Times | ▪ Dist/Bearing Table |
| ▪ Color/BW Support | ▪ Chirp Plot Graphics |

Add'l Contest & DXing Features of IONSOUND HDX TURBO Software

- **ASCII Location File Selectable for TX/RX**
 - Contains Prefixes, ITU & CQ Zones
 - Printable Dist./Bearing from Main Menu
- **Utilize Current Solar Flux for Robustness**
- **Forecast 'Look-Ahead' Predictions Using Projected Solar Flux/Sun Spot Values**
- **Analyze Antenna Stacking for Pattern Peaks/Nulls vs. E/F Hop Distances vs. SF**
- **Predict Optimum Band Opening/Closing Times With Different Working Conditions**
 - Maximize QSO Rates; Enhance QRP Ops

Propagation Prediction Variables

- | | |
|--|---|
| ▪ Locations <ul style="list-style-type: none">-Lat/Lon entry-DXCC list | ▪ Antenna Choices <ul style="list-style-type: none">-Independent Tx/Rx-Gain/Pattern Model |
| ▪ Tx Power Level | ▪ Min. Elevation Ang. |
| ▪ Rx Noise Criteria <ul style="list-style-type: none">-Rural/Res/City | ▪ Short or Long Path |
| ▪ Rx Bandwidth | ▪ SSN or SFN Entry |
| ▪ Rx SNR Criteria | ▪ Time and Month |
| ▪ E/F Mode Search | ▪ Frequencies |
| | ▪ E/F Layer Height |

Opening Screen for IONSOUND HDX TURBO

Welcome to IONSOUND HDX TURBO
Version 3.00 by
Jacob Handwerker / W1FM
SkyWave Technologies
17 Pine Knoll Road
Lexington, MA 02173 USA

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This software is intended to complement the IONCAP predictions found in ARRL's QST magazine How's DX? column. Although the HDX software primarily represents a subset of most capabilities found in the more advanced IONSOUND versions, it provides many of the same features. The first 14 locations available for transmitter and receiver selection are identical to those shown in QST; all 21 are usable for a wide variety of geographic predictions. IONSOUND HDX TURBO provides unrestricted latitude/longitude location choices by allowing location selections from a selected file or manual lat/lon entry.

IONSOUND HDX finds today's date is: 09-13-1994
Hit <ENTER> key to continue or a number 1-12 to select a new month:

Solar Flux Number (SFN)= 84 from default parameter file
Hit <ENTER> key to choose SFN from default file or
Input a SFN (equal to or greater than 63.75) <ENTER>

TX and RX Location Screens

***** TRANSMIT LOCATION SELECTION MENU *****

| | | | |
|------------------|----|--------------------|----|
| Alaska | 1 | Central America | 15 |
| Australia | 2 | East Mediterranean | 16 |
| Central Asia | 3 | Indian Ocean | 17 |
| East Coast (USA) | 4 | Northeast (USA) | 18 |
| Eastern Europe | 5 | Northwest (USA) | 19 |
| Hawaii | 6 | Southeast (USA) | 20 |
| Japan | 7 | Southwest (USA) | 21 |
| Midwest (USA) | 8 | | |
| Puerto Rico | 9 | | |
| South America | 10 | | |
| South Pacific | 11 | | |
| Southern Africa | 12 | | |
| West Coast (USA) | 13 | LAT/LON entry | 22 |
| Western Europe | 14 | Select from File | 23 |

Enter Transmitter Selection 1-23 < 18 >

***** RX LOCATION SELECTION MENU *****

| | | | |
|------------------|----|--------------------|----|
| Alaska | 1 | Central America | 15 |
| Australia | 2 | East Mediterranean | 16 |
| Central Asia | 3 | Indian Ocean | 17 |
| East Coast (USA) | 4 | Northeast (USA) | 18 |
| Eastern Europe | 5 | Northwest (USA) | 19 |
| Hawaii | 6 | Southeast (USA) | 20 |
| Japan | 7 | Southwest (USA) | 21 |
| Midwest (USA) | 8 | | |
| Puerto Rico | 9 | | |
| South America | 10 | | |
| South Pacific | 11 | | |
| Southern Africa | 12 | | |
| West Coast (USA) | 13 | LAT/LON entry | 22 |
| Western Europe | 14 | Select from File | 23 |

Enter Receiver Selection 1-23 < 14 >

Main Menu and Prediction Time

Today's Date 09-13-1994 ***** IONSOUND HDX TURBO by W1FM *****
 * Copyright (C) 1994 SkyWave Technologies *

| (CURRENT VARIABLES) | (SELECTION CHOICES) | |
|----------------------------------|--------------------------------------|----|
| Tx Location: Northeast (USA) | Pick Time/Display 24 Hour Summary | 0 |
| Lat= 42.35 Lon= 71.05 deg | TX/RX Locations & S/L Path | 1 |
| Tx Location Noise: RES | Sunspot/Solar Flux Number (SSN/SFN) | 2 |
| Rx Location: Western Europe | Frequency Menu (ALL MF/HF AMATEUR) | 3 |
| Lat= 51.5 Lon= .2 deg | Month Menu | 4 |
| Rx Location Noise: RURAL | Variables (Noise/Ant/BW/SNR/Pwr...) | 5 |
| Tx-->Rx Bearing= 53 deg Path= S | Propagation Mode Menu | 6 |
| Distance= 3266 mi 5256 km | TX Power Level | 7 |
| Tx Power= 1 kw | Minimum Elevation Angle Menu | 8 |
| Rx Bandwidth= 3000 Hz | Swap TX/RX Locations | 9 |
| Rx min. S/N Ratio= 10 dB | Color Selection Menu | 10 |
| Tx Ant: (Y)agi-Uda | Go to DOS (Type 'EXIT' To Return) | 11 |
| Rx Ant: (Y)agi-Uda | E/F Layer Height Menu | 12 |
| Sunspot Num= 28 Solar Flux= 85 | Tabulate TX/RX Antenna Gains | 13 |
| Layer Ht HF2= 289 km HE= 115 km | Calculate Antenna Lobes/Nulls | 14 |
| Min Elev Ang= 5 E/F Ht Change= N | Choose New Lat/Lon/Cty File | 15 |
| Min F Hops= 2F F Hop Ang= 6 deg | Print Distance/Bearing Table | 16 |
| 24 Hr Summary Types= 8 (8 max.) | Select 24 Hour Summary Types/Order | 17 |
| Last Selected Mon= 9 Next Mon= 9 | Store or Load Default Variables/EXIT | 18 |

Enter Choice: (Default=Pick Time/Display: Type 0 or ENTER)

Choose Prediction Time (UTC)
 One single time from hour 1-24 (HH) or (HH.MM)
 Every hour (1..24) one at a time 25
 Separate individual times 26
 Time interval using time step 27
 24 Hour Summary Table 28
 Main Menu 29
 Enter Choice (Default = Return for 24 Hr Summary)

24 Hour Summary - Total Reliability Percentage

| UTC | MUFo | MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | TOTREL% |
|-----|------|-----|-----|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | 0 | 100 | 100 | 100 | 62 | 7 | | | | | ===== |
| 1 | 10.2 | 0 | 100 | 100 | 91 | 31 | | | | | | Northeast |
| 2 | 8.6 | 1 | 100 | 100 | 63 | | | | | | | (USA)-> |
| 3 | 8.6 | 1 | 100 | 100 | 61 | | | | | | | Western Eu |
| 4 | 8.6 | 0 | 100 | 100 | 53 | | | | | | | rope |
| 5 | 8.6 | 0 | 99 | 100 | 38 | | | | | | | (S PATH) |
| 6 | 8.7 | 0 | 90 | 100 | 39 | | | | | | | BRNG= 53 |
| 7 | 10.5 | 0 | 64 | 70 | 40 | | | | | | | 3266 mi |
| 8 | 9.1 | 0 | 0 | 31 | | | | | | | | 5256 km |
| 9 | 12.3 | 0 | | 91 | | | | | | | | MinEL= 5 |
| 10 | 14.6 | 0 | 0 | | 44 | 25 | | | | | | Min F Hop= |
| 11 | 11.5 | 0 | 0 | 0 | 20 | | | | | | | 2F 6 deg |
| 12 | 16.4 | 0 | 0 | 0 | 31 | 11 | 5 | | | | | SSN= 28 |
| 13 | 16.9 | 0 | 0 | 0 | 29 | 33 | 26 | | | | | SFN= 85 |
| 14 | 17.3 | 0 | 0 | 0 | 25 | 51 | 43 | | | | | Rx Noise= |
| 15 | 17.5 | 0 | 0 | 0 | 26 | 65 | 55 | 6 | | | | RURAL |
| 16 | 17.5 | 0 | 0 | 0 | 36 | 75 | 64 | 15 | | | | Ant= Y/Y |
| 17 | 17.3 | 0 | 0 | 0 | 57 | 81 | 69 | 22 | | | | BW= 3000 |
| 18 | 17.0 | 0 | 0 | 0 | 80 | 83 | 70 | 25 | | | | Kw= 1 |
| 19 | 16.5 | 0 | 0 | | 93 | 81 | 68 | 25 | | | | SNR= 10 |
| 20 | 15.8 | 0 | | 88 | 99 | 100 | 65 | 25 | | | | Mon= 9 |
| 21 | 15.2 | 0 | 0 | 92 | 100 | 100 | 59 | 21 | | | | ===== |
| 22 | 14.2 | 0 | 62 | 100 | 100 | 94 | 46 | 11 | | | | Screen 1/8 |
| 23 | 13.1 | 0 | 98 | 100 | 100 | 80 | 29 | | | | | (C/Q) |

24 Hour Summary - S-Meter Readings

| UTC | MUFo MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | S Mtr+dB |
|-----|----------|-----|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | 5 | 9 | 9+5 | 9+6 | 9+6 | 9+6 | | | | ===== |
| 1 | 10.2 | 5 | 9+1 | 9+5 | 9+6 | 9+6 | | | | | Northeast |
| 2 | 8.6 | 6 | 9+2 | 9+5 | 9+6 | | | | | | (USA)-) |
| 3 | 8.6 | 6 | 9+2 | 9+5 | 9+6 | | | | | | Western Eu |
| 4 | 8.6 | 5 | 9+1 | 9+5 | 9+6 | | | | | | rope |
| 5 | 8.6 | 5 | 9 | 9+5 | 9+6 | | | | | | (S PATH) |
| 6 | 8.7 | 4 | 8 | 9+4 | 9+5 | | | | | | BRNG= 53 |
| 7 | 10.5 | 0 | 6 | 9 | 9+4 | | | | | | 3266 mi |
| 8 | 9.1 | 0 | 2 | 6 | | | | | | | 5256 km |
| 9 | 12.3 | 0 | | 6 | | | | | | | MinEL= 5 |
| 10 | 14.6 | 0 | 0 | | 7 | 9 | | | | | Min F Hop= |
| 11 | 11.5 | 0 | 0 | 2 | 6 | | | | | | 2F 6 deg |
| 12 | 16.4 | 0 | 0 | 1 | 5 | 8 | 9 | | | | SSN= 28 |
| 13 | 16.9 | 0 | 0 | 1 | 4 | 8 | 9 | | | | SFN= 85 |
| 14 | 17.3 | 0 | 0 | 1 | 4 | 8 | 9 | | | | Rx Noise= |
| 15 | 17.5 | 0 | 0 | 1 | 4 | 8 | 9 | 9+1 | | | RURAL |
| 16 | 17.5 | 0 | 0 | 1 | 4 | 8 | 9 | 9+1 | | | Ant= Y/Y |
| 17 | 17.3 | 0 | 0 | 1 | 5 | 8 | 9 | 9+2 | | | BW= 3000 |
| 18 | 17.0 | 0 | 0 | 2 | 5 | 8 | 9+1 | 9+2 | | | Kw= 1 |
| 19 | 16.5 | 0 | 0 | | 6 | 9 | 9+2 | 9+3 | | | SNR= 10 |
| 20 | 15.8 | 0 | | 6 | 8 | 9+1 | 9+4 | 9+4 | | | Mon= 9 |
| 21 | 15.2 | 0 | 1 | 6 | 9 | 9+3 | 9+5 | 9+5 | | | ===== |
| 22 | 14.2 | 0 | 6 | 9 | 9+4 | 9+5 | 9+6 | 9+6 | | | Screen 2/8 |
| 23 | 13.1 | 4 | 8 | 9+4 | 9+5 | 9+6 | 9+6 | | | | (C/Q) |

24 Hour Summary - Signal-to-Noise (S/N) Ratio

| UTC | MUFo MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | S/N(dB) |
|-----|----------|------|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | -4 | 32 | 43 | 45 | 44 | 44 | | | | ===== |
| 1 | 10.2 | -1 | 34 | 43 | 45 | 44 | | | | | Northeast |
| 2 | 8.6 | 2 | 35 | 43 | 45 | | | | | | (USA)-) |
| 3 | 8.6 | 1 | 35 | 43 | 45 | | | | | | Western Eu |
| 4 | 8.6 | -2 | 34 | 43 | 45 | | | | | | rope |
| 5 | 8.6 | -4 | 29 | 43 | 45 | | | | | | (S PATH) |
| 6 | 8.7 | -9 | 22 | 42 | 45 | | | | | | BRNG= 53 |
| 7 | 10.5 | -31 | 12 | 34 | 43 | | | | | | 3266 mi |
| 8 | 9.1 | -60 | -12 | 20 | | | | | | | 5256 km |
| 9 | 12.3 | -104 | | 19 | | | | | | | MinEL= 5 |
| 10 | 14.6 | -157 | -45 | | 25 | 36 | | | | | Min F Hop= |
| 11 | 11.5 | -214 | -66 | -6 | 16 | | | | | | 2F 6 deg |
| 12 | 16.4 | -254 | -81 | -11 | 12 | 29 | 38 | | | | SSN= 28 |
| 13 | 16.9 | -278 | -90 | -14 | 9 | 28 | 37 | | | | SFN= 85 |
| 14 | 17.3 | -291 | -94 | -15 | 7 | 27 | 37 | | | | Rx Noise= |
| 15 | 17.5 | -292 | -95 | -15 | 7 | 27 | 37 | 38 | | | RURAL |
| 16 | 17.5 | -281 | -91 | -14 | 8 | 28 | 37 | 39 | | | Ant= Y/Y |
| 17 | 17.3 | -258 | -82 | -11 | 11 | 29 | 38 | 39 | | | BW= 3000 |
| 18 | 17.0 | -221 | -68 | -7 | 15 | 31 | 39 | 40 | | | Kw= 1 |
| 19 | 16.5 | -167 | -49 | | 20 | 33 | 40 | 41 | | | SNR= 10 |
| 20 | 15.8 | -114 | | 17 | 30 | 39 | 42 | 42 | | | Mon= 9 |
| 21 | 15.2 | -67 | -15 | 19 | 35 | 42 | 43 | 43 | | | ===== |
| 22 | 14.2 | -30 | 12 | 34 | 43 | 43 | 44 | 43 | | | Screen 3/8 |
| 23 | 13.1 | -8 | 26 | 42 | 45 | 44 | 44 | | | | (C/Q) |

24 Hour Summary - Signal Levels (dBuV)

| UTC | MUF _o MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | DBuV(dB) |
|-----|----------------------|------|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | 10 | 36 | 42 | 43 | 43 | 43 | | | | ===== |
| 1 | 10.2 | 13 | 38 | 42 | 43 | 43 | | | | | Northeast |
| 2 | 8.6 | 15 | 39 | 42 | 43 | | | | | | (USA)-> |
| 3 | 8.6 | 15 | 39 | 42 | 43 | | | | | | Western Eu |
| 4 | 8.6 | 12 | 38 | 42 | 43 | | | | | | rope |
| 5 | 8.6 | 10 | 33 | 42 | 43 | | | | | | (S PATH) |
| 6 | 8.7 | 5 | 26 | 41 | 42 | | | | | | BRNG= 53 |
| 7 | 10.5 | -17 | 16 | 33 | 41 | | | | | | 3266 mi |
| 8 | 9.1 | -46 | -8 | 19 | | | | | | | 5256 km |
| 9 | 12.3 | -90 | | 17 | | | | | | | MinEL= 5 |
| 10 | 14.6 | -143 | -41 | | 23 | 35 | | | | | Min F Hop= |
| 11 | 11.5 | -201 | -62 | -7 | 14 | | | | | | 2F 6 deg |
| 12 | 16.4 | -240 | -77 | -12 | 10 | 28 | 37 | | | | SSN= 28 |
| 13 | 16.9 | -265 | -86 | -15 | 7 | 27 | 36 | | | | SFN= 85 |
| 14 | 17.3 | -277 | -91 | -16 | 5 | 26 | 35 | | | | Rx Noise= |
| 15 | 17.5 | -278 | -91 | -16 | 5 | 26 | 35 | 38 | | | RURAL |
| 16 | 17.5 | -267 | -87 | -15 | 6 | 27 | 36 | 38 | | | Ant= Y/Y |
| 17 | 17.3 | -244 | -78 | -12 | 9 | 28 | 37 | 39 | | | BW= 3000 |
| 18 | 17.0 | -207 | -65 | -8 | 13 | 30 | 38 | 39 | | | Kw= 1 |
| 19 | 16.5 | -153 | -45 | | 18 | 32 | 39 | 40 | | | SNR= 10 |
| 20 | 15.8 | -100 | | 16 | 28 | 38 | 41 | 41 | | | Mon= 9 |
| 21 | 15.2 | -53 | -11 | 18 | 33 | 40 | 42 | 42 | | | ===== |
| 22 | 14.2 | -17 | 15 | 33 | 41 | 42 | 43 | 43 | | | Screen 4/8 |
| 23 | 13.1 | 5 | 30 | 41 | 42 | 43 | 43 | | | | (C/Q) |

24 Hour Summary - Takeoff Angles

| UTC | MUF _o MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | ANG(deg) |
|-----|----------------------|-----|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | 6 | 6 | 6 | 6 | 6 | 6 | | | | ===== |
| 1 | 10.2 | 20 | 6 | 6 | 6 | 6 | | | | | Northeast |
| 2 | 8.6 | 20 | 6 | 6 | 6 | | | | | | (USA)-> |
| 3 | 8.6 | 20 | 6 | 6 | 6 | | | | | | Western Eu |
| 4 | 8.6 | 20 | 6 | 6 | 6 | | | | | | rope |
| 5 | 8.6 | 6 | 14 | 6 | 6 | | | | | | (S PATH) |
| 6 | 8.7 | 6 | 10 | 6 | 6 | | | | | | BRNG= 53 |
| 7 | 10.5 | 6 | 6 | 14 | 6 | | | | | | 3266 mi |
| 8 | 9.1 | 6 | 10 | 20 | | | | | | | 5256 km |
| 9 | 12.3 | 6 | | 6 | | | | | | | MinEL= 5 |
| 10 | 14.6 | 6 | 6 | | 14 | 6 | | | | | Min F Hop= |
| 11 | 11.5 | 6 | 6 | 6 | 20 | | | | | | 2F 6 deg |
| 12 | 16.4 | 6 | 6 | 6 | 20 | 14 | 6 | | | | SSN= 28 |
| 13 | 16.9 | 6 | 6 | 6 | 20 | 14 | 6 | | | | SFN= 85 |
| 14 | 17.3 | 6 | 6 | 6 | 20 | 14 | 6 | | | | Rx Noise= |
| 15 | 17.5 | 6 | 6 | 6 | 20 | 14 | 6 | 6 | | | RURAL |
| 16 | 17.5 | 6 | 6 | 6 | 20 | 14 | 6 | 6 | | | Ant= Y/Y |
| 17 | 17.3 | 6 | 6 | 6 | 20 | 14 | 6 | 6 | | | BW= 3000 |
| 18 | 17.0 | 6 | 6 | 6 | 20 | 14 | 6 | 6 | | | Kw= 1 |
| 19 | 16.5 | 6 | 6 | | 20 | 14 | 6 | 6 | | | SNR= 10 |
| 20 | 15.8 | 6 | | 6 | 14 | 6 | 6 | 6 | | | Mon= 9 |
| 21 | 15.2 | 6 | 10 | 20 | 14 | 6 | 6 | 6 | | | ===== |
| 22 | 14.2 | 6 | 6 | 14 | 6 | 6 | 6 | 6 | | | Screen 5/8 |
| 23 | 13.1 | 6 | 14 | 6 | 6 | 6 | 6 | | | | (C/Q) |

24 Hour Summary - Lowest Order E and F Hop Modes

| UTC | MUFo MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | E/F Hops |
|-----|----------|-----|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | 4E | 2F | 2F | 2F | 2F | 2F | | | | ===== |
| 1 | 10.2 | 4F | 2F | 2F | 2F | 2F | | | | | Northeast |
| 2 | 8.6 | 4F | 2F | 2F | 2F | | | | | | (USA)-> |
| 3 | 8.6 | 4F | 2F | 2F | 2F | | | | | | Western Eu |
| 4 | 8.6 | 4F | 2F | 2F | 2F | | | | | | rope |
| 5 | 8.6 | 4E | 3F | 2F | 2F | | | | | | (S PATH) |
| 6 | 8.7 | 4E | 2FE | 2F | 2F | | | | | | BRNG= 53 |
| 7 | 10.5 | 4E | F2E | 3F | 2F | | | | | | 3266 mi |
| 8 | 9.1 | 4E | F3E | 4F | | | | | | | 5256 km |
| 9 | 12.3 | 4E | | F2E | | | | | | | MinEL= 5 |
| 10 | 14.6 | 4E | 4E | | 3F | 2F | | | | | Min F Hop= |
| 11 | 11.5 | 4E | 4E | 4E | 4F | | | | | | 2F 6 deg |
| 12 | 16.4 | 4E | 4E | 4E | 4F | 3F | 2F | | | | SSN= 28 |
| 13 | 16.9 | 4E | 4E | 4E | 4F | 3F | 2F | | | | SFN= 85 |
| 14 | 17.3 | 4E | 4E | 4E | 4F | 3F | 2F | | | | Rx Noise= |
| 15 | 17.5 | 4E | 4E | 4E | 4F | 3F | 2F | 2F | | | RURAL |
| 16 | 17.5 | 4E | 4E | 4E | 4F | 3F | 2F | 2F | | | Ant= Y/Y |
| 17 | 17.3 | 4E | 4E | 4E | 4F | 3F | 2F | 2F | | | BW= 3000 |
| 18 | 17.0 | 4E | 4E | 4E | 4F | 3F | 2F | 2F | | | Kw= 1 |
| 19 | 16.5 | 4E | 4E | | 4F | 3F | 2F | 2F | | | SNR= 10 |
| 20 | 15.8 | 4E | | 2EF | 3F | 2F | 2F | 2F | | | Mon= 9 |
| 21 | 15.2 | 4E | 3EF | 4F | 3F | 2F | 2F | 2F | | | ===== |
| 22 | 14.2 | 4E | 2EF | 3F | 2F | 2F | 2F | 2F | | | Screen 6/8 |
| 23 | 13.1 | 4E | 3F | 2F | 2F | 2F | 2F | | | | (C/Q) |

24 Hour Summary - Path Reliability Percentage

| UTC | MUFo MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | PATHREL% |
|-----|----------|-----|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | 100 | 100 | 100 | 100 | 62 | 7 | | | | ===== |
| 1 | 10.2 | 100 | 100 | 100 | 91 | 31 | | | | | Northeast |
| 2 | 8.6 | 100 | 100 | 100 | 63 | | | | | | (USA)-> |
| 3 | 8.6 | 100 | 100 | 100 | 61 | | | | | | Western Eu |
| 4 | 8.6 | 100 | 100 | 100 | 53 | | | | | | rope |
| 5 | 8.6 | 100 | 100 | 100 | 38 | | | | | | (S PATH) |
| 6 | 8.7 | 100 | 93 | 100 | 39 | | | | | | BRNG= 53 |
| 7 | 10.5 | 100 | 100 | 70 | 40 | | | | | | 3266 mi |
| 8 | 9.1 | 100 | 67 | 33 | | | | | | | 5256 km |
| 9 | 12.3 | 100 | | 100 | | | | | | | MinEL= 5 |
| 10 | 14.6 | 100 | 100 | | 45 | 26 | | | | | Min F Hop= |
| 11 | 11.5 | 100 | 100 | 100 | 24 | | | | | | 2F 6 deg |
| 12 | 16.4 | 100 | 100 | 100 | 48 | 11 | 5 | | | | SSN= 28 |
| 13 | 16.9 | 100 | 100 | 100 | 71 | 33 | 26 | | | | SFN= 85 |
| 14 | 17.3 | 100 | 100 | 100 | 91 | 52 | 43 | | | | Rx Noise= |
| 15 | 17.5 | 100 | 100 | 100 | 100 | 66 | 55 | 6 | | | RURAL |
| 16 | 17.5 | 100 | 100 | 100 | 100 | 76 | 64 | 15 | | | Ant= Y/Y |
| 17 | 17.3 | 100 | 100 | 100 | 100 | 82 | 69 | 22 | | | BW= 3000 |
| 18 | 17.0 | 100 | 100 | 100 | 100 | 83 | 70 | 25 | | | Kw= 1 |
| 19 | 16.5 | 100 | 100 | | 100 | 81 | 68 | 25 | | | SNR= 10 |
| 20 | 15.8 | 100 | | 100 | 100 | 100 | 65 | 25 | | | Mon= 9 |
| 21 | 15.2 | 100 | 100 | 100 | 100 | 100 | 60 | 21 | | | ===== |
| 22 | 14.2 | 100 | 100 | 100 | 100 | 94 | 46 | 11 | | | Screen 7/8 |
| 23 | 13.1 | 100 | 100 | 100 | 100 | 80 | 29 | | | | (C/Q) |

