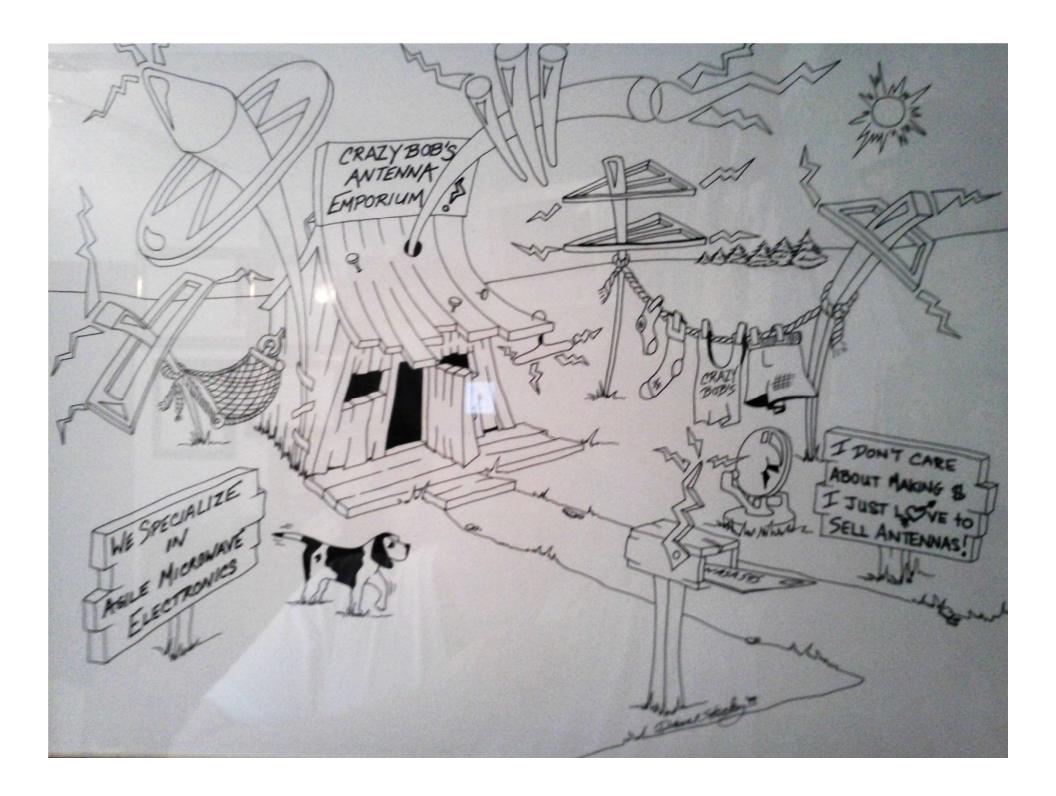
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Crazy Antennas

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<u>Abstract</u>

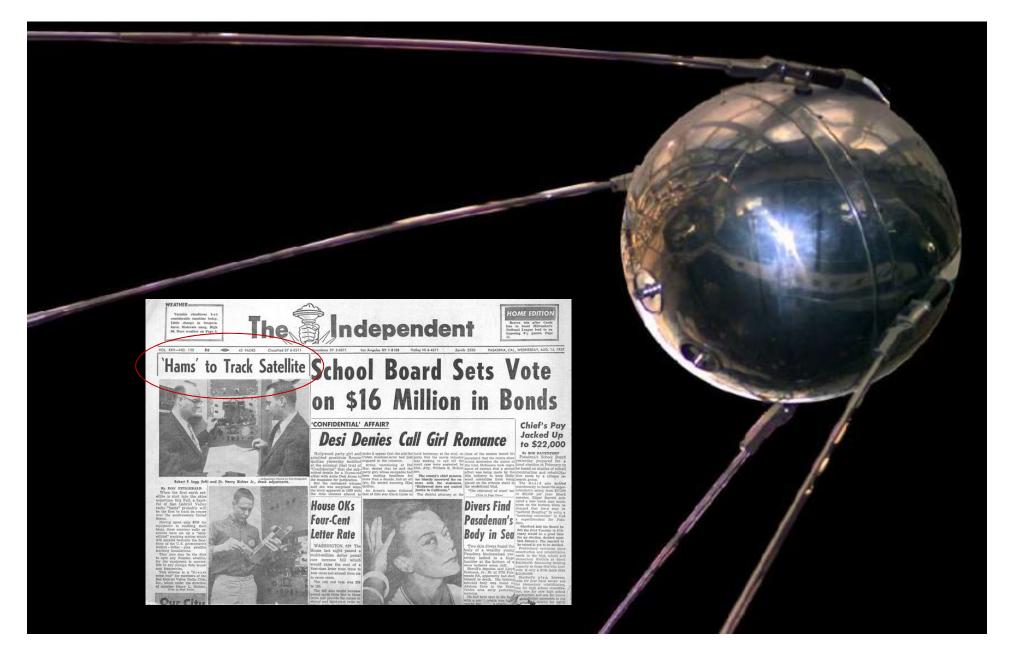
Everyone here is familiar with traditional antennas, time-honored favorites like dipoles and solid parabolic reflectors. But occasionally, circumstances call for something peculiar. This paper will describe a number of unusual antennas for particular communications scenarios that have been developed by the author and his colleagues at the NASA Glenn Research over the past decade or so. The list includes:

- K-band scanning ferroelectric reflectarray;
- UHF "Vivaldi" for cellular connectivity to unmanned aerial vehicles;
- Ku-band array that develops a top-hat pattern to feed a zone plate antenna;
- Active antenna that toggles between Iridium and GPS bands;
- VHF hybrid spiral/dipole for orientation determination on Venus;
- Ku-band deployable reflector that strongly resembles a giant beach ball,
- Combination Ka-band parabolic reflector and 1550 nm telescope called the "teletenna."