24 Hour Summary - Signal Reliability Percentage

| UTC | MUFo MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | SIGREL% |
|-----|----------|-----|-----|-----|------|------|------|------|------|------|------------|
| 0 | 11.9 | 0 | 100 | 100 | 100 | 100 | 100 | | | | ===== |
| 1 | 10.2 | 0 | 100 | 100 | 100 | 100 | | | | | Northeast |
| 2 | 8.6 | 1 | 100 | 100 | 100 | | | | | | (USA)-) |
| 3 | 8.6 | 1 | 100 | 100 | 100 | | | | | | Western Eu |
| 4 | 8.6 | 0 | 100 | 100 | 100 | | | | | | rope |
| 5 | 8.6 | 0 | 99 | 100 | 100 | | | | | | (S PATH) |
| 6 | 8.7 | 0 | 96 | 100 | 100 | | | | | | BRNG= 53 |
| 7 | 10.5 | 0 | 64 | 100 | 100 | | | | | | 3266 mi |
| 8 | 9.1 | 0 | 0 | 94 | | | | | | | 5256 km |
| 9 | 12.3 | 0 | | 91 | | | | | | | MinEL= 5 |
| 10 | 14.6 | 0 | 0 | | 98 | 100 | | | | | Min F Hop= |
| 11 | 11.5 | 0 | 0 | 0 | 83 | | | | | | 2F 6 deg |
| 12 | 16.4 | 0 | 0 | 0 | 63 | 99 | 100 | | | | SSN= 28 |
| 13 | 16.9 | 0 | 0 | 0 | 41 | 99 | 100 | | | | SFN= 85 |
| 14 | 17.3 | 0 | 0 | 0 | 28 | 99 | 100 | | | | Rx Noise= |
| 15 | 17.5 | 0 | 0 | 0 | 26 | 99 | 100 | 100 | | | RURAL |
| 16 | 17.5 | 0 | 0 | 0 | 36 | 99 | 100 | 100 | | | Ant= Y/Y |
| 17 | 17.3 | 0 | 0 | 0 | 57 | 99 | 100 | 100 | | | BW= 3000 |
| 18 | 17.0 | 0 | 0 | 0 | 80 | 99 | 100 | 100 | | | Kw= 1 |
| 19 | 16.5 | 0 | 0 | | 93 | 100 | 100 | 100 | | | SNR= 10 |
| 20 | 15.8 | 0 | | 88 | 99 | 100 | 100 | 100 | | | Mon= 9 |
| 21 | 15.2 | 0 | 0 | 92 | 100 | 100 | 100 | 100 | | | ===== |
| 22 | 14.2 | 0 | 62 | 100 | 100 | 100 | 100 | 100 | | | Screen 8/8 |
| 23 | 13.1 | 0 | 98 | 100 | 100 | 100 | 100 | | | | (C/Q) |

Main Menu Showing Display of Antenna Gain Selected

```

Today's Date      ***** IONSOUND HDX TURBO by W1FM *****
09-13-1994        * Copyright (C) 1994 SkyWave Technologies *
                   *****

(CURRENT VARIABLES)
Tx Location: Northeast (USA)
Lat= 42.35 Lon= 71.05 deg
Tx Location Noise: RES
Rx Location: Western Europe
Lat= 51.5 Lon= .2 deg
Rx Location Noise: RURAL
Tx-->Rx Bearing= 53 deg Path= S
Distance= 3266 mi 5256 km
Tx Power= 1 kw
Rx Bandwidth= 3000 Hz
Rx min. S/N Ratio= 10 dB
Tx Ant: (Y)agi-Uda
Rx Ant: (Y)agi-Uda
Sunspot Num= 28 Solar Flux= 85
Layer Ht HF2= 289 km HE= 115 km
Min Elev Ang= 5 E/F Ht Change= N
Min F Hops= 2F F Hop Ang= 6 deg
24 Hr Summary Types= 8 (8 max.)
Last Selected Mon= 9 Next Mon= 9

(SELECTION CHOICES)
Pick Time/Display 24 Hour Summary 0
TX/RX Locations & S/L Path 1
Sunspot/Solar Flux Number (SSN/SFN) 2
Frequency Menu (ALL MF/HF AMATEUR) 3
Month Menu 4
Variables (Noise/Ant/BW/SNR/Pwr...) 5
Propagation Mode Menu 6
TX Power Level 7
Minimum Elevation Angle Menu 8
Swap TX/RX Locations 9
Color Selection Menu 10
Go to DOS (Type 'EXIT' To Return) 11
E/F Layer Height Menu 12
Tabulate TX/RX Antenna Gains 13
Calculate Antenna Lobes/Nulls 14
Choose New Lat/Lon/Cty File 15
Print Distance/Bearing Table 16
Select 24 Hour Summary Types/Order 17
Store or Load Default Variables/EXIT 18

Enter Choice: (Default=Pick Time/Display: Type 0 or ENTER) 13

```

TX/RX Antenna Elevation Angle Gain Variation

| *** Elevation Angle vs. Transmit and Receive ANT Gain Variation *** | | | | | |
|---|--------------|-----------|-----------|------------|-----------|
| ANG(deg) | Tx+Rx (num) | Tx (dB) | Rx (dB) | Tx+Rx (dB) | ANT Codes |
| 1 | 9.492241 | 4.886844 | 4.886844 | 9.773687 | Tx=Y Rx=Y |
| 5 | 23.13322 | 6.821181 | 6.821181 | 13.64236 | Tx=Y Rx=Y |
| 10 | 67.31529 | 9.140569 | 9.140569 | 18.28114 | Tx=Y Rx=Y |
| 15 | 104.5586 | 10.0968 | 10.0968 | 20.1936 | Tx=Y Rx=Y |
| 20 | 109.2109 | 10.19133 | 10.19133 | 20.38266 | Tx=Y Rx=Y |
| 25 | 96.96384 | 9.933049 | 9.933049 | 19.8661 | Tx=Y Rx=Y |
| 30 | 80.99794 | 9.54237 | 9.54237 | 19.08474 | Tx=Y Rx=Y |
| 35 | 64.83851 | 9.059165 | 9.059165 | 18.11833 | Tx=Y Rx=Y |
| 40 | 49.59016 | 8.476977 | 8.476977 | 16.95395 | Tx=Y Rx=Y |
| 45 | 36.0019 | 7.781627 | 7.781627 | 15.56325 | Tx=Y Rx=Y |
| 50 | 24.58458 | 6.953314 | 6.953314 | 13.90663 | Tx=Y Rx=Y |
| 55 | 15.58719 | 5.963839 | 5.963839 | 11.92768 | Tx=Y Rx=Y |
| 60 | 9.001506 | 4.771576 | 4.771576 | 9.543152 | Tx=Y Rx=Y |
| 65 | 4.603479 | 3.315431 | 3.315431 | 6.630862 | Tx=Y Rx=Y |
| 70 | 2.025527 | 1.53269 | 1.53269 | 3.065381 | Tx=Y Rx=Y |
| 75 | .7632784 | -.5865852 | -.5865852 | -1.17317 | Tx=Y Rx=Y |
| 80 | .2196722 | -3.291125 | -3.291125 | -6.58225 | Tx=Y Rx=Y |
| 85 | 2.118986E-02 | -8.369359 | -8.369359 | -16.73872 | Tx=Y Rx=Y |
| 89 | 4.083621E-05 | -21.94477 | -21.94477 | -43.88955 | Tx=Y Rx=Y |

Hit Enter to Continue

TX and RX Antenna Selection Menu

Enter the number code for the following TRANSMIT Antenna or Gain

- 1) 10 dBi Gain Yagi-Uda array (over ground): 1
 - 2) 2.15 dBi gain Vertical Monopole (over ground): 2
 - 3) 5.2 dBi gain Horizontal or Vertical Dipole: 3
 - 4) 7 to 12 dBi Var. gain (1.8-30 MHz) Log Periodic & Rhombic: 4
 - 5) 23 to 28 dBi Variable gain (1.8-30 MHz) Curtain array: 5
 - 6) -40 to +40 dBi: Choose your own Isotropic gain: 6
- ANT= (Y)agi-Uda Enter Choice (Return= 0 dBi (I)sotropic): 1

Choose RX Antenna identical to TX Antenna: Y/N (Default = Y)

n

Enter the number code for the following RECEIVE Antenna or Gain

- 1) 10 dBi Gain Yagi-Uda array (over ground): 1
 - 2) 2.15 dBi gain Vertical Monopole (over ground): 2
 - 3) 5.2 dBi gain Horizontal or Vertical Dipole: 3
 - 4) 7 to 12 dBi Var. gain (1.8-30 MHz) Log Periodic & Rhombic: 4
 - 5) 23 to 28 dBi Variable gain (1.8-30 MHz) Curtain array: 5
 - 6) -40 to +40 dBi: Choose your own Isotropic gain: 6
- ANT= (Y)agi-Uda Enter Choice: (Return= 0 dB (I)sotropic) 6
- Total RX Gain (-40 to +40 dBi) (Return= 0 dBi) 0

Main Menu Showing Antenna Lobes/Nulls Selected

```

Today's Date      ***** IONSOUND HDX TURBO by W1FM *****
09-13-1994        * Copyright (C) 1994 SkyWave Technologies *
*****

(CURRENT VARIABLES)
Tx Location: Northeast (USA)
Lat= 42.35 Lon= 71.05 deg
Tx Location Noise: RES
Rx Location: Western Europe
Lat= 51.5 Lon= .2 deg
Rx Location Noise: RURAL
Tx-->Rx Bearing= 53 deg Path= 5
Distance= 3266 mi 5256 km
Tx Power= 1 kw
Rx Bandwidth= 3000 Hz
Rx min. S/N Ratio= 10 dB
Tx Ant: (Y)agi-Uda
Rx Ant: (Y)agi-Uda
Sunspot Num= 28 Solar Flux= 85
Layer Ht HF2= 289 km HE= 115 km
Min Elev Ang= 5 E/F Ht Change= N
Min F Hops= 2F F Hop Ang= 6 deg
24 Hr Summary Types= 8 (8 max.)
Last Selected Mon= 9 Next Mon= 9

(SELECTION CHOICES)
Pick Time/Display 24 Hour Summary 0
TX/RX Locations & S/L Path 1
Sunspot/Solar Flux Number (SSN/SFN) 2
Frequency Menu (ALL MF/HF AMATEUR) 3
Month Menu 4
Variables (Noise/Ant/BW/SNR/Pwr...) 5
Propagation Mode Menu 6
TX Power Level 7
Minimum Elevation Angle Menu 8
Swap TX/RX Locations 9
Color Selection Menu 10
Go to DOS (Type 'EXIT' To Return) 11
E/F Layer Height Menu 12
Tabulate TX/RX Antenna Gains 13
Calculate Antenna Lobes/Nulls 14
Choose New Lat/Lon/Cty File 15
Print Distance/Bearing Table 16
Select 24 Hour Summary Types/Order 17
Store or Load Default Variables/EXIT 18

Enter Choice: (Default=Pick Time/Display: Type 0 or ENTER) 14

```

***** ANTENNA LOBES AND NULLS *****

```

ENTER SELECTION OF ANTENNA HEIGHT UNITS:
F=Feet or M=Meters (Default = F)

Height above ground (ft): 65

Enter frequency (1.8-30 MHz) 21

Maximum number of Lobes desired (1-6) (DEFAULT=6)

```

Antenna Lobes/Nulls Calculation Summary

```

***** ANTENNA LOBES AND NULLS *****
Vertical Angle Calculations
for Antennas over Perfectly Conducting Ground
and One-Hop Distances for E-Layer & F-Layer Propagation
SS/FN= 28 / 84.83176 Frequency= 21 MHz

```

```

E-Layer ht= 115 km F-Layer ht= 289 km Ht of Antenna= 65 Feet

Segment  HORIZ Ant  VERT Ant  Angle  E Hop(km)  E Hop(mi)  F Hop(km)  F Hop(mi)
1  1ST PEAK  1ST NULL  10.37854  1013.876  629.9932  2091.553  1299.631
2  1ST NULL  1ST PEAK  21.1187  553.6707  344.035  1269.413  788.7764
3  2ND PEAK  2ND NULL  32.71436  344.321  213.9512  819.9174  509.4731
4  2ND NULL  2ND PEAK  46.10406  215.4898  133.8992  521.6332  324.1278
5  3RD PEAK  3RD NULL  64.25641  108.6083  67.48605  265.1528  164.7583

```

NO MORE LOBES/NULLS

FOR MORE LOBE/NULL CALCULATIONS TYPE Y OR N (DEFAULT=Y)

```

***** ANTENNA LOBES AND NULLS *****
Vertical Angle Calculations
for Antennas over Perfectly Conducting Ground
and One-Hop Distances for E-Layer & F-Layer Propagation
SS/FN= 28 / 84.83176 Frequency= 21 MHz

```

```

E-Layer ht= 115 km F-Layer ht= 289 km Ht of Antenna= 120 Feet

Segment  HORIZ Ant  VERT Ant  Angle  E Hop(km)  E Hop(mi)  F Hop(km)  F Hop(mi)
1  1ST PEAK  1ST NULL  5.599928  1457.14  905.425  2715.663  1687.435
2  1ST NULL  1ST PEAK  11.25426  955.6617  593.8207  1998.981  1242.109
3  2ND PEAK  2ND NULL  17.02235  678.844  421.8141  1514.916  941.3254
4  2ND NULL  2ND PEAK  22.9748  508.8018  316.1548  1177.127  731.4328
5  3RD PEAK  3RD NULL  29.20314  393.1849  244.3138  929.0298  577.2724
6  3RD NULL  3RD PEAK  35.83751  307.5285  191.0894  736.2131  457.4616
7  4TH PEAK  4TH NULL  43.08396  239.0222  148.5215  577.1449  358.6212
8  4TH NULL  4TH PEAK  51.32009  179.7239  111.6753  436.534  271.2496
9  5TH PEAK  5TH NULL  61.42944  122.5913  76.17471  299.0409  185.8154
10 5TH NULL  5TH PEAK  77.37072  50.50784  31.38411  123.6472  76.83079

```

NO MORE LOBES/NULLS

FOR MORE LOBE/NULL CALCULATIONS TYPE Y OR N (DEFAULT=Y) n

Main Menu Showing Frequency Data File Selected

```

Today's Date      ***** IONSOUND HDX TURBO by W1FM *****
09-13-1994        * Copyright (C) 1994 SkyWave Technologies *
                  *****

(CURRENT VARIABLES)
Tx Location: Northeast (USA)
Lat= 42.35 Lon= 71.05 deg
Tx Location Noise: RES
Rx Location: Western Europe
Lat= 51.5 Lon= .2 deg
Rx Location Noise: RURAL
Tx-->Rx Bearing= 53 deg Path= S
Distance= 3266 mi 5256 km
Tx Power= 1 kw
Rx Bandwidth= 3000 Hz
Rx min. S/N Ratio= 10 dB
Tx Ant: (Y)agi-Uda
Rx Ant: (Y)agi-Uda
Sunspot Num= 28 Solar Flux= 85
Layer Ht HF2= 289 km HE= 115 km
Min Elev Ang= 5 E/F Ht Change= N
Min F Hops= 2F F Hop Ang= 6 deg
24 Hr Summary Types= 8 (8 max.)
Last Selected Mon= 9 Next Mon= 9

(SELECTION CHOICES)
Pick Time/Display 24 Hour Summary 0
TX/RX Locations & S/L Path 1
Sunspot/Solar Flux Number (SSN/SFN) 2
Frequency Menu (ION_FREQ.DAT File) 3
Month Menu 4
Variables (Noise/Ant/BW/SNR/Pwr...) 5
Propagation Mode Menu 6
TX Power Level 7
Minimum Elevation Angle Menu 8
Swap TX/RX Locations 9
Color Selection Menu 10
Go to DOS (Type 'EXIT' To Return) 11
E/F Layer Height Menu 12
Tabulate TX/RX Antenna Gains 13
Calculate Antenna Lobes/Nulls 14
Choose New Lat/Lon/Cty File 15
Print Distance/Bearing Table 16
Select 24 Hour Summary Types/Order 17
Store or Load Default Variables/EXIT 18

Enter Choice: (Default=Pick Time/Display: Type 0 or ENTER)

```

24 Hour Summary Showing Prestored Frequencies

Prestored Frequencies from ION_FREQ.DAT are as follows

```

Frequency # 1 = 2.5 MHZ
Frequency # 2 = 5 MHZ
Frequency # 3 = 10 MHZ
Frequency # 4 = 15 MHZ
Frequency # 5 = 20 MHZ

```

Type Y (Continue) or N (Return to Freq Menu) (Default=Continue)

| UTC | MUFo | MHZ | 2.5 | 5.0 | 10.0 | 15.0 | 20.0 | TOTREL% |
|-----|------|-----|-----|-----|------|------|------|------------|
| 0 | 11.9 | 87 | 100 | 100 | 48 | | | ===== |
| 1 | 10.2 | 94 | 100 | 93 | 16 | | | Northeast |
| 2 | 8.6 | 95 | 100 | 65 | | | | (USA)-> |
| 3 | 8.6 | 95 | 100 | 63 | | | | Western Eu |
| 4 | 8.6 | 93 | 100 | 55 | | | | rope |
| 5 | 8.6 | 57 | 100 | 40 | | | | (S PATH) |
| 6 | 8.7 | 0 | 100 | 41 | | | | BRNG= 53 |
| 7 | 10.5 | 98 | 42 | | | | | 3266 mi |
| 8 | 10.8 | 0 | 85 | | | | | 5256 km |
| 9 | 10.4 | 0 | 0 | | | | | MinEL= 5 |
| 10 | 14.6 | 0 | | | 6 | | | Min F Hop= |
| 11 | 15.7 | 0 | 0 | 22 | 36 | | | 2F 6 deg |
| 12 | 16.4 | 0 | 0 | 30 | 60 | | | SSN= 28 |
| 13 | 16.9 | 0 | 0 | 26 | 80 | | | SFN= 85 |
| 14 | 17.3 | 0 | 0 | 20 | 96 | 10 | | Rx Noise= |
| 15 | 17.5 | 0 | 0 | 20 | 44 | 23 | | RURAL |
| 16 | 17.5 | 0 | 0 | 30 | 54 | 32 | | Ant= Y/Y |
| 17 | 17.3 | 0 | 0 | 53 | 61 | 38 | | BW= 3000 |
| 18 | 17.0 | 0 | 0 | 78 | 63 | 40 | | Kw= 1 |
| 19 | 16.5 | 0 | 0 | 92 | 100 | 40 | | SNR= 10 |
| 20 | 15.8 | 0 | 0 | 99 | 100 | 39 | | Mon= 9 |
| 21 | 15.2 | 0 | 80 | 100 | 96 | 34 | | ===== |
| 22 | 14.2 | 0 | 98 | 100 | 82 | 23 | | Screen 1/8 |
| 23 | 13.1 | 1 | 100 | 100 | 68 | 5 | | (C/Q) |

Main Menu Showing Effect of TX/RX Location Swap

```

Today's Date      ***** IONSOUND HDX TURBO by W1FM *****
09-13-1994      * Copyright (C) 1994 SkyWave Technologies *
                  *****

(CURRENT VARIABLES)
Tx Location: Western Europe
Lat= 51.5 Lon= .2 deg
Tx Location Noise: RURAL
Rx Location: Northeast (USA)
Lat= 42.34 Lon= 71.05 deg
Rx Location Noise: RES
Tx-->Rx Bearing= 288 deg Path= S
Distance= 3266 mi 5256 km
Tx Power= 1 kw
Rx Bandwidth= 3000 Hz
Rx min. S/N Ratio= 10 dB
Tx Ant: 0 dBi (Gain, Iso.
Rx Ant: (Y)agi-Uda
Sunspot Num= 28 Solar Flux= 85
Layer Ht HF2= 289 km HE= 115 km
Min Elev Ang= 5 E/F Ht Change= N
Min F Hops= 2F F Hop Ang= 6 deg
24 Hr Summary Types= 8 (8 max.)
Last Selected Mon= 9 Next Mon= 9

(SELECTION CHOICES)
Pick Time/Display 24 Hour Summary 0
TX/RX Locations & S/L Path 1
Sunspot/Solar Flux Number (SSN/SFN) 2
Frequency Menu (ION_FREQ.DAT File) 3
Month Menu 4
Variables (Noise/Ant/BW/SNR/Pwr...) 5
Propagation Mode Menu 6
TX Power Level 7
Minimum Elevation Angle Menu 8
Swap TX/RX Locations 9
Color Selection Menu 10
Go to DOS (Type 'EXIT' To Return) 11
E/F Layer Height Menu 12
Tabulate TX/RX Antenna Gains 13
Calculate Antenna Lobes/Nulls 14
Choose New Lat/Lon/Cty File 15
Print Distance/Bearing Table 16
Select 24 Hour Summary Types/Order 17
Store or Load Default Variables/EXIT 18

Enter Choice: (Default=Pick Time/Display: Type 0 or ENTER)

```

Main Menu Followed by Color Selections

```

Today's Date      ***** IONSOUND HDX TURBO by W1FM *****
09-13-1994      * Copyright (C) 1994 SkyWave Technologies *
                  *****

(CURRENT VARIABLES)
Tx Location: Northeast (USA)
Lat= 42.35 Lon= 71.05 deg
Tx Location Noise: RES
Rx Location: Western Europe
Lat= 51.5 Lon= .2 deg
Rx Location Noise: RURAL
Tx-->Rx Bearing= 53 deg Path= S
Distance= 3266 mi 5256 km
Tx Power= 1 kw
Rx Bandwidth= 3000 Hz
Rx min. S/N Ratio= 10 dB
Tx Ant: (Y)agi-Uda
Rx Ant: 0 dBi (Gain, Iso.
Sunspot Num= 28 Solar Flux= 85
Layer Ht HF2= 289 km HE= 115 km
Min Elev Ang= 5 E/F Ht Change= N
Min F Hops= 2F F Hop Ang= 6 deg
24 Hr Summary Types= 8 (8 max.)
Last Selected Mon= 9 Next Mon= 9

(SELECTION CHOICES)
Pick Time/Display 24 Hour Summary 0
TX/RX Locations & S/L Path 1
Sunspot/Solar Flux Number (SSN/SFN) 2
Frequency Menu (ION_FREQ.DAT File) 3
Month Menu 4
Variables (Noise/Ant/BW/SNR/Pwr...) 5
Propagation Mode Menu 6
TX Power Level 7
Minimum Elevation Angle Menu 8
Swap TX/RX Locations 9
Color Selection Menu 10
Go to DOS (Type 'EXIT' To Return) 11
E/F Layer Height Menu 12
Tabulate TX/RX Antenna Gains 13
Calculate Antenna Lobes/Nulls 14
Choose New Lat/Lon/Cty File 15
Print Distance/Bearing Table 16
Select 24 Hour Summary Types/Order 17
Store or Load Default Variables/EXIT 18

Enter Choice: (Default=Pick Time/Display: Type 0 or ENTER)

```

***** COLOR SELECTION MENU *****

```

Color Set 1 (YELLOW Text on BLACK) Type 1
Color Set 2 (YELLOW Text on RED) Type 2
Color Set 3 (BLUE Text on WHITE) Type 3
Color Set 4 (Normal WHITE on BLACK) Type 4
Color Set 5 (WHITE Text on BLUE) Type 5
Color Set 6 (BLACK Text on WHITE) Type 6
Color Set 7 (YELLOW Text on BLUE) Type 7
Color Set 8 (WHITE Text on GREEN) Type 8
Color Set 9 (WHITE Text on BLACK) Type 9

```

[NOTE: Actual Monitor Colors may vary]

Enter Selection (Default = 5) 4

For EGA or VGA Color Monitor Type Y; CGA Type N (Y)

TX and RX Location Selections

TX LOC is: Northeast (USA) Lat= 42.35 Lon= 71.05
 RX LOC is: Western Europe Lat= 51.5 Lon= .2
 Dist= 3266 Miles (S PATH) Front/Back Bearing at TX= 53 / 233 degrees
 Previous Transmitter Location? Type Y or N (ENTER=Yes) y

TX LOC is: Northeast (USA) LAT= 42.35 LON= 71.05
 RX LOC is: Western Europe LAT= 51.5 LON= .2
 DIST= 3266 Miles (S PATH) Front/Back Bearing at Tx= 53 / 233 DEGREES
 Previous Receiver Location? Type Y or N (ENTER=No) n

******* RX LOCATION SELECTION MENU *******

| | | | |
|------------------|----|--------------------|----|
| Alaska | 1 | Central America | 15 |
| Australia | 2 | East Mediterranean | 16 |
| Central Asia | 3 | Indian Ocean | 17 |
| East Coast (USA) | 4 | Northeast (USA) | 18 |
| Eastern Europe | 5 | Northwest (USA) | 19 |
| Hawaii | 6 | Southeast (USA) | 20 |
| Japan | 7 | Southwest (USA) | 21 |
| Midwest (USA) | 8 | | |
| Puerto Rico | 9 | | |
| South America | 10 | | |
| South Pacific | 11 | | |
| Southern Africa | 12 | | |
| West Coast (USA) | 13 | LAT/LON entry | 22 |
| Western Europe | 14 | Select from File | 23 |

Enter Receiver Selection 1-23 (14) 23

Location Selection Screen

| NUM | PREFIX | COUNTRY | CONTINENT | ITU ZONE | CQ ZONE |
|-----|--------|-------------------|-----------|----------|---------|
| 1 | 1A0 | S.M.O. of Malta | EU | 28 | 15 |
| 2 | 1S | Spratly Island | AS | 50 | 26 |
| 3 | 3A | Monaco | EU | 27 | 14 |
| 4 | 3B6 | Agalega | AF | 53 | 39 |
| 5 | 3B7 | St. Brandon | AF | 53 | 39 |
| 6 | 3B8 | Mauritius | AF | 53 | 39 |
| 7 | 3B9 | Rodriguez Is. | AF | 53 | 39 |
| 8 | 3C | Equatorial Guinea | AF | 47 | 36 |
| 9 | 3C0 | Pagalu Island | AF | 52 | 36 |
| 10 | 3D2 | Fiji | OC | 56 | 32 |
| 11 | 3D2/R | Rotuma Island | OC | 56 | 32 |
| 12 | 3D6 | Swaziland | AF | 57 | 38 |
| 13 | 3V | Tunisia | AF | 37 | 33 |
| 14 | 3W | Vietnam | AS | 49 | 26 |
| 15 | 3X | Rep. of Guinea | AF | 46 | 35 |
| 16 | 3Y/B | Bouvet Island | AF | 67 | 38 |
| 17 | 3Y/P | Peter Island | AN | 72 | 12 |
| 18 | 4K2 | Franz Josef Land | EU | 75 | 40 |
| 19 | 4S | Sri Lanka | AS | 41 | 22 |
| 20 | 4U/ITU | ITU Geneva | EU | 28 | 14 |

Choose Number 1 - 20 or Hit ENTER for More Choices (ENTER=More)

Latitude/Longitude Entry Screen

***** RX LOCATION SELECTION MENU *****

| | | | |
|------------------|----|--------------------|----|
| Alaska | 1 | Central America | 15 |
| Australia | 2 | East Mediterranean | 16 |
| Central Asia | 3 | Indian Ocean | 17 |
| East Coast (USA) | 4 | Northeast (USA) | 18 |
| Eastern Europe | 5 | Northwest (USA) | 19 |
| Hawaii | 6 | Southeast (USA) | 20 |
| Japan | 7 | Southwest (USA) | 21 |
| Midwest (USA) | 8 | | |
| Puerto Rico | 9 | | |
| South America | 10 | | |
| South Pacific | 11 | | |
| Southern Africa | 12 | | |
| West Coast (USA) | 13 | LAT/LON entry | 22 |
| Western Europe | 14 | Select from File | 23 |

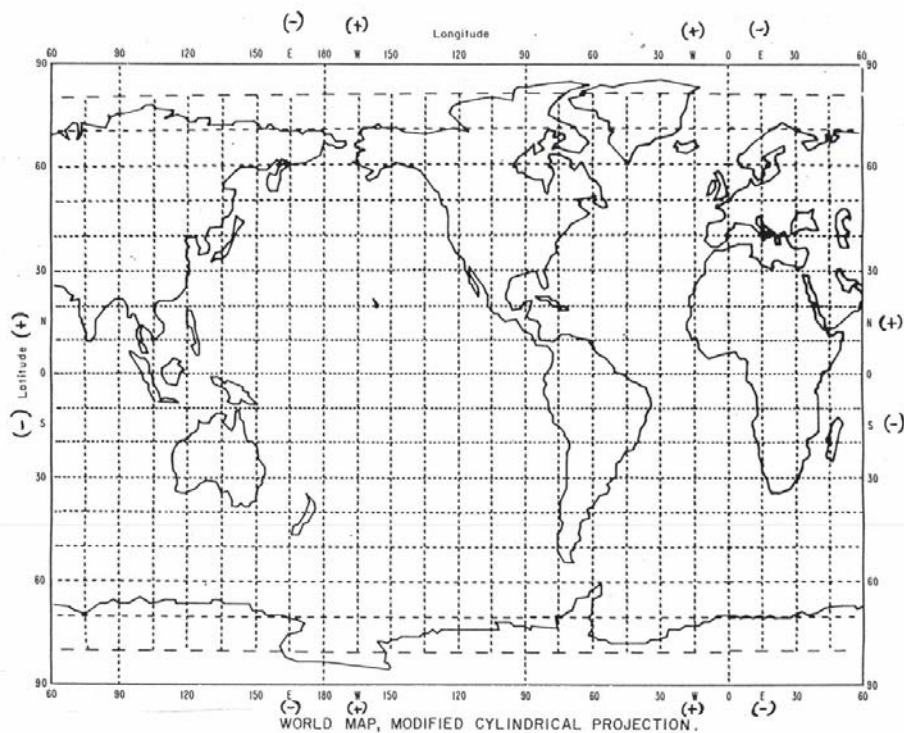
Enter Receiver Selection 1-23 < 23 > 22

Enter Receiver Location (18 Char Max.) Your Qth
Decimal Degrees? Enter Y/N <Y>

Enter RX LAT: DEC DEG or DEG.MIN (N +, S -) <0> 38.45
Enter RX LONG: DEC DEG or DEG.MIN (W +, E -) <0> 111.25

For Short or Long Path enter S or L <S>

World Map Showing Lat/Lon Entry Criteria



Typical Distance/Bearing Table

| IONSOUND DIST/BRNG TABLE FROM: EAST COAST (USA) LAT: 39 LON: 77 | | | | | | | |
|---|--------------------|----------|-----------|------|-------|----------|----------|
| PREFIX | COUNTRY | LATITUDE | LONGITUDE | BRNG | LBRNG | DIST(MI) | DIST(KM) |
| 1A0 | S.M.O. of Malta | 41.9 | -12.48 | 55 | 235 | 4475 | 7202 |
| 1S | Spratly Island | 8.75 | -111.9 | 348 | 168 | 9082 | 14615 |
| 3A | Monaco | 43.7 | -7.4 | 56 | 236 | 4190 | 6743 |
| 3B6 | Agalega | -10.42 | -56.65 | 68 | 248 | 8968 | 14433 |
| 3B7 | St. Brandon | -16.6 | -59.6 | 72 | 252 | 9398 | 15125 |
| 3B8 | Mauritius | -20.2 | -57.5 | 78 | 258 | 9442 | 15195 |
| 3B9 | Rodriguez Is. | -19.72 | -63.43 | 72 | 252 | 9729 | 15657 |
| 3C | Equatorial Guinea | 3.1 | -9.4 | 90 | 270 | 5886 | 9472 |
| 3C0 | Pagalu Island | -1.4 | -5.62 | 96 | 276 | 5879 | 9462 |
| 3D2 | Piji | -17.9 | -178.6 | 264 | 84 | 7744 | 12463 |
| 3D2/R | Rotuma Island | -12 | -176 | 271 | 91 | 7641 | 12298 |
| 3D6 | Swaziland | -26.9 | -31.3 | 102 | 282 | 8295 | 13350 |
| 3V | Tunisia | 35 | -10 | 63 | 243 | 4610 | 7420 |
| 3W | Vietnam | 16 | -106 | 356 | 176 | 8625 | 13881 |
| 3X | Rep. of Guinea | 9.7 | 11.9 | 98 | 278 | 4462 | 7180 |
| 3Y/B | Bouvet Island | -54.4 | -3.28 | 140 | 320 | 7995 | 12867 |
| 3Y/P | Peter Island | -68.83 | 90.58 | 185 | 5 | 7477 | 12033 |
| 4K2 | Franz Josef Land | 81 | -55 | 8 | 188 | 3956 | 6367 |
| 4S | Sri Lanka | 7.4 | -80.4 | 29 | 209 | 8912 | 14342 |
| 4U/ITU | ITU Geneva | 46.2 | -6.15 | 53 | 233 | 4058 | 6531 |
| 4U/UN | United Nations Hq. | 40.75 | 73.97 | 52 | 232 | 201 | 323 |
| 4W | Yemen | 15 | -45 | 57 | 237 | 7152 | 11509 |
| 4X | Israel | 31.7 | -35.1 | 52 | 232 | 5889 | 9478 |
| 5A | Libya | 30 | -15 | 65 | 245 | 5045 | 8119 |
| 5B | Cyprus | 35.1 | -33.5 | 51 | 231 | 5661 | 9111 |
| 5H | Tanzania | -7 | -37 | 80 | 260 | 7800 | 12553 |

Main Menu Followed by Store/Retrieve/Exit Screen

```

Today's Date      ***** IONSOUND HDX TURBO by W1FM *****
09-13-1994      * Copyright (C) 1994 SkyWave Technologies *
*****

(CURRENT VARIABLES)
Tx Location: Northeast (USA)
Lat= 42.35 Lon= 71.05 deg
Tx Location Noise: RES
Rx Location: Your Qth
Lat= 38.45 Lon= 111.25 deg
Rx Location Noise: RURAL
Tx-->Rx Bearing= 276 deg Path= S
Distance= 2111 mi 3397 km
Tx Power= 1 kw
Rx Bandwidth= 3000 Hz
Rx min. S/N Ratio= 10 dB
Tx Ant: (Y)agi-Uda
Rx Ant: 0 dBi (G)ain, Iso.
Sunspot Num= 28 Solar Flux= 85
Layer Ht HF2= 289 km HE= 115 km
Min Elev Ang= 5 E/F Ht Change= N
Min F Hops= 2F F Hop Ang= 15 deg
24 Hr Summary Types= 8 (8 max.)
Last Selected Mon= 9 Next Mon= 9

(SELECTION CHOICES)
Pick Time/Display 24 Hour Summary 0
TX/RX Locations & S/L Path 1
Sunspot/Solar Flux Number (SSN/SFN) 2
Frequency Menu (ION_FREQ.DAT File) 3
Month Menu 4
Variables (Noise/Ant/BW/SNR/Pwr...) 5
Propagation Mode Menu 6
TX Power Level 7
Minimum Elevation Angle Menu 8
Swap TX/RX Locations 9
Color Selection Menu 10
Go to DOS (Type 'EXIT' To Return) 11
E/F Layer Height Menu 12
Tabulate TX/RX Antenna Gains 13
Calculate Antenna Lobes/Nulls 14
Choose New Lat/Lon/Cty File 15
Print Distance/Bearing Table 16
Select 24 Hour Summary Types/Order 17
Store or Load Default Variables/EXIT 18

Enter Choice: <Default=Pick Time/Display: Type 0 or ENTER>

```

Store current variables, load variables, EXIT to DOS, or return to Main Menu

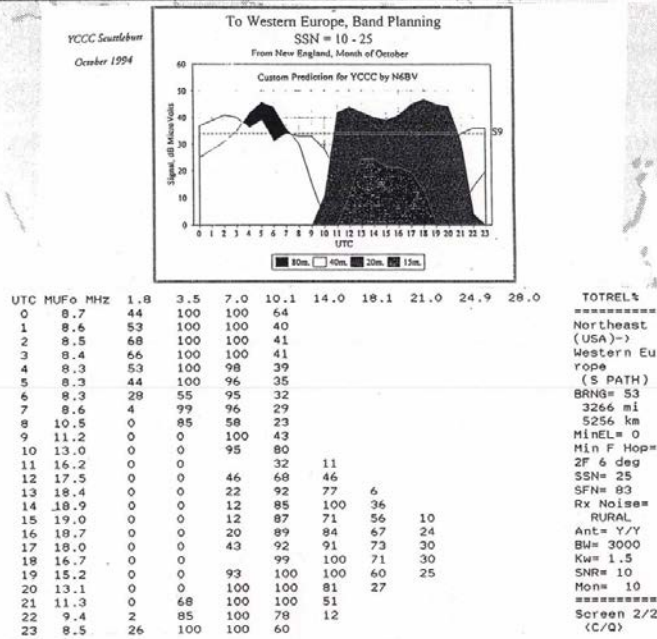
```

Type (S) to Store variables to Default File: (S)
Type (R) to Retrieve (Load) Default File Variables (Restart Program): (R)
Type (E) for EXIT to DOS (Quit Program): (E)
Hit (ENTER) to Return to Main Menu: (ENTER)

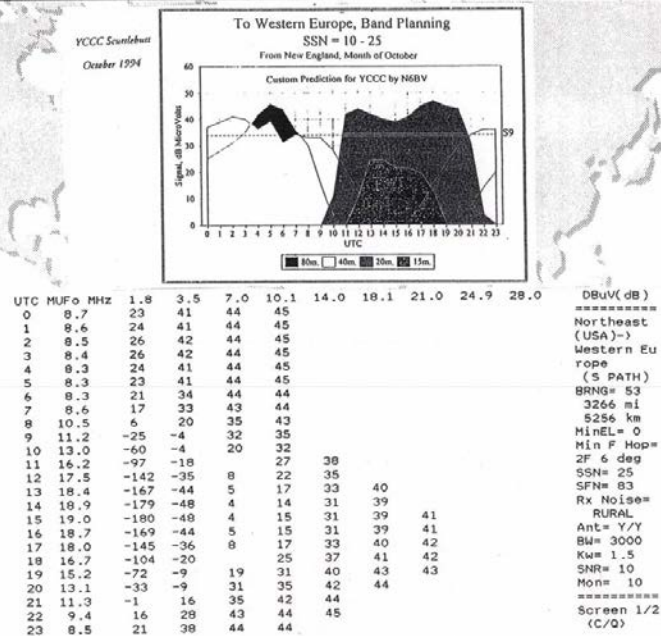
Enter Choice: <Default = Main Menu>

```


CQWW Predictions for Oct 1994



CQWW Predictions for Oct 1994



SKYWAVE PROPAGATION PREDICTION SMOOTHED SUNSPOT NUMBERS EXPECTED FOR 1995-1996

Shown below, from data provided by the National Geophysical Data Center in Boulder, Colorado, is a table of smoothed running sunspot numbers for the present solar cycle along with predicted values of activity expected for 1995-1996.

| | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 |
|------|------|------|------|------|------|------|------|------|------|------|------|
| Jan | | 18 | 58 | 142 | 151 | 148 | 124 | 71 | 37 | 24 | 14* |
| Feb | | 20 | 65 | 145 | 151 | 148 | 116 | 69 | 35 | 23 | 13* |
| Mar | | 22 | 71 | 150 | 152 | 147 | 108 | 67 | 34 | 22 | 13* |
| Apr | | 24 | 78 | 154 | 149 | 146 | 103 | 64 | 34 | 21* | 12* |
| May | | 26 | 84 | 157 | 147 | 146 | 100 | 60 | 33 | 20* | 12* |
| June | | 28 | 94 | 158 | 144 | 145 | 97 | 56 | 31 | 19* | 11* |
| July | | 31 | 104 | 159 | 141 | 146 | 91 | 55 | 29 | 19* | 11* |
| Aug | | 35 | 114 | 158 | 141 | 147 | 84 | 52 | 27 | 18* | 10* |
| Sept | 12 | 39 | 121 | 157 | 142 | 145 | 80 | 49 | 27 | 18* | 9* |
| Oct | 13 | 44 | 125 | 157 | 142 | 142 | 76 | 45 | 27 | 17* | 9* |
| Nov | 15 | 47 | 130 | 158 | 142 | 138 | 74 | 41 | 26 | 16* | 8* |
| Dec | 16 | 51 | 138 | 154 | 144 | 132 | 73 | 39 | 26 | 15* | 8* |

Smoothed Sunspot Numbers for Cycle 22 and Forecasts for 1995-96.
(Predicted Values shown with an *)

Propagation Indices During 3Y0PI Peter Island DXpedition to Antarctica

| geomagnetic activity | | Typical K indices | |
|----------------------|------------------|-------------------|------------------------------|
| Category | Range of A index | Range of A index | Typical K indices |
| Quiet | 0-7 | 0-7 | Usually no Ks greater than 2 |
| Unsettled | 8-15 | 8-15 | Usually no Ks greater than 3 |
| Active | 16-29 | 16-29 | A few Ks of 4 |
| Minor storm | 30-49 | 30-49 | Ks mostly 4 and 5 |
| Major storm | 50-99 | 50-99 | Some Ks of 6 or greater |
| Severe storm | 100-400 | 100-400 | Some Ks of 7 or greater |

| Date (All 1994) | Solar Flux | A-Index | K-Index |
|-----------------|------------|---------|---------|
| Feb 1 | 98 | 5 | 1-2 |
| Feb 2 | 94 | 6 | 3-4 |
| Feb 3 | 96 | 12 | 1-3 |
| Feb 4 | 98 | 8 | 2-3 |
| Feb 5 | 95 | 8 | 2-4 |
| Feb 6 | 93 | 20 | 4-6 |
| Feb 7 | 95 | 46 | 4-5 |
| Feb 8 | 96 | 49 | 5-6 |
| Feb 9 | 95 | 50 | 5 |
| Feb 10 | 101 | 34 | 4-5 |
| Feb 11 | 94 | 29 | 4-5 |
| Feb 12 | 93 | 36 | 4-5 |
| Feb 13 | 98 | 29 | 3-5 |
| Feb 14 | 98 | 24 | 3-5 |
| Feb 15 | 101 | 23 | 3-4 |
| Feb 16 | 104 | 19 | 3-4 |
| Feb 17 | 105 | 14 | 2-3 |
| Feb 18 | 106 | 8 | 1-3 |

Source: Robert W. Schmieder, KK6EK, "3Y0PI Peter I Island Antarctica", 1994

3Y0PI BAND OPENING TIMES OBSERVED BY WA0PUJ (MINN.)

| Band | m | 160 | 80 | 40 | 30 | 20 | 17 | 15 | 12 | 10 m | TOTREL% |
|--------------|------|-----|-----|------|------|------|------|------|------|------|------------|
| UTC MUfo MHz | 1.8 | 3.5 | 7.0 | 10.1 | 14.0 | 18.1 | 21.0 | 24.9 | 28.0 | | ===== |
| 0 | 18.4 | | | 7 | 98 | 49 | 12 | | | | Minnesota |
| 1 | 18.2 | | | 92 | 99 | 45 | | | | | -) |
| 2 | 19.1 | | 0 | 99 | 77 | 11 | | | | | Peter Isla |
| 3 | 18.4 | | 0 | 99 | 71 | 6 | | | | | nd |
| 4 | 17.2 | | 77 | 99 | 72 | 12 | | | | | (S PATH) |
| 5 | 16.1 | | 76 | 100 | 77 | 22 | | | | | BRNG= 179 |
| 6 | 14.8 | | 64 | 100 | 75 | 21 | | | | | 7860 mi |
| 7 | 13.7 | | 74 | 100 | 80 | 28 | | | | | 12649 km |
| 8 | 12.6 | | 80 | 99 | 81 | 26 | | | | | MinEL= 0 |
| 9 | 11.7 | | 1 | 99 | 81 | 22 | | | | | Min F Hop= |
| 10 | 10.8 | | 0 | 99 | 71 | 3 | | | | | 4F 3 deg |
| 11 | 10.1 | | | 95 | 52 | | | | | | SSN= 45 |
| 12 | 14.6 | | | 0 | 28 | 17 | | | | | SFN= 98 |
| 13 | 14.9 | | | | | 46 | | | | | Rx Noise= |
| 14 | 16.0 | | | | | 0 | 58 | 23 | | | RURAL |
| 15 | 16.9 | | | | | 0 | 67 | 49 | | | Ant= Y/Y |
| 16 | 17.7 | | | | | 0 | 23 | 59 | 10 | | BW= 3000 |
| 17 | 18.0 | | | | | | 8 | 60 | 14 | | Kw= 1.5 |
| 18 | 18.1 | | | | | | 4 | 61 | 17 | | SNR= 10 |
| 19 | 18.2 | | | | | | 6 | 63 | 19 | | Mon= 2 |
| 20 | 18.3 | | | | | 0 | 19 | 66 | 21 | | ===== |
| 21 | 18.3 | | | | | 0 | 62 | 69 | 23 | | Screen 2/2 |
| 22 | 18.3 | | | | | 0 | 89 | 71 | 25 | | (C/Q) |
| 23 | 18.4 | | | | | 46 | 97 | 68 | 26 | | |

WA0PUJ

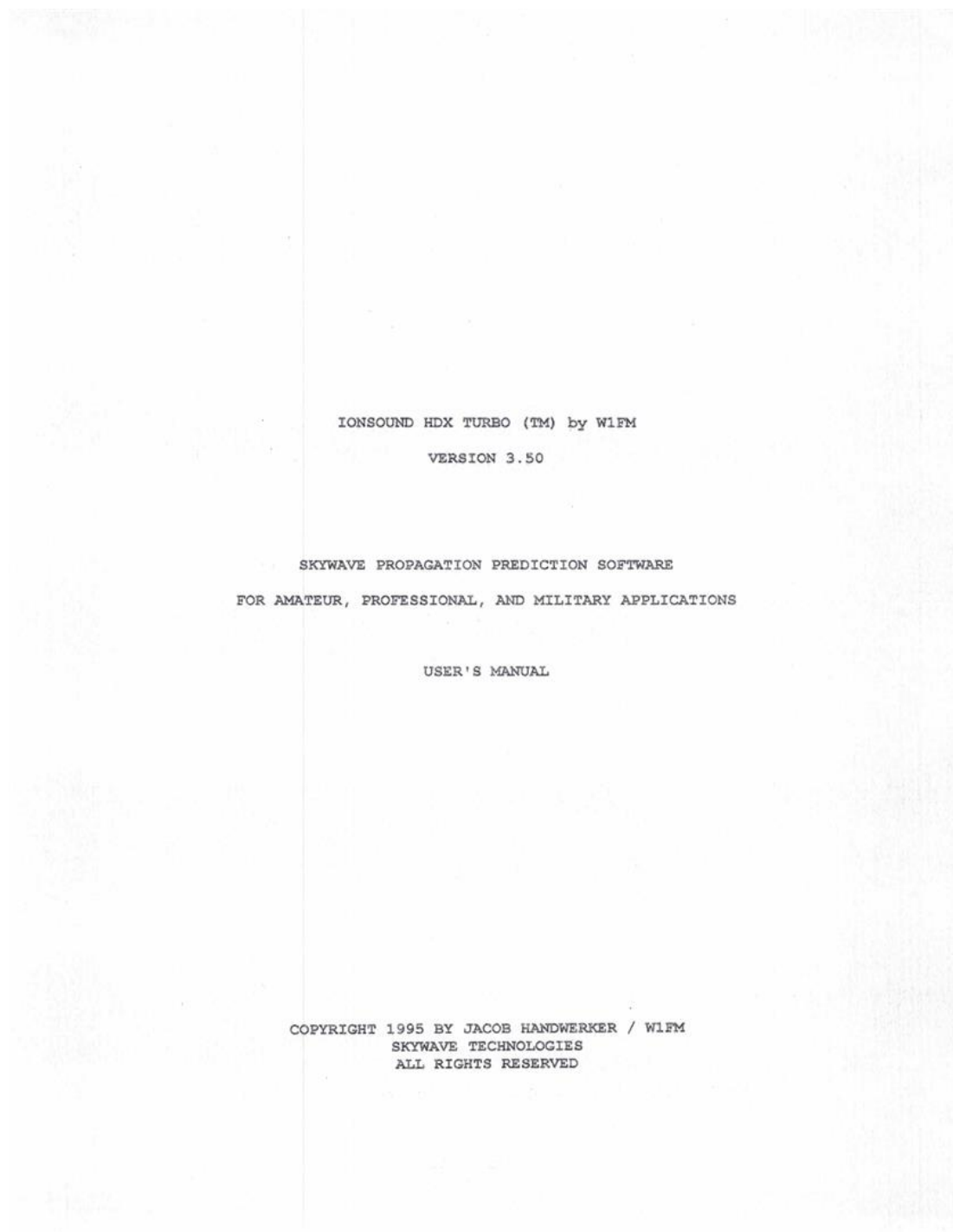
3Y0PI BAND OPENING TIMES OBSERVED BY WA0PUJ (MINN.)

| Band | Open Times |
|-------|------------|
| 160 m | 0400-0430Z |

SS/FN= 45 / 98 HF2(KM)= 297 UFS(DBWM,DBUVM)= -122 , 23 Noise=RURAL VER=HDX3.2
TX LAT= 45 TX Long= 93 RX LAT=-68.84 RX Long= 90.58 Dist(mi)= 7860
Minnesota to Peter Island (S PATH) Min F Mode= 4 Elev Ang 3
T= 4.15 UT Mon= 2 FB BRNG= 179 / 359 Dist(km)= 12649 Mode= 5 HE(km)= 115
BW(Hz)= 3000 SNR Req= 10 TX PWR(KW)= 1.5 MinEle= 0 Date: 09-23-1994
FREQ HOP NPW SVM SPW S/N %S %P %T ELE MSDEL MUfo MUFv GAIN

| | | | | | | | | | | | | | |
|-------|-----|------|-----|------|-----|-----|-----|----|----|-------|-------|------|---------|
| 1.80 | 7E | -123 | -17 | -154 | -31 | 0 | 100 | 0 | 1 | 42.79 | 4.07 | 0.77 | 9.75YY |
| | 8E | -123 | -27 | -164 | -40 | 0 | 100 | 0 | 3 | 42.88 | 4.00 | 0.78 | 11.63YY |
| | 9E | -123 | -37 | -174 | -51 | 0 | 100 | 0 | 5 | 43.02 | 3.82 | 0.80 | 14.00YY |
| 3.50 | 3FE | -133 | 19 | -118 | 15 | 80 | 100 | 80 | 1 | 43.44 | 4.07 | 0.77 | 9.75YY |
| | 4FE | -133 | 15 | -122 | 11 | 56 | 76 | 43 | 5 | 43.86 | 3.82 | 0.80 | 14.00YY |
| | 6F | -133 | 12 | -125 | 8 | 33 | 100 | 33 | 11 | 44.70 | 14.22 | 5.34 | 18.66YY |
| | 7F | -133 | 6 | -131 | 2 | 2 | 100 | 2 | 14 | 45.28 | 12.92 | 5.30 | 19.92YY |
| | 8F | -133 | 0 | -137 | -4 | 0 | 100 | 0 | 17 | 45.93 | 11.78 | 5.27 | 20.38YY |
| 7.00 | 4F | -138 | 30 | -107 | 31 | 99 | 100 | 99 | 3 | 43.75 | 16.94 | 5.45 | 11.63YY |
| | 5F | -138 | 26 | -111 | 27 | 99 | 100 | 99 | 7 | 44.19 | 15.64 | 5.39 | 16.02YY |
| | 6F | -138 | 21 | -116 | 22 | 96 | 92 | 88 | 11 | 44.70 | 14.22 | 5.34 | 18.66YY |
| | 7F | -138 | 15 | -122 | 16 | 83 | 77 | 64 | 14 | 45.28 | 12.92 | 5.30 | 19.92YY |
| | 8F | -138 | 8 | -129 | 9 | 40 | 61 | 24 | 17 | 45.93 | 11.78 | 5.27 | 20.38YY |
| 10.10 | 4F | -139 | 31 | -106 | 34 | 100 | 73 | 73 | 3 | 43.75 | 16.94 | 5.45 | 11.63YY |
| | 5F | -139 | 27 | -110 | 30 | 99 | 54 | 54 | 7 | 44.19 | 15.64 | 5.39 | 16.02YY |
| | 6F | -139 | 22 | -115 | 24 | 98 | 32 | 32 | 11 | 44.70 | 14.22 | 5.34 | 18.66YY |
| | 7F | -139 | 16 | -121 | 18 | 90 | 10 | 9 | 14 | 45.28 | 12.92 | 5.30 | 19.92YY |
| 14.00 | 4F | -138 | 32 | -105 | 33 | 100 | 14 | 14 | 3 | 43.75 | 16.94 | 5.45 | 11.63YY |

5. IONSOUND HDX TURBO S/W MANUAL



The author has made every effort to ensure that this program is correct and accurate. However, no expressed or implied warranty or guarantee of any kind with respect to its accuracy or effectiveness is made. The author will therefore not be liable for incidental or otherwise consequential damages, either direct or indirect, in connection with furnishing of, or the performance of, or as a result of the use of this program. The author does not warrant that the functions of the software will meet your needs or that it will operate error-free and uninterrupted.

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INTRODUCTION

1. Ionospheric Propagation Background

Radio waves can be classified according to various types of propagation. These propagation types are ionospheric, tropospheric, or ground waves. Ionospheric, also known as skywave, propagation provides the major portion of the overall radiation that leaves an antenna at some elevation angle above the horizontal plane. Much of the short and long-distance communications below 30 MHz depends on the bending or refraction of the transmitted wave in the earth's ionosphere which are regions of ionization caused by the sun's ultraviolet radiation and lying about 60 to 200 miles above the earth's surface.

The useful regions of ionization are the E layer (at about 70 miles in height for maximum ionization) and the F layer (lying at about 175 miles in height at night). During the daylight hours, the F layer splits into two distinguishable parts: F1 (lying at a height of about 140 miles) and F2 (lying at a height of about 200 miles). After sunset the F1 and F2 layers recombine again into a single F layer. During daylight, a lower layer of ionization known as the D layer exists in proportion to the sun's height, peaking at local noon and largely dissipating after sunset. This lower layer primarily acts to absorb energy in the low end of the High Frequency (HF) band. The F layer ionization regions are primarily responsible for long distance communications, sometimes in conjunction with the E layer in a variety of mixed propagation modes.

Vertical incidence ionospheric sounding devices are used to determine the virtual height of an ionospheric layer at various frequencies by beaming energy upward and measuring the time delay required for the round trip. The critical frequency for a vertical incidence sounder is the maximum frequency above which no energy is returned to earth for a given layer. An ionogram is a graphic representation of such sounding and usually depicts the height of the layer (or the time delay) as a function of the sounding frequency, along with the intensity of the return signal. An oblique sounding device may require the cooperation of a corresponding receiving device at a distant point in order to depict received energy which has been transmitted at incidence angles less than 90 degrees in elevation; it may also make use of backscatter techniques to assess the propagation path. Devices such as these can then be used to assess (in real time) the propagation path frequencies which can be supported, up to and including the Maximum Usable Frequency (MUF).

As an adjunct to this Users Manual, it is recommended that other sources of information concerning HF propagation prediction and related antenna theory be consulted since this operating manual is not meant to be a comprehensive tutorial on the theoretical aspects of these subjects. A bibliography of several of these source materials is shown at the end of this manual.

2. IONSOUND HDX TURBO Overview

IONSOUND HDX TURBO is a very sophisticated ionospheric propagation prediction program for frequencies between 1.8 MHz and 30 MHz. IONSOUND HDX

TURBO is a member of the IONSOUND family of programs which have been evolving for a number of years. Geographical regions corresponding to those shown in ARRL's QST magazine "How's DX?" column can primarily be chosen from the TX and RX location menus along with several others not found in QST.

IONSOUND HDX TURBO has been designed with user friendliness in mind and is entirely menu-driven, with prompting for various user inputs to the program. It should be emphasized that a comprehensive understanding of propagation phenomena and the technical terms associated with the scientific forecasting of propagation is helpful, but not necessary, to become skilled in the use of IONSOUND HDX TURBO. The goal of the program is to produce an easy-to-interpret tabular prediction of radio frequency (RF) link performance between two locations on the earth's surface.

Technical jargon and output detail has been minimized to essential elements in the interest of simplicity, without a sacrifice in overall performance of the program or its presentation display capabilities. To simplify matters, default inputs have been provided. An explanation of the use of these menus and screens will be provided in this manual, but the program should be largely self explanatory. Once the operator has customized IONSOUND HDX TURBO to suit his/her particular needs, the information is saved to disk as a set of defaults. When the program is started, the operator need only hit the <Enter> key several times to accept the custom defaults and then make a propagation prediction.

3. General Requirements

IONSOUND HDX TURBO is designed for use with IBM or IBM-compatible personal computers. The program operates with or without an 8087, 80287, or 80387 math coprocessor. It will automatically take advantage of the coprocessor if it finds it. However, if at all possible, a coprocessor should be utilized, due to the mathematically intensive nature of the calculations performed in the propagation prediction process. Processing times can become lengthy without a coprocessor; in fact, a coprocessor will usually speed up operation by a factor of 15 or even more. Note that the 80486DX and the Pentium processors have the coprocessor built-in, while 80486SX versions do not. If you intend to do antenna modeling and propagation predictions, an investment in a numeric coprocessor is worthwhile.

A personal computer with 640 kilobytes of RAM is desirable, along with DOS version 2.11 or greater. For hard copy printout, a printer supporting IBM Graphics is recommended.

4. Printing IONSOUND HDX TURBO Operator Manual

You may print out this Operators Manual. First, make sure your printer is on-line, then type the following:

```
TYPE ION_HDXT.DOC > PRN <Enter> or PRINTDOC <Enter>
```

5. Starting IONSOUND HDX TURBO

To start IONSOUND HDX TURBO type the following:

```
ION_HDXT <Enter>
```

For convenience use the batch file:

```
ION <Enter>
```

Following the start-up of IONSOUND HDX TURBO, the program will prompt the user, in a step-by-step fashion, with several screens prompting user responses.

6. General, Menus and Screens

All entries, such as for YES/NO (Y/N) selections, can be made in either lower case or upper case. Default conditions for most of the menus and screens are shown by a notation such as:

```
<DEFAULT= #> or <Y> or <N> or <C/Q>.
```

Default= # is the option number which will result if the enter key is pressed instead of actually inputting a number value. Likewise, Y or N defaults indicate YES or NO, respectively.

When a <C/Q> option is encountered, the default is C (continue); typing Q indicates "Quit" back to the Main Menu.

7. Display Color Selection

There are eight possible color combinations for the display text and background. The program comes up in black and white unless you choose another combination. Caution: a background color other than black will cause a black/white monitor to be unreadable!

8. Transmit and Receive Location

The selection menu for transmit (TX) and receive (RX) locations each consist of up to 24 choices. Choices 1-14 allow selection of predefined locations corresponding to those shown in QST magazine's "How's DX?" column, published monthly by the American Radio Relay League (ARRL). Choices 15 through 21 are for additional predefined locations not covered in "How's DX?" Choice 22 allows for input of latitude and longitude for any user-specified location on Earth. Choice 23 allows selection of predefined locations found in the file 'ION_CTY.DAT' or a file of your own choosing. Choice 24 allows the selection of the prior location in choice 22 or 23.

[Note: When inputting a user-specified location in Choice 22, the Degree.Decimal format allows decimal fraction degrees (i.e., 39.25 represents 39 + 25/100 degrees); the Degrees.Minutes format allows degrees and minutes (i.e., 39.25 represents 39 degrees + 25 minutes) as an entry.]

These selections make it easy to compute IONSOUND HDX TURBO predictions for comparison with the Highest Possible Frequency (HPF), Maximum Usable Frequency (MUF), and the Frequency of Optimum Transmission (FOT) predictions derived from U.S. Department of Commerce, National Telecommunications and Information Administration (NTIA) IONCAP program as found in QST.

[Note: Although the "How's DX?" list in QST is limited, it can be successfully used to predict propagation performance between many other locations which are near those shown in Table 1.]

Table 1
Expanded List of QST "How's DX?" TX/RX Locations

| Choice | Location | Latitude | Longitude | Nearest City |
|--------|--------------------|----------|-----------|-----------------------|
| 1 | Alaska | 61.00 | 150.00 | Anchorage |
| 2 | Australia | -33.87 | -151.22 | Sydney |
| 3 | Central Asia | 28.50 | -77.50 | New Delhi, India |
| 4 | U.S. East Coast | 39.00 | 77.00 | Washington, DC |
| 5 | Eastern Europe | 50.50 | -30.50 | Kiev, Ukraine |
| 6 | Hawaii | 21.33 | 157.80 | Honolulu |
| 7 | Japan | 35.75 | -139.80 | Tokyo |
| 8 | U.S. Midwest | 39.00 | 95.00 | Kansas City, KS |
| 9 | Caribbean | 18.50 | 66.00 | San Juan, Puerto Rico |
| 10 | South America | -25.00 | 57.50 | Asuncion, Paraguay |
| 11 | South Pacific | -14.33 | 170.70 | Pago Pago, Am. Samoa |
| 12 | Southern Africa | -15.50 | -28.00 | Lusaka, Zambia |
| 13 | U.S. West Coast | 38.00 | 122.00 | San Francisco, CA |
| 14 | Western Europe | 51.50 | 0.20 | London, England |
| 15 | Central America | 15.00 | 90.00 | Guatemala City |
| 16 | East Mediterranean | 31.50 | -35.00 | Jerusalem, Israel |
| 17 | Indian Ocean | -6.50 | -107.00 | Djakarta, Indonesia |
| 18 | U.S. Northeast | 42.35 | 71.05 | Boston, MA |
| 19 | U.S. Northwest | 47.50 | 122.50 | Seattle, WA |
| 20 | U.S. Southeast | 30.25 | 81.50 | Jacksonville, FL |
| 21 | U.S. Southwest | 33.50 | 112.00 | Phoenix, AZ |

Latitude and longitude values are given in decimal degree format. Positive values of latitude (+) are north of the Equator; negative values (-) of latitude are south of the Equator. Positive values of longitude (+) are west of Greenwich, UK; negative values of longitude (-) are east of Greenwich.

See QST Magazine, December 1990, Technical Correspondence, Pages 58-59, "Propagation Predictions and Personal Computers" for a discussion of how these locations are used in conjunction with sunspot numbers and minimum elevation angle requirements to derive IONCAP predictions for QST Magazine's "How's DX?" column.

9. Short/Long Path Selection

Selection of Short <S> or Long <L> path gives an opportunity to choose either the shortest or the longest great circle path from the transmitting to the receiving location. The default for this selection is the short or S path. IONSOUND HDX TURBO is designed to support only direct paths; skew paths that are not on great circles are not supported. Following the selection of either short or long path, the distance in kilometers, statute miles, and nautical miles from the transmitter to the receiver is provided by the program.

Also shown is the front/back (F/B) bearing in degrees (eg, 315 / 135). The front value is the bearing (or heading) direction from the transmitter toward the receiver. The positive value of bearing indicates the clockwise number of degrees offset heading from True North (0 degrees) which a radiated signal will follow on a great circle path from transmitter location to receiver location. The back value is the direction opposite (or 180 degrees away) from the transmitter-to-receiver direction.

10. Receiver Noise

Receiver noise code can be independently selected for the transmitter (TX) location and the receiver (RX) location. Since link predictions are always made for the path from the transmitter to the receiver, it makes a difference in predicted performance when the two locations are 'swapped' and the TX receiver noise code is not the same as the RX receiver noise code. Swapping of the TX and RX locations can easily be done from the Main Menu. When this 'SWAP' function is exercised, the respective noise codes are interchanged for prediction purposes, along with the latitudes, longitudes and location descriptions. A choice of three receiver noise codes can be inputted by the user. These choices are CITY, RESIDENTIAL, or RURAL noise. This selection is used in determining the received signal-to-noise ratio.

The selection of receiver noise code should be made by considering the geographic location of the TX location receiver and the RX location receiver in relation to city, residential or rural surroundings. Choosing city noise results in more noise at the receiver than residential noise. Likewise, residential noise is less than city noise but more than rural noise. The received noise power density, also varies as a function of frequency at the receive end of the RF link. Lower frequencies have greater ambient noise background levels than higher frequencies. The actual receive noise power (expressed in Watts) depends upon the receiver bandwidth. The default for choosing a TX or RX location receiver noise code is residential noise.

11. Antenna/Gain Selection

The Transmit and Receive Antenna Selection Menu allows the operator to choose the antenna for both the transmitter and receiver locations. The selections offered for transmit/receive antennas represent typical candidate configurations for predicting propagation performance. Each is represented by a mathematical model whose gain varies as a function of the elevation angle. Please note that the overall response of each antenna selection is a generic, theoretical response, since real-world effects for an individual location (such as local terrain, other antennas, or nearby power lines) cannot be included.

Table 2

TX/RX Antenna Gains vs. Elevation Angle

| Takeoff Angle (deg) | Dipole Ant D (dB) | Vertical Ant V (dB) | Yagi Ant Y (dB) | Log/Rhom Ant L (dB) | Curtain Ant C (dB) | Isotropic Antennas G I (dB) (dB) | |
|------------------------|-------------------------|---------------------------|-----------------------|---------------------------|--------------------------|--|---|
| 1 | -9.37 | -3.15 | 4.89 | -4.28 | 11.72 | -40 to +40 | 0 |
| 5 | -2.40 | -1.21 | 6.82 | 2.68 | 18.68 | -40 to +40 | 0 |
| 10 | 0.54 | 1.11 | 9.14 | 5.57 | 21.57 | -40 to +40 | 0 |
| 15 | 2.19 | 2.06 | 10.10 | 7.13 | 23.13 | -40 to +40 | 0 |
| 20 | 3.28 | 2.16 | 10.19 | 8.11 | 24.11 | -40 to +40 | 0 |
| 25 | 4.04 | 1.90 | 9.93 | 8.71 | 24.71 | -40 to +40 | 0 |
| 30 | 4.58 | 1.51 | 9.54 | 9.05 | 25.05 | -40 to +40 | 0 |
| 35 | 4.93 | 1.02 | 9.06 | 9.16 | 25.16 | -40 to +40 | 0 |
| 40 | 5.13 | 0.44 | 8.48 | 9.07 | 25.07 | -40 to +40 | 0 |
| 45 | 5.20 | -0.25 | 7.78 | 8.79 | 24.79 | -40 to +40 | 0 |
| 50 | 5.13 | -1.08 | 6.95 | 8.31 | 24.31 | -40 to +40 | 0 |
| 55 | 4.93 | -2.07 | 5.96 | 7.62 | 23.61 | -40 to +40 | 0 |
| 60 | 4.58 | -3.26 | 4.77 | 6.66 | 22.66 | -40 to +40 | 0 |
| 65 | 4.04 | -4.72 | 3.32 | 5.40 | 21.40 | -40 to +40 | 0 |
| 70 | 3.28 | -6.50 | 1.53 | 3.72 | 19.72 | -40 to +40 | 0 |
| 75 | 2.19 | -8.62 | -0.59 | 1.41 | 17.41 | -40 to +40 | 0 |
| 80 | 0.54 | -11.33 | -3.29 | -1.97 | 14.03 | -40 to +40 | 0 |
| 85 | -2.40 | -16.41 | -8.37 | -7.91 | 8.09 | -40 to +40 | 0 |
| 89 | -9.37 | -29.99 | -21.96 | -21.86 | -5.86 | -40 to +40 | 0 |

Notes on IONSOUND HDX TURBO Antennas:

| | |
|------------------|--|
| D=Dipole | Horizontal or Vertical Dipole, approx. 3/8 wave high |
| V=Vertical | Vertical Monopole, ground-mounted |
| Y=Yagi-Uda | Yagi-Uda Array, approximately 3/4 wave high |
| L=Log/Rhom | Log Periodic or Rhombic Array, approx. 1/2 wave high |
| C=Curtain | Curtain Array, wide elevation takeoff angle coverage |
| G=Isotropic Gain | -40 to +40 dBi, constant gain at all takeoff angles |
| I=Isotropic | 0 dBi, constant gain at all takeoff angles |

The Yagi-Uda (Y) in IONSOUND HDX TURBO emulates a Yagi mounted approximately at 3/4 wavelength above ground. It has a peak gain of +10 dBi (that is, referenced to an isotropic radiator in free space) at 15 degrees

and has essentially no output at very high elevation angles. Most amateurs select the IONSOUND HDX TURBO Yagi model for predictions in the HF bands above 14 MHz, or even 7 MHz if they have a 40-meter Yagi. [Note: Many use the Yagi even for 3.5 MHz just to see how the predictions come out for those lucky hams who do have 80-meter Yagis!]

The Vertical Monopole (V) selection emulates the behavior of a ground-mounted vertical antenna over real earth ground. It has a peak gain of 2 dBi at an elevation angle of 30 degrees, with essentially no output near 0 degrees or at very high elevation angles. The upward-tilted elevation pattern for the vertical monopole is broad and usable for low/medium launch-angle coverage.

The Horizontal or Vertical Dipole (D) selection emulates a dipole mounted approximately $3/8$ wavelengths over ground, with a peak gain of +5 dBi at 45 degrees elevation. The upward-tilted elevation pattern is broad and usable for all-around elevation coverage. Many amateurs use this IONSOUND HDX TURBO dipole selection for the lower HF bands, mostly on 1.8 and 3.5 MHz.

The variable gain Log-Periodic and Rhombic (L) selection has been weighted to provide gain ranging from +7 dBi at 1.8 MHz to +16 dBi gain at 30 MHz. The maximum gain is maintained at an angle of approximately 30 degrees above the horizon, again with essentially no output near 0 degrees or at very high elevation angles. This pattern emulates a very large multi-band horizontal Log-Periodic or a terminated Rhombic antenna. At each frequency the height of the antenna is approximately one-half wavelength above ground.

The variable gain Curtain (C) Array antenna selection has been weighted to provide a variable peak gain over an isotropic radiator ranging from approximately +23 dBi at 1.8 MHz to +28 dBi gain at 30 MHz. The maximum gain is maintained at an angle of approximately 30 degrees above the horizon. Of course, most 160-meter operators have a hard time achieving any gain at 1.8 MHz, so this curtain antenna provides an upper bound on what is imaginable for antenna gain on all frequencies. In other words, if the band doesn't open up for this antenna, nothing will make HF communication possible!

Selection of 'Choose Your Own Gain' (G) provides an opportunity to pick an Isotropic Gain antenna between -40 to +40 dBi. An isotropic radiator is an ideal antenna that radiates uniformly in all directions. The weighting function for this choice provides the same gain at all elevation angles, allowing the program to pick out all possible propagation modes on a theoretical basis, with virtually no limitations due to the use of real antennas over real ground. Most of the time the lowest possible elevation angles are predicted when a high-gain isotropic antenna is used, even on the low frequencies.

The selection of any particular antenna or isotropic gain value will cause the program to utilize this gain value for all frequencies. If a particular antenna is suitable at some frequencies but not at others, the program should be rerun with the correct antenna selection if more accurate or realistic results are desired.

[Note: The user can use selection 14 from the Main Menu to show the influence of electrical height on an antenna's major lobe and null

characteristics and the resulting single hop E and F layer distances.]

12. Receiver Bandwidth

The selection of a receiver bandwidth is used to determine the noise power used into the calculation of signal-to-noise (S/N) ratio. This entry must be greater than 0 Hz and should be consistent with the type of communications activity being predicted. A typical value for single sideband (SSB) voice communication is 3000 Hz. For Morse code (CW) operation, a value of 500 Hz is typical. For AM, a value of 6000 Hz is adequate. A default value of 3000 Hz is selected if the <Enter> key is hit without a numeric value entered.

For direct comparison with IONCAP S/N predictions, a normalized 1 Hz bandwidth can be used, since that is what IONCAP uses internally.

13. Required S/N Ratio

The selection of a required Signal-to-Noise (S/N) ratio determines the threshold level of signal quality on which the propagation prediction is based. Typically, 10 dB or more S/N ratio is required for minimum voice communications capabilities in a 3 KHz (typical) bandwidth. In case of severe interference, or fading conditions due to multipath ionospheric effects, this value should be made higher. The required S/N ratio input by the operator is used to determine the %S availability of the link (i.e., S/N Availability). As the required minimum S/N value is raised, the RF link is less likely to support the requirement.

Therefore, you should usually choose the absolute minimum S/N that is needed in order to assess the %S (S/N Availability percentage) and the %T (Total Reliability percentage) of the link. The %P (Path Availability percentage) of the link is independent of the minimum required S/N ratio, indicating instead that the path is open for some level of communication.

14. Transmitter Power

The selection of transmitter power represents the amount of power (in kilowatts) delivered to the selected antenna. For example, to designate 100 watts delivered to the antenna, the entry would be made as 0.1 (i.e., 1/10 kilowatt). Transmitter power must be entered as a value greater than 0. Increasing or decreasing the amount of power has a direct bearing on the received S/N ratio and thus affects %N S/N Availability and %T Total Link Reliability. Thus, a 10 dB increase in signal power results in a 10 dB increase in received S/N ratio. The default selection value is 1 kW.

[Note: Feedline and other losses to the antenna should be considered in the selection of transmitter power, since this value represents the amount of power actually delivered to a matched antenna.]

15. Sunspot Number (SSN) or Solar Flux Number (SFN)

The level of solar activity influences ionospheric propagation. IONSOUND HDX TURBO accepts either SSN (Smoothed Sunspot Number) or SFN (Solar Flux Number) values. The program uses these values for computation of D, E, and F layer absorption effects on transmitted signals in the ionosphere. The SSN is based upon a statistically smoothed set of observations of sunspots and clusters of sunspots. The SSN can be obtained

from publications such as QST (published by the ARRL) or from CQ Magazine. The SFN is based upon a 2800 MHz measurement of solar noise and is broadcast hourly on broadcast services such as WWV. Solar flux data is also available on most packet clusters. If real-time indications of solar activity are utilized, either SSN or SFN, running-averages should be kept and used as input to IONSOUND HDX TURBO. Robust predictions may involve 5, 10, 15 or 30 day running averages, while longer-term averages may be 6 months or longer.

Prior to actual entry of SSN or SFN, a choice is presented for selection of using either SSN or SFN. To pick use of SSN an S should be entered; to pick use of SFN, an F should be entered. The default for this selection is use of the SSN.

For SSN input, a value greater than 0 must be entered. For SFN input, a value greater than or equal to 63.75. If SSN is entered, IONSOUND HDX TURBO computes the equivalent SFN. Likewise, it computes and displays SSN if SFN is used. The default selection value for SSN is 0.

[Note: Sunspot data can also be obtained from the "Solar Indices Bulletin", National Geophysical Data Center, Boulder, Colorado. See Appendix for a discussion of National Bureau of Standards (NBS) forecasts and prediction availability via radio broadcasts and on-line telephone/modem services.]

[CAUTION: Following SSN/SFN entry, any manually entered changes to the F-layer height or the E-layer height should be carefully considered since program derived values will be overridden. In general, knowledge of vertical height from ionospheric soundings is useful and may be used if available.]

16. Minimum Elevation Angle

The operator may enter a minimum elevation angle. This is useful if the horizon towards the desired target location is blocked by hills or other obstructions. Selecting a higher minimum angle precludes unrealistic low-order modes from being used in the computations.

Following the elevation angle selection, the program computes the lowest-order F layer propagation mode (showing the number of hops), the calculated takeoff angle, and the unabsorbed isotropic receiver power density and field strength available at the distant receiver at the oblique critical frequency for this mode. Additional elevation angles may be tried if desired.

With each minimum elevation angle the program finds the corresponding F layer hops, power density and field strength. Finally, after you have decided on a minimum elevation angle (or choose 0 degrees by default), the program will proceed.

17. Choosing Prediction Frequencies

The menu for selection of prediction frequencies presents a variety of choices. In all cases, the entry of any frequency is a MHz value.

Selection 1 allows entry of up to nine separate frequencies in the 1.8 MHz to 30 MHz range. The prediction order will be in the same sequence as

the frequencies are entered.

Selection 2 allows entry of a range of frequencies defined by the lowest frequency (greater than or equal to 1.8 MHz), a frequency increment (greater than 0), and a highest frequency (less than or equal to 30 MHz). A number must be entered for each prompt, or the program will simply cycle back to the first prompt. If the frequency increment chosen is too small, resulting in more than nine frequencies, the upper frequency limit will be truncated in order to limit the total number of frequencies to nine.

If selection 2 is chosen and a previously defined range of frequencies already exists, the program will prompt the user whether to keep this previous range of frequencies by typing Y or N. The default for this choice is <Y> so that the program can continue with this previously defined range by simply hitting the <Enter> key.

Selection 3 allows a predefined subset of all 9 HF amateur band frequencies (based on U.S.A. Allocations) currently available in the 1.8-30 MHz range. The frequencies are chosen such that there is one representative frequency from each band. [Note: Technically the 1.80 MHz frequency lies in the Medium Frequency (MF) band which is in the range 0.3 MHz to 3 MHz.] The All HF Amateur Band predefined frequencies are:

1.8, 3.5, 7.0, 10.1, 14.0, 18.1, 21.0, 24.9, 28.0 MHz.

Selection 4 allows a predefined subset of 5 high-band HF amateur band frequencies (based on U.S.A. Allocations) currently available in the 14-30 MHz range. The frequencies are chosen such that there is one representative frequency from each band. The High-Band HF Amateur frequencies are:

14.0, 18.1, 21.0, 24.9, 28.0 MHz.

Selection 5 will automatically load prestored frequencies from the file ION_FREQ.DAT. Up to nine frequencies, covering the range 1.8-30 MHz, can be prestored in the file. This file can be automatically modified by the user from within the program. It can be used to store frequency net lists or other favorite sets of frequency information.

The default selection for the Frequency Menu is <3> which picks the 9 HF amateur band frequencies to be used for prediction purposes. The default selection is also obtained by hitting the <Enter> key.

18. Choosing Prediction Months

The Month Selection Menu for selection of prediction months presents a variety of choices.

If a selection entry between 1 and 12 is made, this entry will then represent a single prediction month. For example, an entry of 3 represents the month of March; 12 represents December.

If selection 13 is made, all 12 months in sequence starting from January and ending with December will be used for prediction purposes.

If selection 14 is made, the program will prompt you for the total number of months (between 1 and 12) for which you want predictions. Following the entry of the number of months, the program then prompts you

for each month in the sequence which you care to use for prediction purposes.

If selection 15 is made for entering an interval of months, the program will prompt you for the starting month, an integer increment value, and then the ending month. The program will then list the months corresponding to this selected interval and will ask you if you wish to change the range of months selected. If the month range interval is not acceptable to you, type Y to change the range. If the range is acceptable, then type N, the default, to proceed. Should the increment of months or range be inconsistent or inappropriate, the program will ask you to re-enter the month range.

If selection 16 is made then the user has an opportunity to change the default month to be used in the selection process. When first executing, the default month is set to the present month. Select a new default month by entering a value from 1 to 12. The new default month will then be used for all subsequent propagation predictions. The setting of the default month does not preclude using any other month or months or month intervals when this menu is subsequently accessed.

Selection 17 from the Month Selection Menu allows a return to the Main Menu of the IONSOUND HDX TURBO program.

19. Choosing Prediction Times

The operator uses the Time Selection Menu to choose propagation prediction times.

If 0 or <Enter> is selected, IONSOUND HDX TURBO computes a 24 Hour Summary Table for presentation to the computer screen. A maximum of 8 unique parameters may be chosen, in any order, for these predictions.

Selections from 1 to 24 compute predictions for a single point in time. The hour and the minutes are entered in Universal Coordinated Time (UTC), using a number between 1.00 and 24.00. The digit (or digits) to the left of the decimal point correspond to the hour; the digits to the right of the decimal point correspond to the minutes (i.e., 12.35 corresponds to 12 hours and 35 minutes, UTC).

Selection 25 chooses every full hour from 1 to 24 for the prediction process.

Selection 26 allows entry of particular times of your own choosing. The user is prompted for the number of individual times, up to a maximum of 50. Each individual time is then entered one at a time following prompts.

Selection 27 allows an interval of time values to be selected. The starting time is entered, then the time increment (which must be greater than 0), and finally the ending time. As a simplification, the time moment selected for the interval should be rounded to the nearest 15 minutes. If a very small time increment is selected such that the total number of individual times exceeds 50, a message will appear indicating that the total number of time moments has been truncated to 50.

Following a continuation prompt indicating hit <Enter> to continue, the individual times in the overall time interval selected will appear on

the screen. A prompt by the program will then ask whether you wish to change these times. If you want to change these times type Y; if these times are acceptable, type N. The default value for changing these times is <N> so that the program can continue by simply hitting the <Enter> key.

[Note: If selection 27 is chosen by the user and a previously defined interval of time exists, the program will prompt whether you wish to use the previous time interval. The default for keeping the previously defined time interval is <Y> so that the program can continue by simply hitting the <Enter> key.]

Selection 28 of the Time Selection Menu allows the user to return to the Main Menu.

20. Choosing Prediction Modes

The Mode Selection Menu for choosing prediction modes presents a variety of choices, mainly for advanced users of IONSOUND HDX TURBO. These choices can greatly influence the propagation prediction process. At the beginning of the Mode Selection Menu, the lowest-order predicted F layer mode is displayed. Selecting a value of N from 1 to 10 causes the program to automatically seek other propagating modes supported by the ionosphere (for both the E layer and F layer) in addition to the value of the lowest order F layer mode.

Selection of N = 1 (the default value) will cause the mode searching algorithm to consider at least 1 hop for the minimum number of F layer hops. Selecting N = 2 will cause mode searching to consider at least 2 hops. Likewise, further increasing the value of N selected will cause the algorithm to search out an ever-increasing complexity of E layer and F layer hop combinations, up to the maximum value of N = 10. As the value of selected N is increased, the prediction time will also increase accordingly.

[Note: The mode searching algorithm is a complex process, since the program also considers mixed (i.e., combined E and F layer) modes of propagation. If at any time and at any frequency the lowest calculated F layer mode is blocked by the E layer, the program will seek mixed modes having the same number of hops, except that an E layer hop will replace one of the F layer hops. If this mode does not appear to propagate, another try is then made but with one more F layer hop than the original. If this mode in turn does not propagate, then a mixed mode at this increased number of hops is tried, except that one or two E layer hops are substituted in succession. The types of attempts at finding a propagating mode are continued in this fashion until all modes have been exhausted, up to and including two more hops than the starting number determined by the lowest F layer mode.]

Selection 11 allows the user to enumerate which E layer, F layer or combined E and F layer hop modes the program should be forced to consider. Following this selection, the user is asked to input the number of modes to predict, up to a maximum of value of 10. Prompting for the desired number of modes takes place through individual entry of each separate E layer and F layer hop mode combination desired. To input a given mode, the value of the hop corresponding to the F layer mode is entered first, followed by a comma and then the value of the hop corresponding to the E layer mode. For example, to enter a mode corresponding to 3 hops using the F layer and 1

hop using the E layer a value of 3,1 is entered.

Selection 12 allows the user to force the program to consider a single E layer propagation mode between the transmitter and the receiver. This one-hop E layer prediction can be useful when it becomes possible for E layer propagation to result in a higher MUF than the F layer mode.

Selection 13 from the Mode Selection Menu allows the user to return to the Main Menu of the IONSOUND HDX TURBO program.

21. Printing

Make sure that your printer is powered up and on-line before attempting to print anything. The most common usage of IONSOUND HDX TURBO is showing 24-hour prediction screens. These may be captured to the printer by the use of <Shift PrintScreen>. Two screens may be printed on a single sheet of paper. Most printers will require that you take them off-line and force a form feed in order to eject a printed page of paper.

[Note: As an alternative to printing on paper, various file capture utilities may be utilized. An example of such a computer program utility is PRN2FILE.COM and its documentation PRN2FILE.DOC which is available from Ziff-Davis Publishing Co., 1 Park Avenue, New York, NY 10016. Download of PRN2FILE.COM from PC-Magnet, an online service of PC-Magazine is also available. Call 1-800-346-3247 for closest access point.]

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Glossary of Terms

| | |
|-------------|---|
| ARRL | American Radio Relay League |
| BBC | British Broadcasting Corporation |
| BRNG | bearing |
| CCIR | International Radio Consultative Committee |
| CW | continuous wave, Morse code |
| dB | decibel |
| dBuV | dB signal level with respect to 1 microvolt |
| DBUVM | dB field strength with respect to 1 microvolt/meter (dBuV/m) |
| dBW | dB power with respect to 1 Watt |
| dBWn | dB noise power with respect to 1 Watt |
| dBWs | dB signal power with respect to 1 Watt |
| DBWM | dB power density with respect to 1 Watt/meter squared (dBW/m ²) |
| DOS | disk operating system |
| ELE or ANG | elevation or takeoff angle |
| F/B | front/back |
| FOE | E Layer critical vertical incidence frequency |
| FOF | F Layer critical vertical incidence frequency |
| FOT | optimum working frequency (usually below MUF) |
| FREQ | frequency |
| Ham | amateur radio operator |
| HF | high frequency |
| HPF | highest possible frequency |
| Hz | hertz (unit of frequency) |
| IONCAP | Ionospheric Communications Analysis and Prediction Program |
| L PATH | long path |
| LUF | lowest useful frequency (usually limited by absorption and noise) |
| MCFO | maximum critical oblique frequency |
| MCFV | maximum critical vertical frequency |
| MHz | megaHertz |
| MUF | maximum useable frequency (for a particular layer and distance) |
| NOAA | National Oceanographic and Atmospheric Administration (U.S.) |
| NFW | Noise Power in dB-Watts (decibels above or below 1 watt) |
| NTIA | National Telecommunications and Information Administration (U.S.) |
| %SIG or %S | signal-to-noise availability N, expressed in percent (%) [percentage of days of the month that the signal-to-noise ratio meets or exceeds the minimum signal-to-noise ratio] |
| %PATH or %P | propagation path availability P, expressed in percent (%) [percentage of days of the month that the predicted propagation path will be available] |
| %TOT or %T | total link reliability N x P, expressed in percent (%) [represents the numeric product of signal-to-noise availability, %SIG, and propagation path availability, %PATH, and signifies overall link quality] |
| RX | receiver |
| S/N or SNR | signal-to-noise ratio in decibels |
| S PATH | short path |

Glossary of Terms
(continued)

| | |
|-------|---|
| SBRNG | switched bearing (long path bearing, 180 degrees opposite BRNG) |
| SESC | Space Environmental Services Center, NOAA, Boulder, CO (U.S.) |
| SSN | smoothed sunspot number |
| SFN | solar flux number (measured at 2800 MHz) |
| SM+dB | S Meter + dB [represents S0-S9 plus dB readings above S9] |
| SVM | signal voltage in dB-Microvolts (dBuV) |
| SWL | shortwave listener |
| TX | transmitter |
| UTC | Universal Coordinated Time |
| VHF | very high frequency |
| WWV | A radio station of the National Bureau of Standards (U.S.) |

Appendix

NATIONAL BUREAU OF STANDARDS (NBS) SERVICES

The U.S. National Bureau of Standards (NBS) broadcasts the latest geomagnetic Ap and K indices, the 2800 MHz solar flux level number (SFN), and short-term forecasts of expected propagation conditions on radio station WWV, simultaneously at 18 minutes past each hour on 2.5, 5, 10, 15, and 20 MHz. These transmissions originate from Ft. Collins, CO. In addition, radio station WWVH, located in Hawaii, broadcasts Geophysical Alerts at 45 minutes past the hour on 2.5, 5, 10 and 15 MHz. WWV and WWVH information is updated every 3 hours starting at 0000 UTC.

The on-duty forecaster at the National Oceanographic and Atmospheric Administration (NOAA) Space Environmental Services Center (SESC) in Boulder, CO is also able to provide Alert data by calling 303-497-3171. This information is also available, free of charge, by calling NOAA's SESC at 303-497-3235. The SESC also provides a free on-line, menu-driven modem bulletin board service at 303-497-5000, 24 hours a day, for access to propagation data, solar reports, solar and geomagnetic data, and MUF predictions. Modem access is at 300, 1200, or 2400 baud, with a standard protocol of 8-bit data word, 1 stop bit, and no parity.

NOAA publishes a booklet which should be considered required reading for those who would like to more completely understand and utilize WWV and WWVH propagation forecasts. It provides complete and easy-to-understand descriptions of the solar/terrestrial indices, a glossary of terms, sources of information, and key details of NOAA's telephone bulletin board service (EBS). This booklet, "A User's Guide to the Space Environment Services Center Geophysical Alert Broadcasts," is available free of charge from the NOAA SESC by requesting a copy of NOAA Technical Memorandum ERL SEL-79. The address for obtaining this free booklet is:

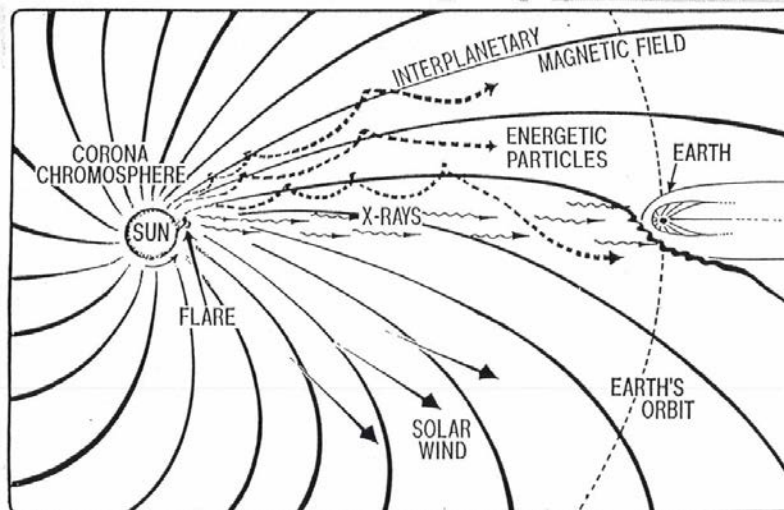
The Space Environment Services Center
NOAA/ERL/SEL - R/E/SE2
325 Broadway
Boulder, CO 80303-3328, USA

2. SOLAR WIND AND SPACE WEATHER

THE EARTH IN THE SOLAR WIND

- This next chart, published in NOAA Technical Memorandum ERL SEL-80 by the Space Environment Laboratory (Boulder, CO), shows the primary influences by the sun on the earth.
- These influences result from the solar wind as the earth orbits the sun and encounters a host of energetic particles, x-rays, flares and other emanations from the corona chromosphere, along with an interplanetary magnetic field.
- All of these influences contribute to a complex interaction that affects ionospheric propagation.

THE EARTH IN THE SOLAR WIND



NOAA Technical Memorandum ERL SEL-80

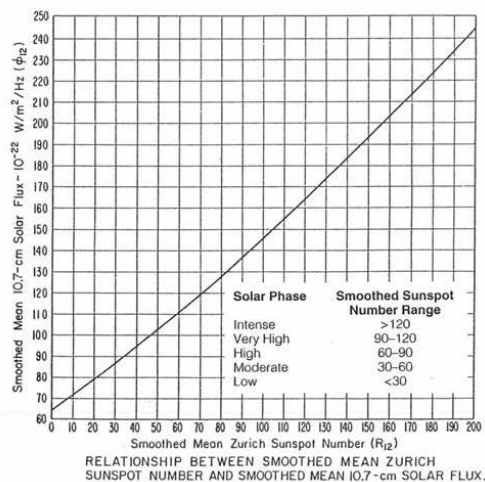
Space Environment Laboratory
Boulder, Colorado
June 1990

A RADIO FREQUENCY USER'S GUIDE TO THE SPACE ENVIRONMENT
SERVICES CENTER GEOPHYSICAL ALERT BROADCASTS

SMOOTHED SUNSPOT NUMBERS VS. SMOOTHED SOLAR FLUX

- Shown in this next graphic is the relationship between Smoothed Mean 10.7-cm Solar Flux and Smoothed Mean Zurich Sunspot Number.
- The Smoothed Sunspot Number range is further categorized according to the Solar Phase as Low, Moderate, High, Very High, and Intense.
- Smoothed Sunspot Number or Smoothed 10.7-cm Solar Flux is essential to IONSOUND HDX Turbo propagation prediction and is made available from the Space Environment Services Center Geophysical Alert Broadcasts.

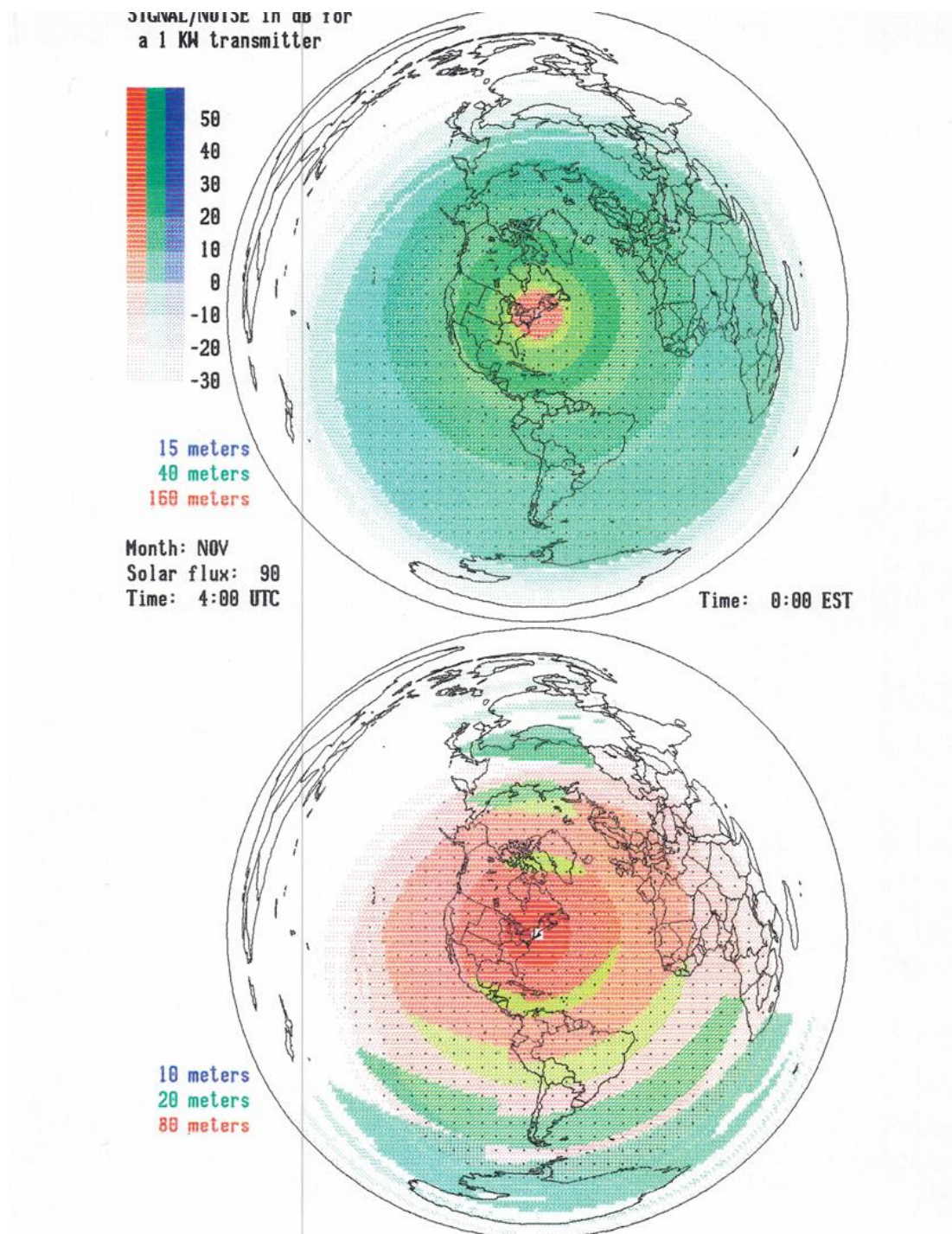
Smoothed Sunspot Numbers vs. Smoothed Solar Flux

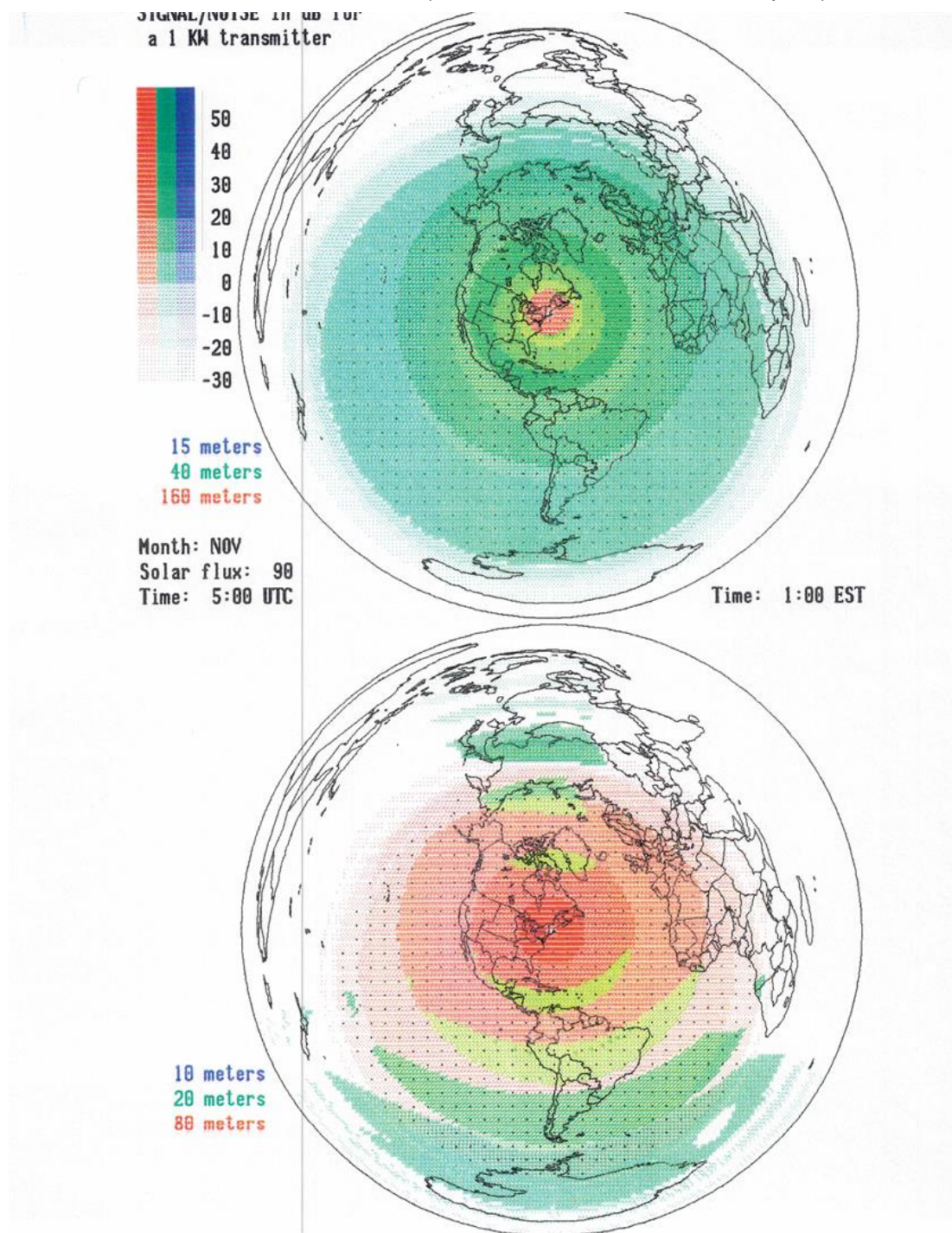


NOAA WWV/WWVH AND CHU BROADCASTS AND SPACE WEATHER GEOPHYSICAL ALERTS

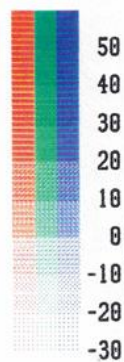
- The National Oceanic and Atmospheric Administration (NOAA) uses WWV and WWVH to broadcast geophysical alert messages that provide information about solar terrestrial conditions. Geophysical alerts are broadcast from WWV at 18 minutes after the hour and from WWVH at 45 minutes after the hour. The messages are less than 45 seconds in length and are updated every 3 hours (typically at 0000, 0300, 0600, 0900, 1200, 1500, 1800, and 2100 UTC). More frequent updates are made when necessary. WWV broadcasts on 2.5, 5, 10, 15 and 20 MHz from a location near Fort Collins, Colorado. WWVH broadcasts on 2.5, 5, 10 and 15 MHz from Kauai, Hawaii. Both stations broadcast a timing signal 24 hours per day, 7 days per week, to listeners all over the world. CHU transmitted frequencies from Ottawa, at 3.330, 7.335 and 14.670 MHz, are provided by the government of Canada in order to disseminate standard time information.
- All broadcast frequencies used by WWV and WWVH are in the high frequency (HF) radio spectrum which extends from 3 to 30 MHz. This part of the spectrum is commonly referred to as "shortwave". General coverage shortwave receivers typically receive all frequencies from 530 kHz (the beginning of the AM broadcast band) to 30 MHz and are capable of receiving WWV, WWVH and CHU on all of the available frequencies.

EXAMPLES OF HOURLY WORLD-WIDE S/N PREDICTIONS FOR NOVEMBER (SFN=90) DERIVED FROM IONSOUND HDX TURBO SOFTWARE, CENTERED ON BOSTON, MA



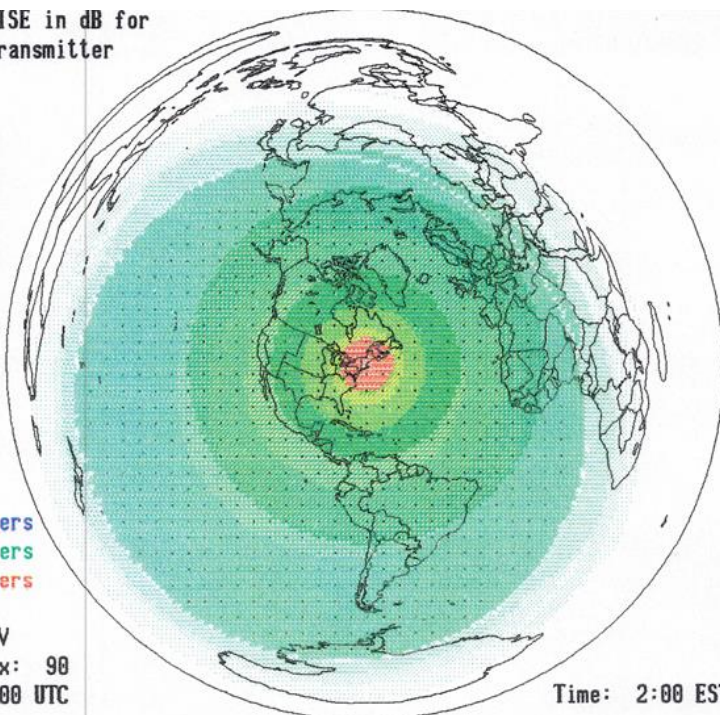


SIGNAL/NOISE in dB for
a 1 KW transmitter

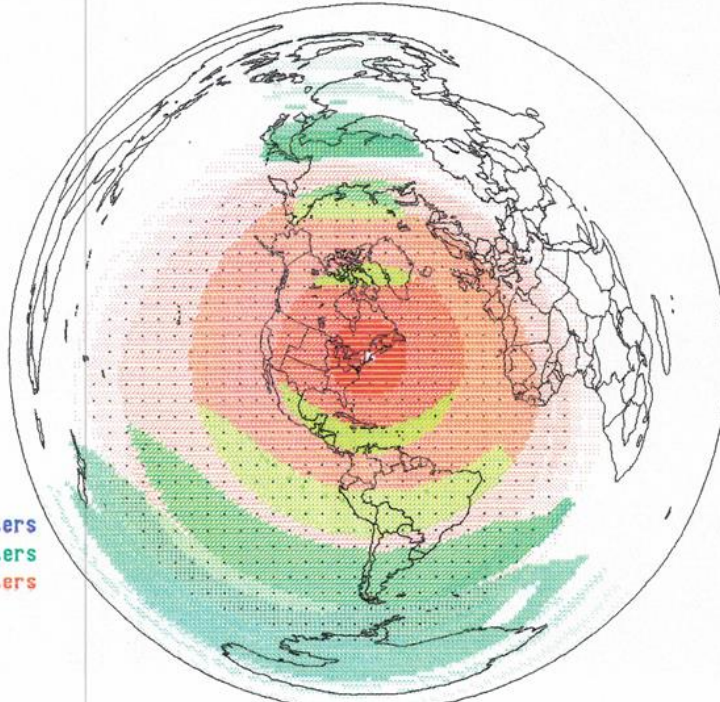


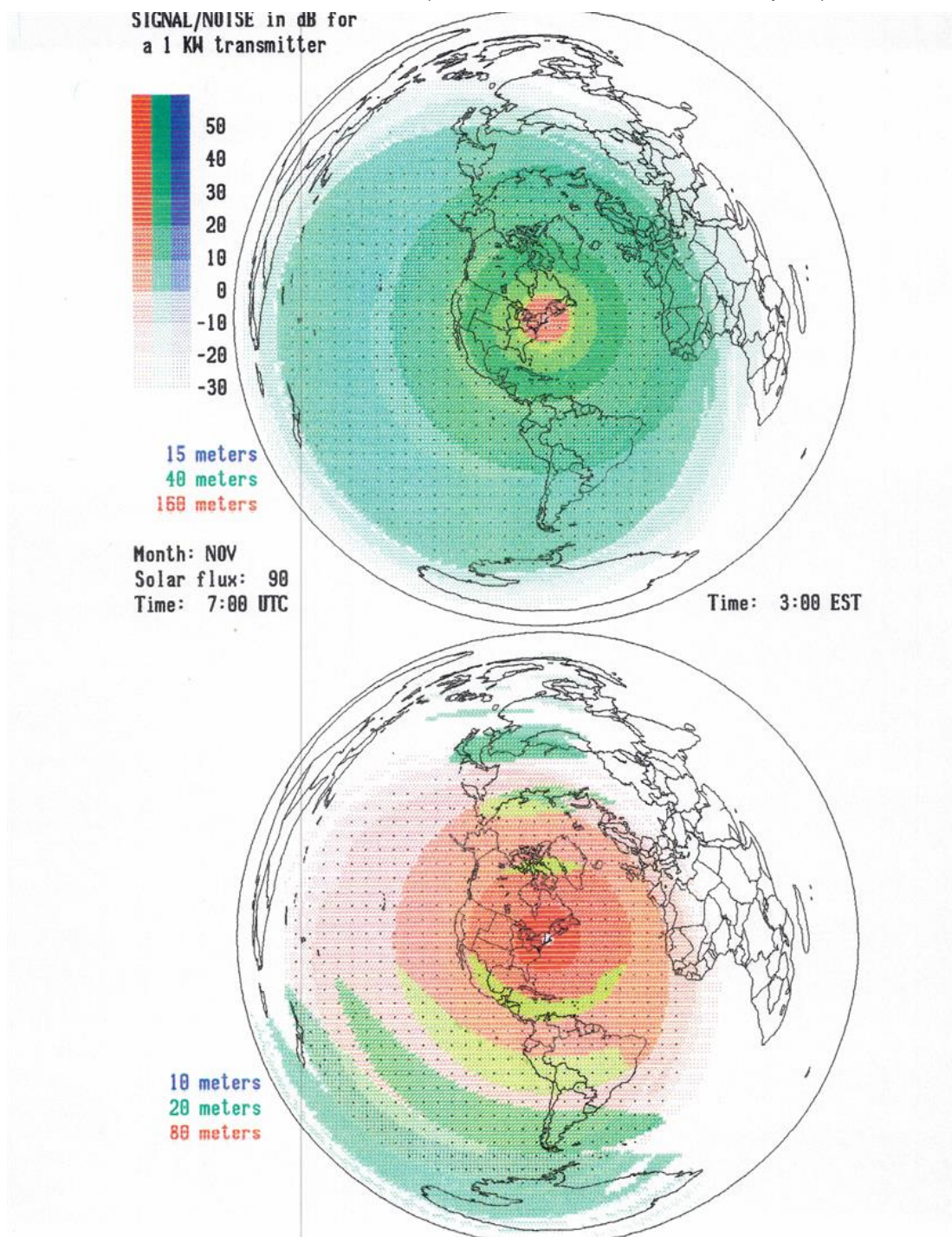
15 meters
40 meters
160 meters

Month: NOV
Solar flux: 90
Time: 6:00 UTC

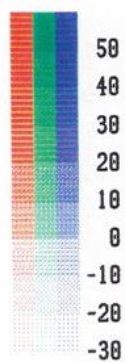


10 meters
20 meters
80 meters



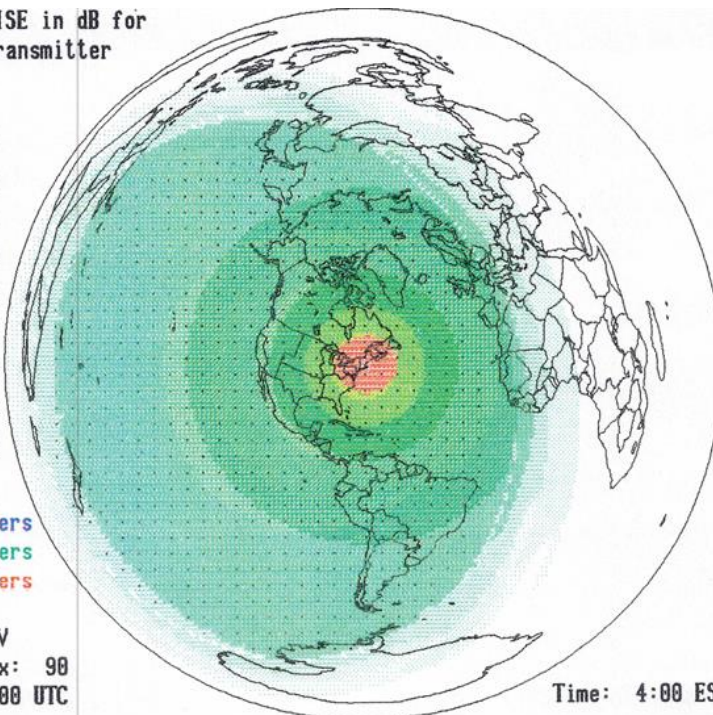


SIGNAL/NOISE in dB for
a 1 KW transmitter



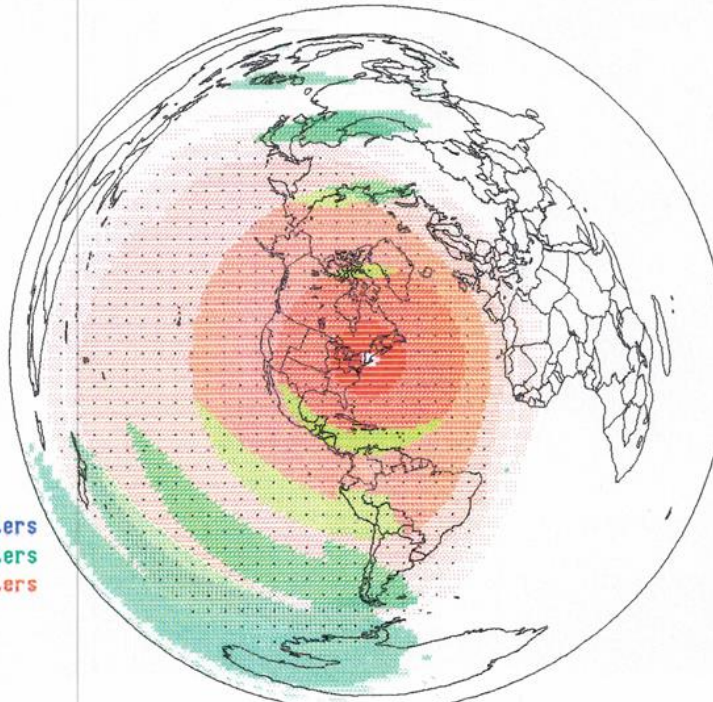
15 meters
40 meters
160 meters

Month: NOV
Solar flux: 90
Time: 8:00 UTC

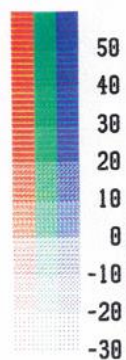


Time: 4:00 EST

10 meters
20 meters
80 meters



SIGNAL/NOISE in dB for
a 1 KW transmitter

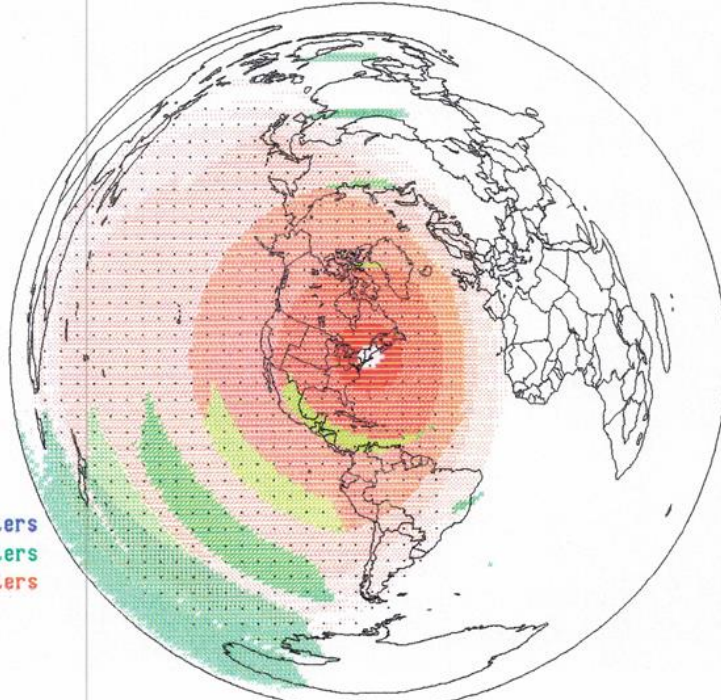


15 meters
40 meters
160 meters

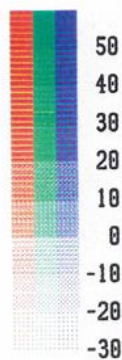
Month: NOV
Solar flux: 90
Time: 9:00 UTC

Time: 5:00 EST

10 meters
20 meters
80 meters



SIGNAL/NOISE in dB for
a 1 KW transmitter

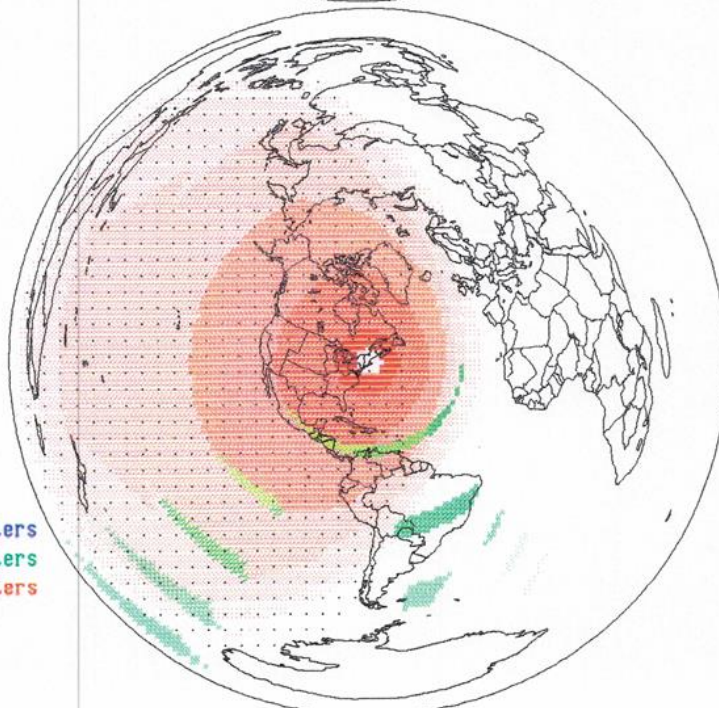


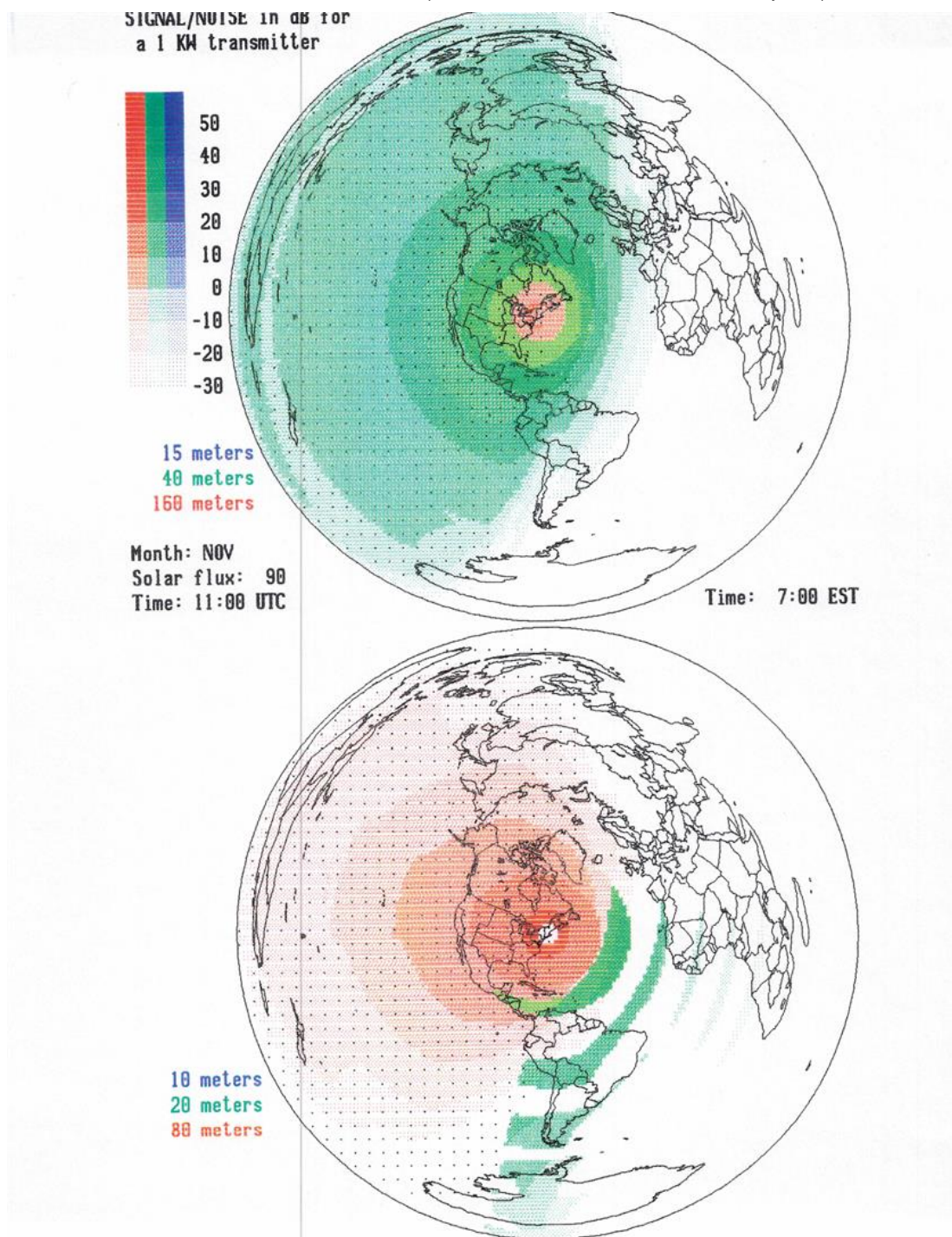
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40 meters
160 meters

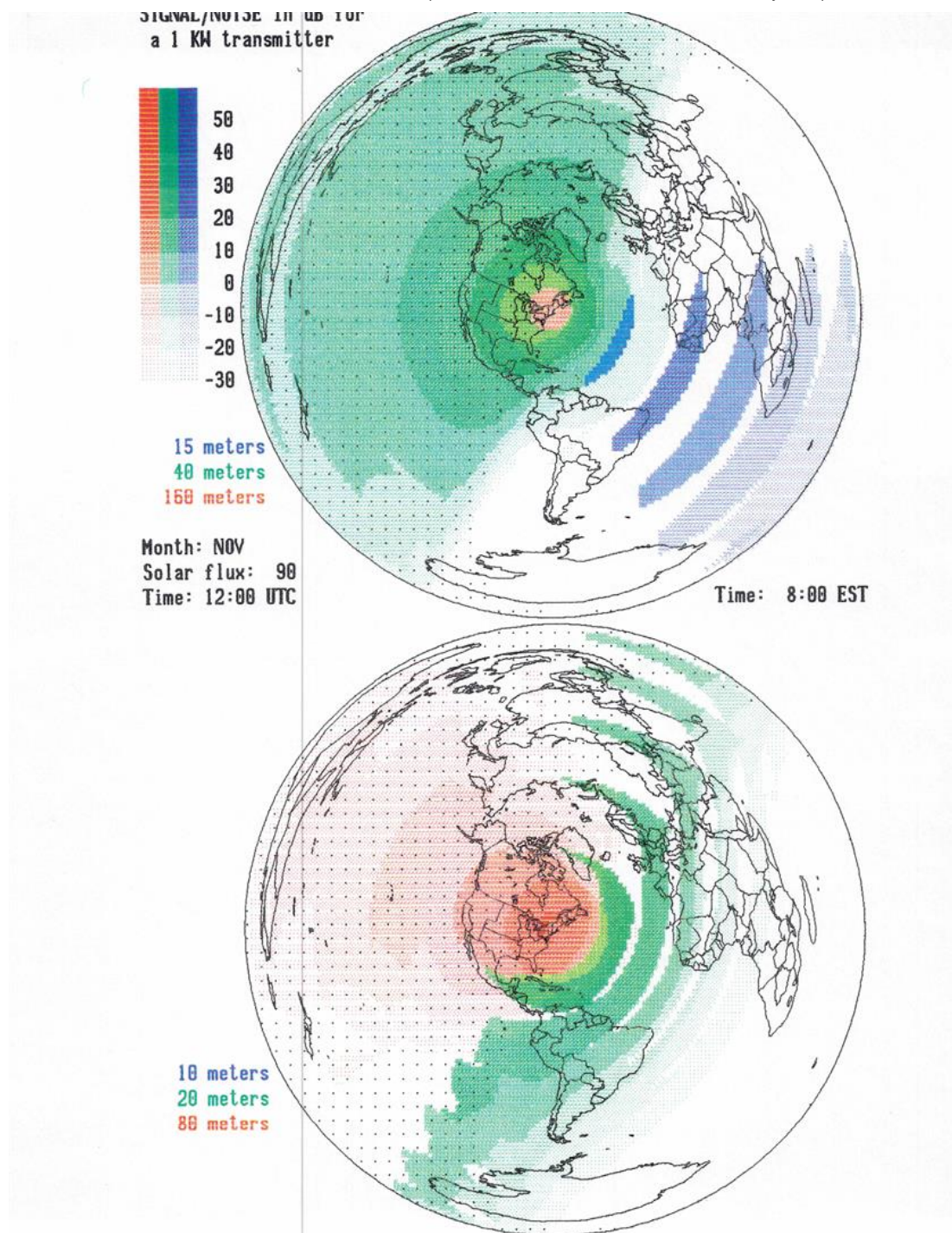
Month: NOV
Solar flux: 90
Time: 10:00 UTC

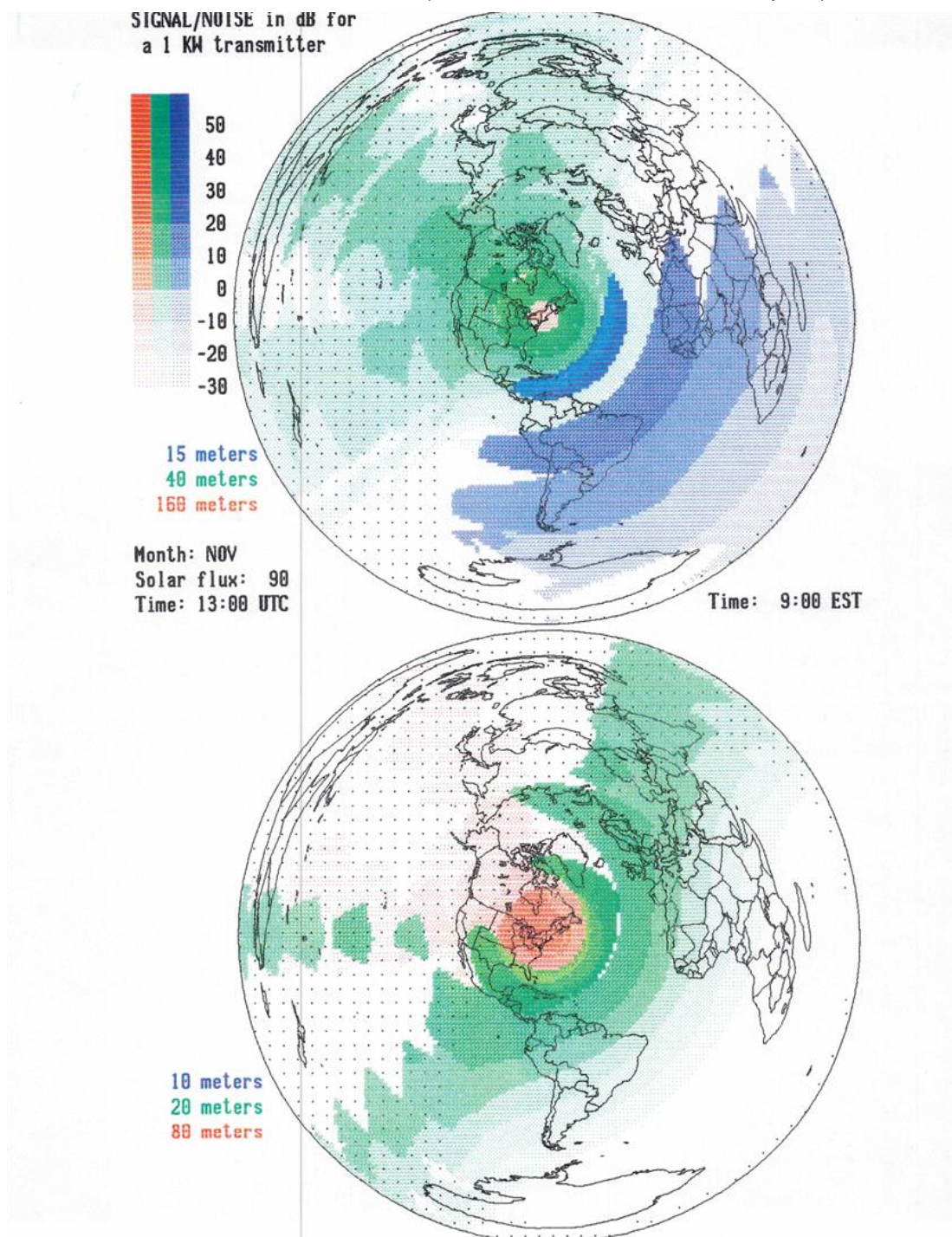
Time: 6:00 EST

10 meters
20 meters
80 meters

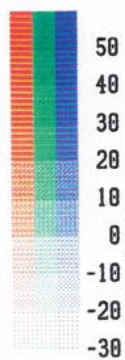








SIGNAL/NOISE in dB for
a 1 KW transmitter

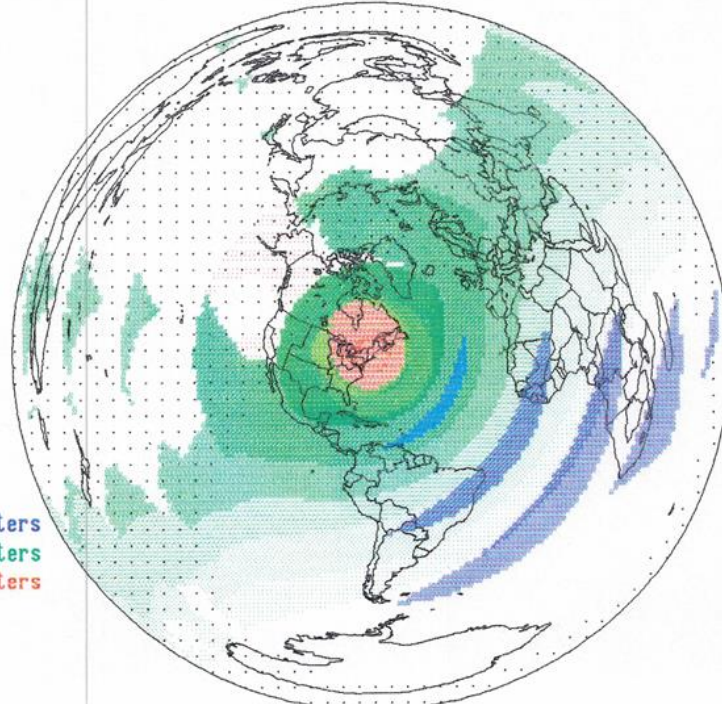


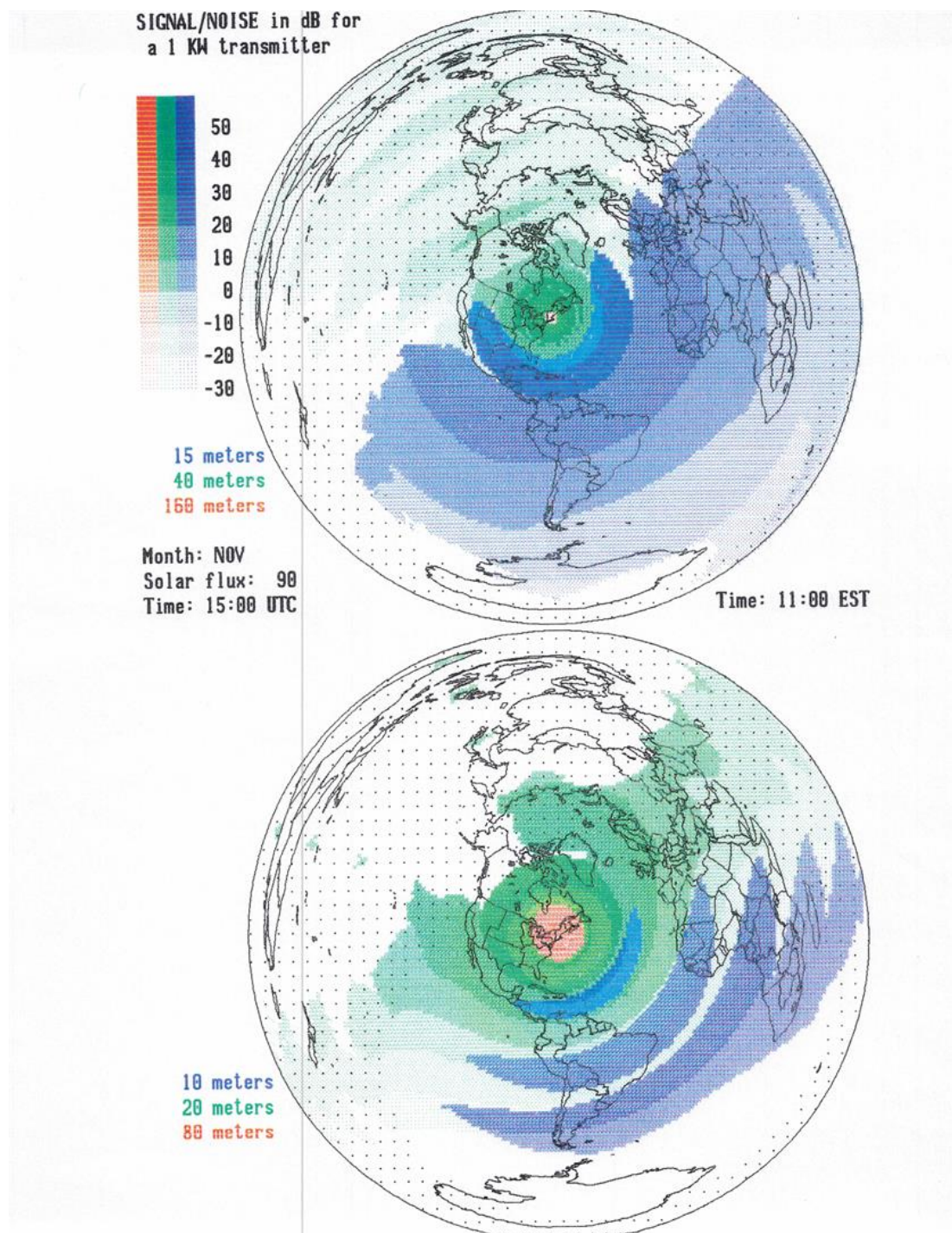
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40 meters
160 meters

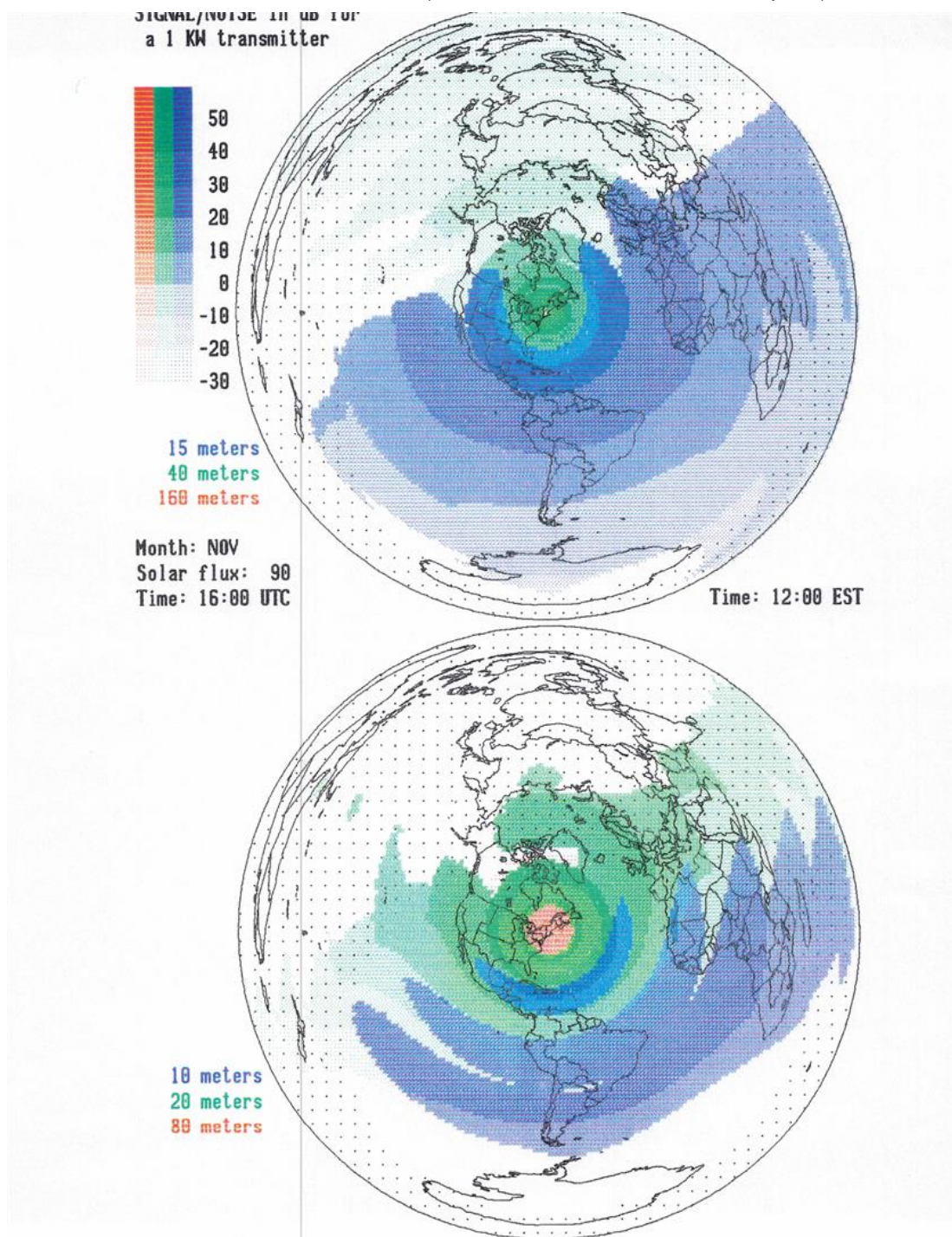
Month: NOV
Solar flux: 90
Time: 14:00 UTC

Time: 10:00 EST

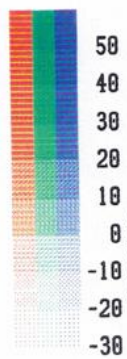
10 meters
20 meters
80 meters







SIGNAL/NOISE in dB for
a 1 KW transmitter

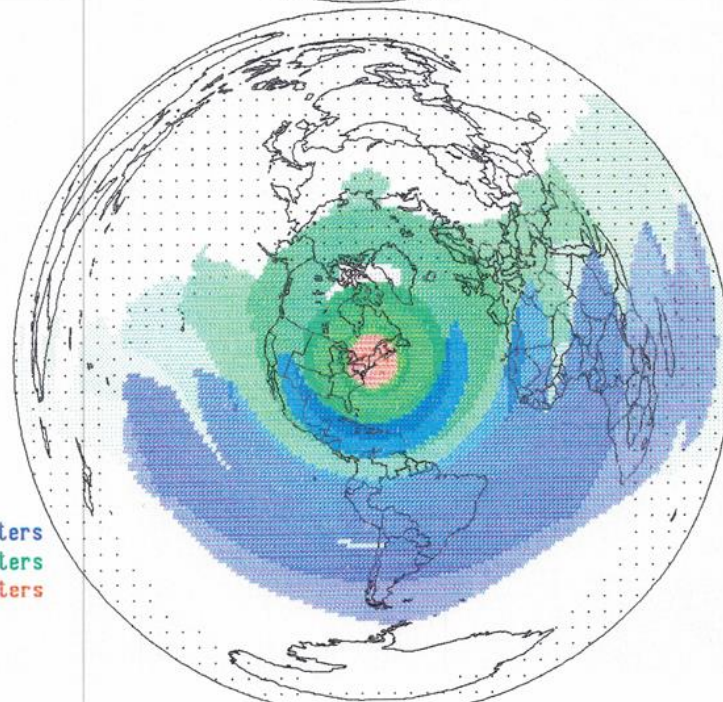


15 meters
40 meters
160 meters

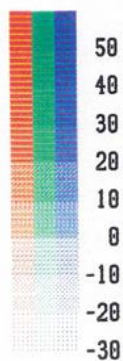
Month: NOV
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Time: 17:00 UTC

Time: 13:00 EST

10 meters
20 meters
80 meters



SIGNAL/NOISE in dB for
a 1 KW transmitter

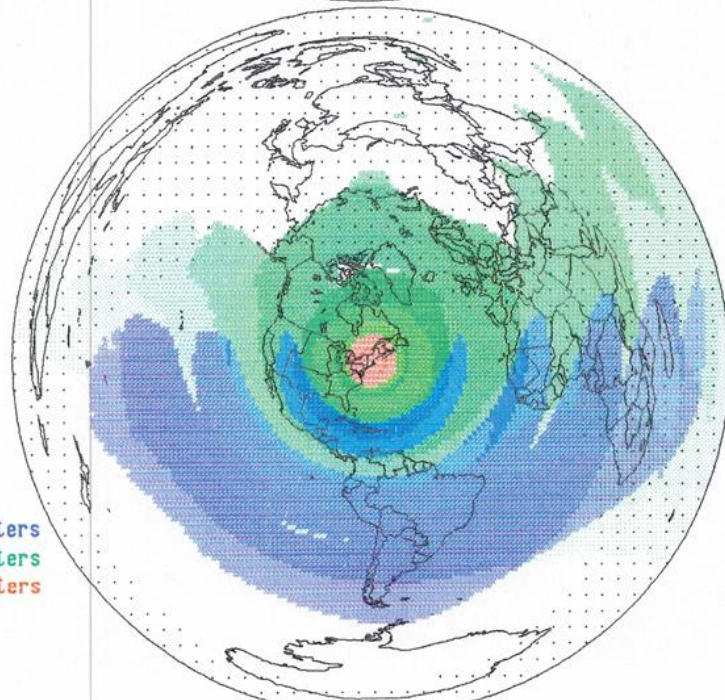


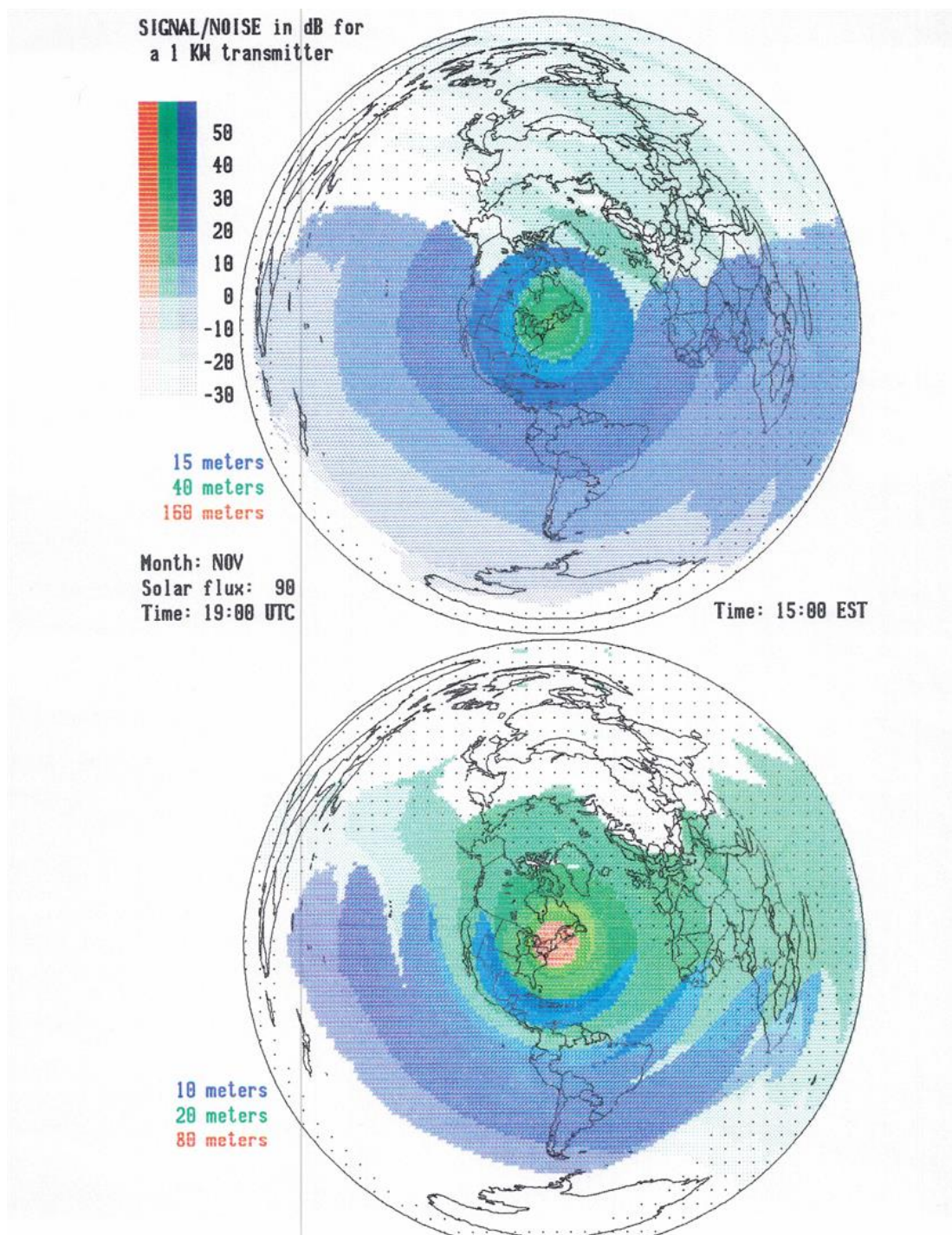
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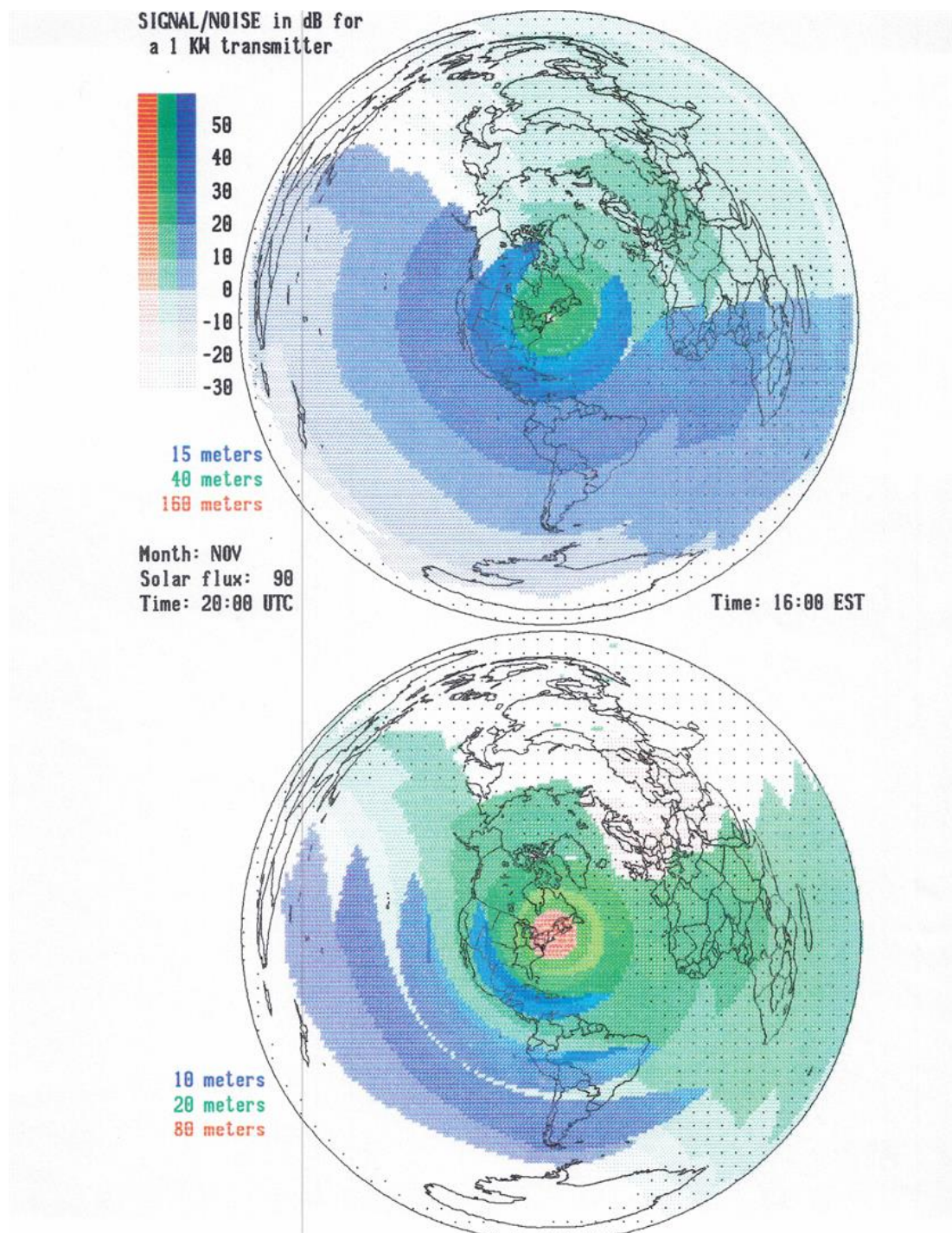
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Solar flux: 90
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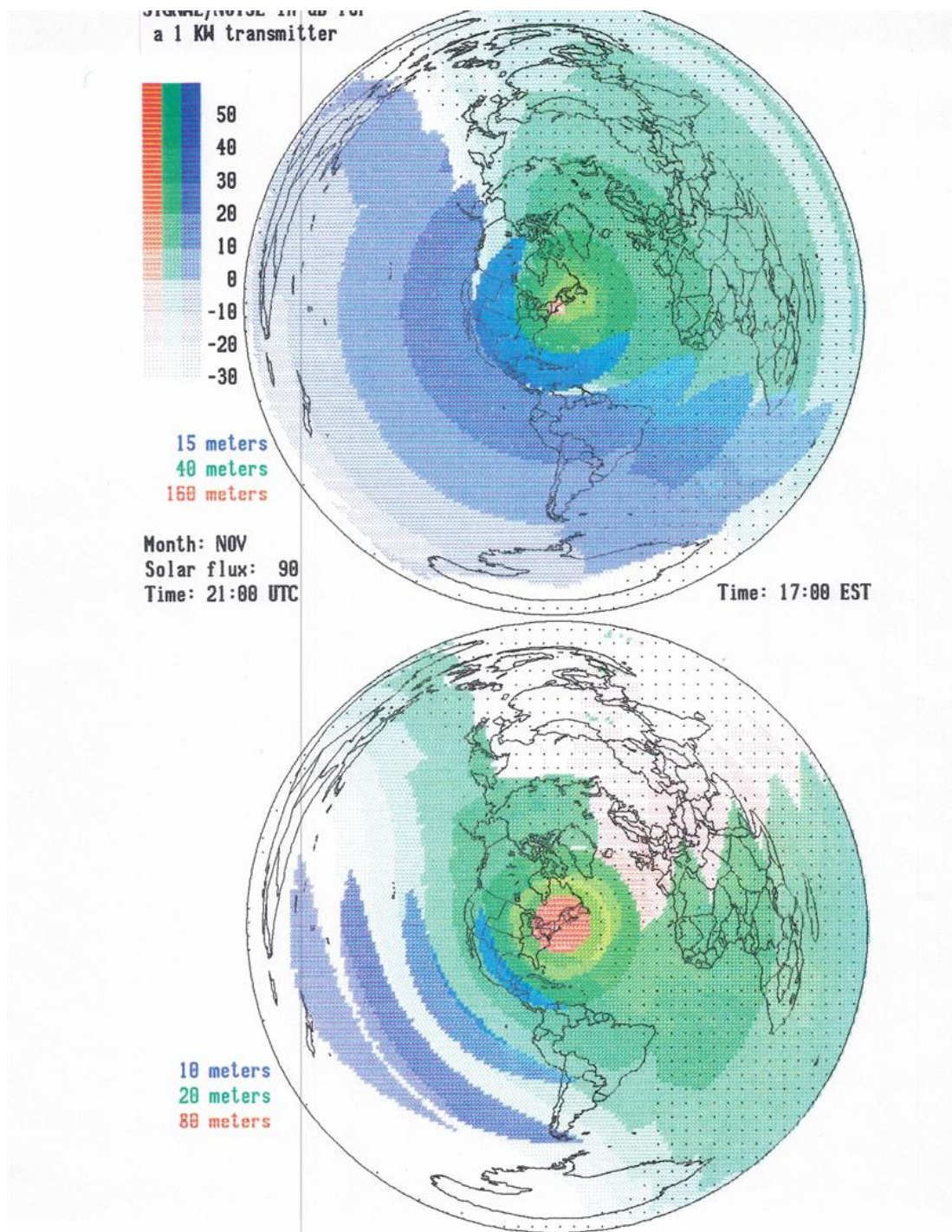
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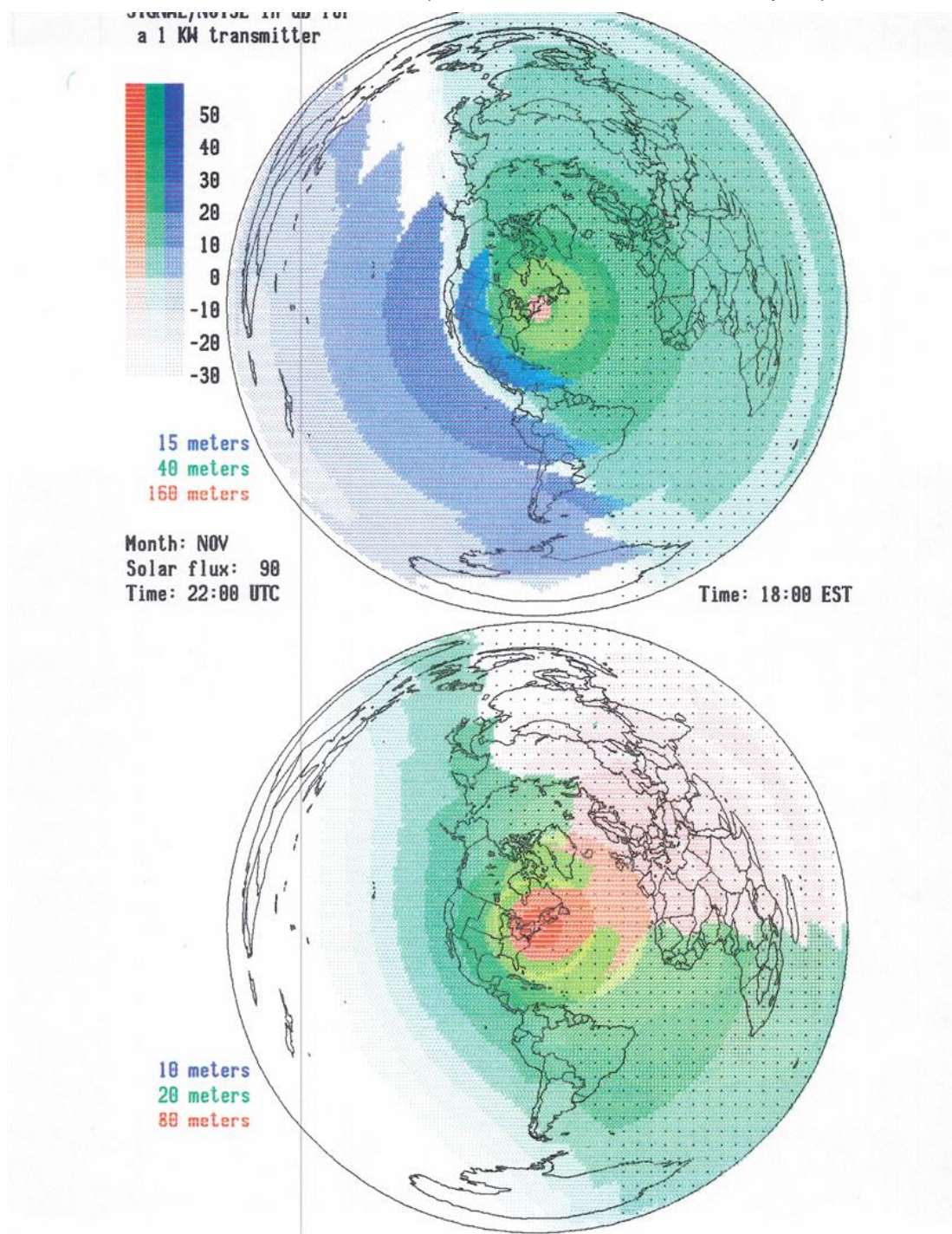
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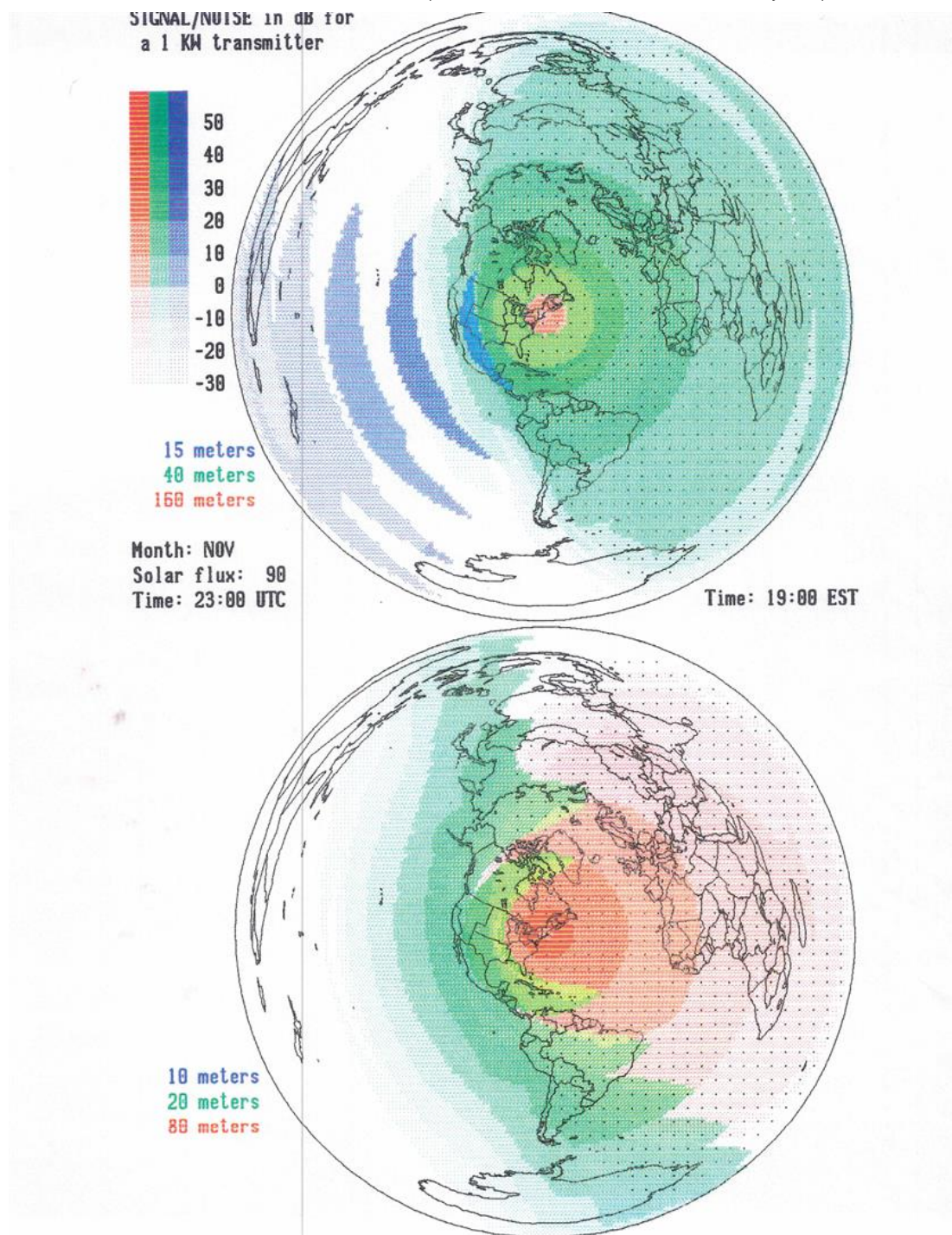


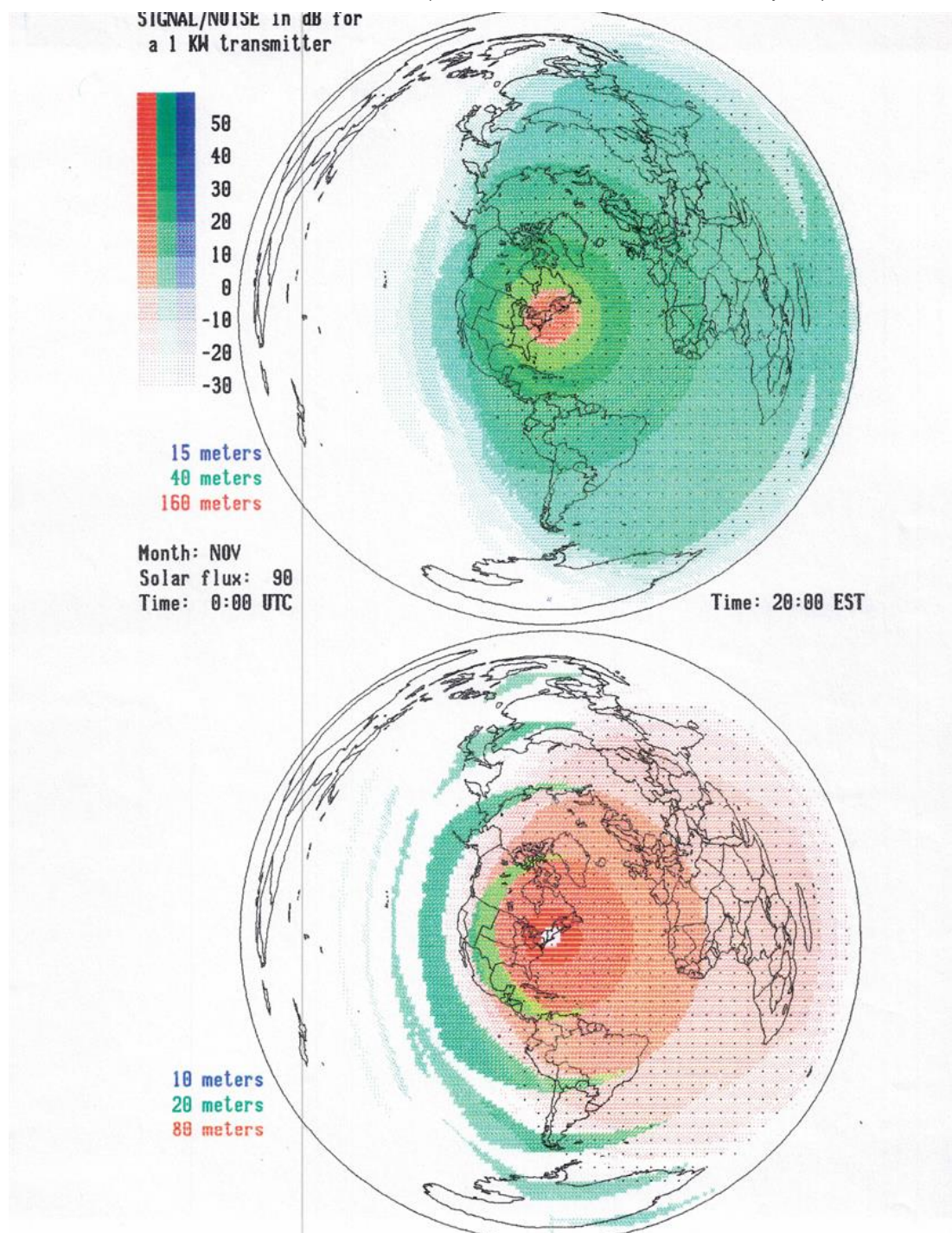


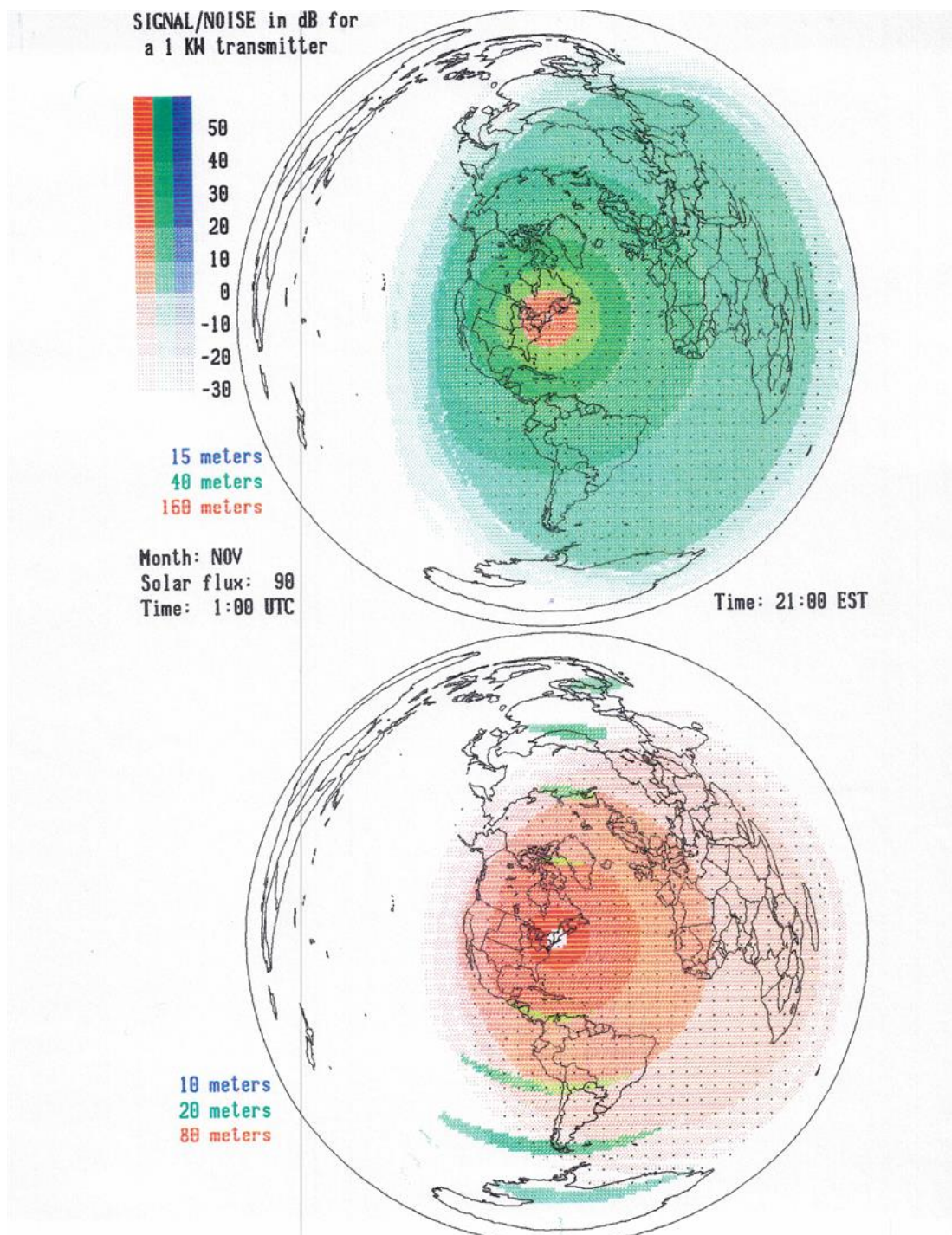


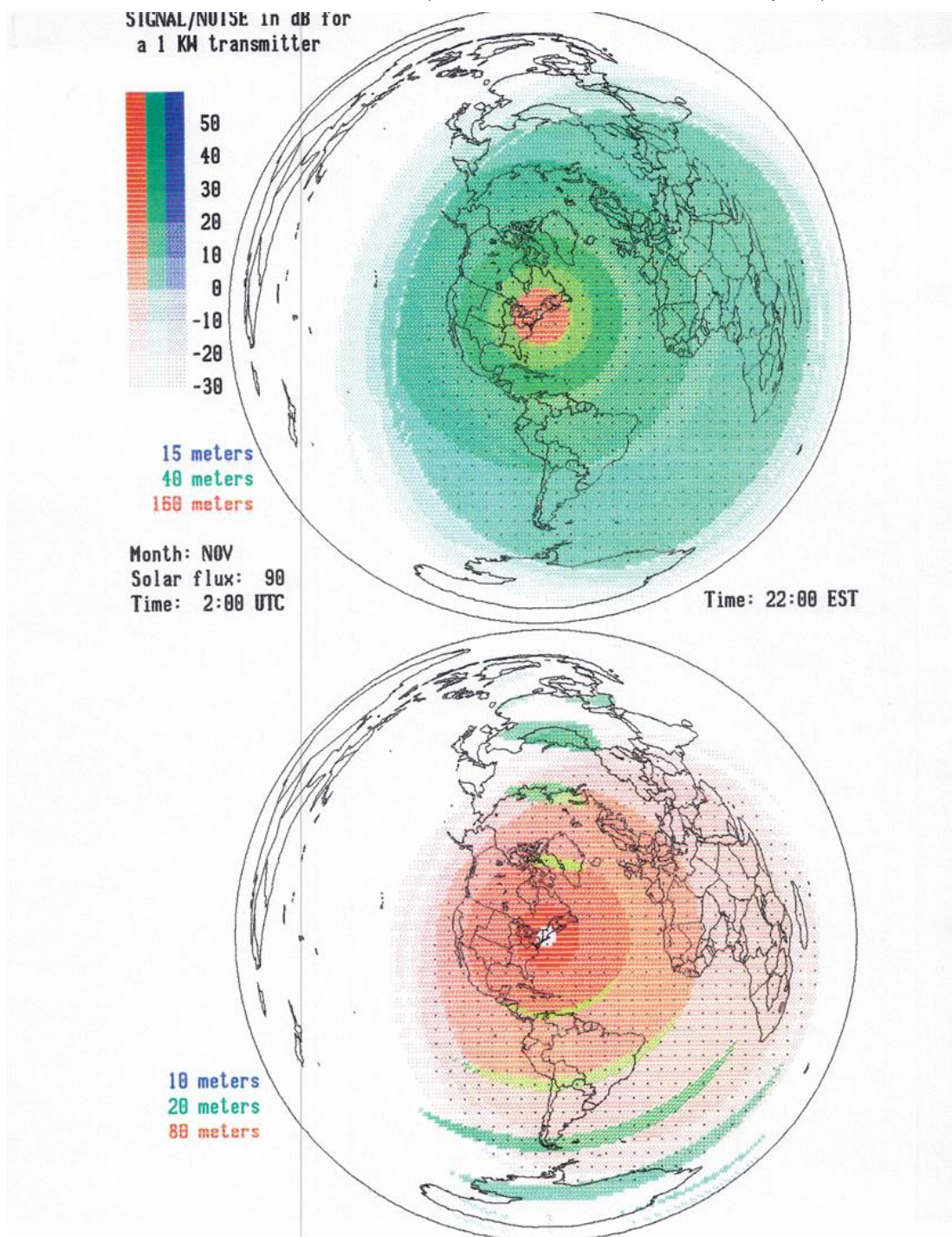


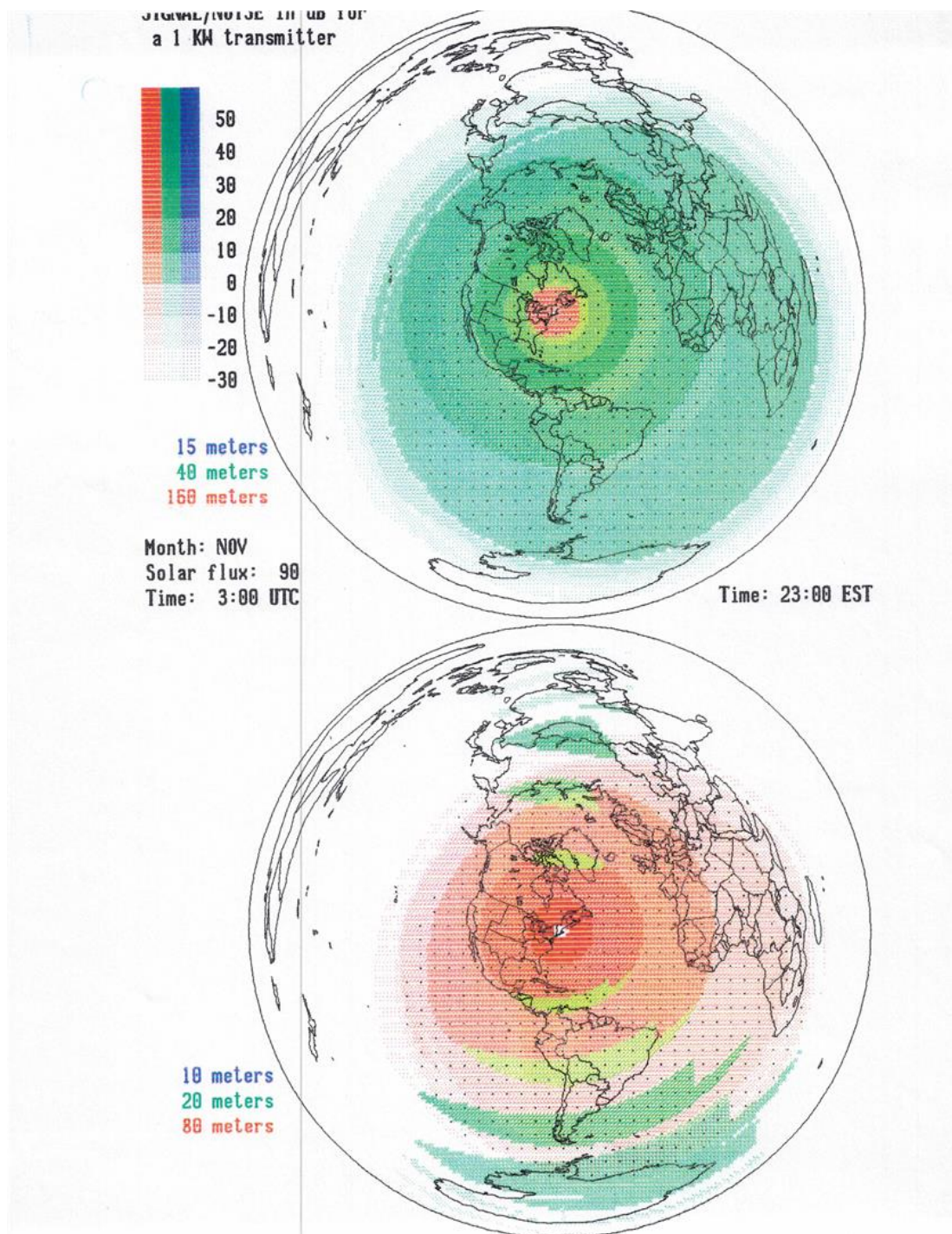












6. IONSOUND HDX TURBO SOFTWARE AVAILABILITY

A free copy of IONSOUND HDX TURBO software may be obtained electronically (by e-mail) for HAMSCI participants upon request from the author, Jake / W1FM. Send your request with your name, affiliation, amateur call-sign (if applicable), and e-mail address to the following email address of SkyWave Technologies:

SkyWaveTec@AOL.com

As a suggestion, please consider a donation to The American Radio Relay League, Inc. They are located at:

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225 Main Street

Newington, CT

06111-1400

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ABSTRACT

IONSOUND HDX TURBO is a software propagation prediction program that evolved over a number of years and was primarily marketed in the 1990's by its author, W1FM, for use with IBM or IBM-compatible personal computers using DOS. It was intended to produce easy-to-interpret tabular predictions of radio frequency link performance between any two locations on the earth's surface. Menu selections within IONSOUND made it possible to compute predictions for comparison with Highest Possible Frequency (HPF), Maximum Possible Frequency (MPF) and Frequency of Optimum Transmission (FOT) predictions derived from U.S. Department of Commerce, National Telecommunications and Information Administration (NTIA) IONCAP program as found in ARRL's monthly QST Magazine "How's DX" Column. Parameters used in predictions included: Transmit and Receive Location, Short or Long Path, Local Receiver Noise Condition, Transmit and Receive Antenna/Gain, Receiver Bandwidth, Required Signal-to-Noise Ratio, Transmitter Power, Sunspot Number (SSN) or Solar Flux Number (SFN), Minimum Elevation Angle from the horizon, Prediction Frequencies, Prediction Months, Prediction Times, and Prediction Modes involving E and F layer propagation. The Receive Reliability prediction estimates include Total Receive Reliability which is composed of the product of Path Reliability and Signal-to-Noise (S/N) Availability. Path Reliability deals with the physics of the communication path specified by user-supplied transmitter/receiver latitude/longitude or location choices whereas the S/N Availability deals with the effects of absorption on the actual signal levels and local noise conditions relative to the minimum required S/N specified by the user. Takeoff radiation angle dependency on E, F, or multimode E/F hops along with antenna elevation angle gain, E and F ionospheric absorption, polarization loss, and ground reflection losses are also taken into account.