Design strategy and performance results will be included, and trends towards cognitive antennas will be discussed.

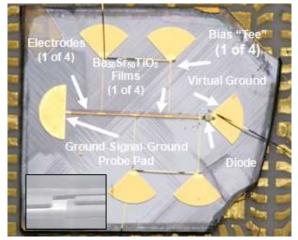
Let's Put Things in Perspective: Over five decades would pass between the first wireless telegraph clicks and the world's first artificial Earth satellite - Sputnik 1. Sputnik 1 was a 58.0 cm-diameter aluminum sphere that carried four whip antennas that were about 2.5 m long.



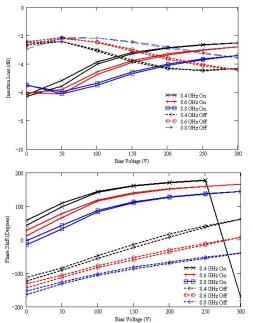


Scanning Ferroelectric Reflectarray ¹

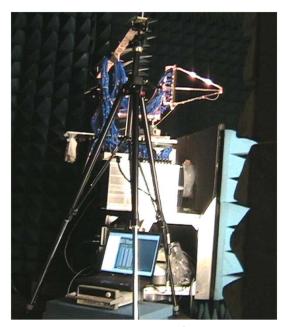




Hybrid X-band ferroelectric/semiconductor phase shifter on 0.5 mm thick lanthanum aluminate. The device is 10 mm X 9 mm. The 1.2 mm long G-S-G pad is sacrificed (sawed) after characterization, so final size is about 9 X 9 mm2. Each $\lambda g/4$ electrode produces $\approx 40^{\circ}$ of phase shift. Inset shows SEM of partial electrode.

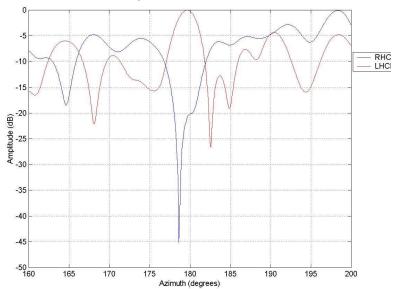


Measured insertion loss and phase of hybrid ferroelectric/ semiconductor phase shifter as a function of bias voltage on the ferroelectric section and switch state.



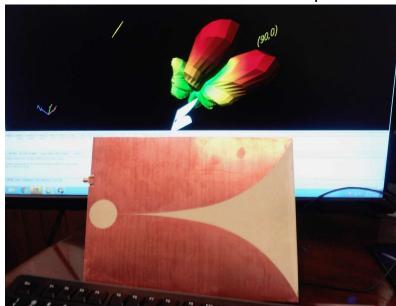


Testing the 615 Element K-band Reflectarray and Low Power Controller in NASA Glenn's Far Field Chamber



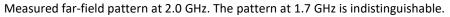
Measured Ferroelectric Reflectarray Antenna Pattern at 19 GHz

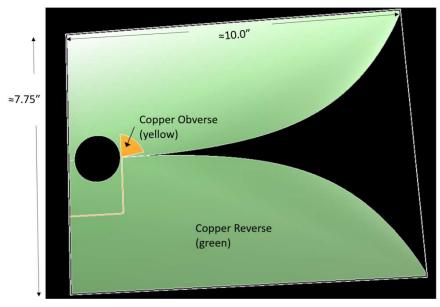
700 MHz to 2 GHz Vivaldi Proposed for Cellular Control of Unmanned Aerial Vehicles ²



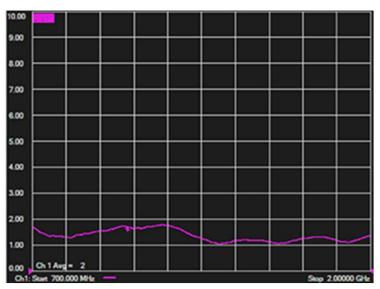
0 -5 -10 -15-20 -25 -30 -35 -40 -45 -50 -70 -50 -30 2 GHz Co-Pol 2 GHz Cross-Pol

Simulated pattern at 2 GHz (background). The discontinuity at θ =90°, Φ =0° is an artifact of the finite ground plane but infinite substrate that was used in the model. Fabricated copper antenna on low-loss Teflon substrate (foreground) ³





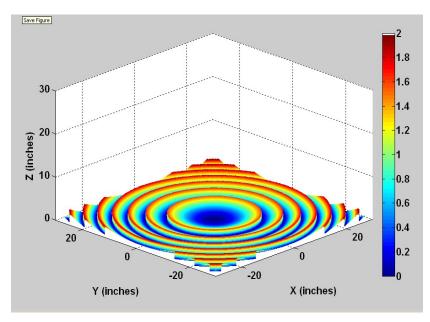
Design, with dimensions, showing both sides – the feed and radiator



Measured VSWR - better than 2:1 from 700 MHZ to 2000 MHz

Synthesized Antenna for "Top-Hat" Radiation Pattern for Zone Plate Antenna ⁴





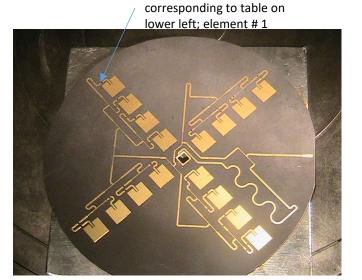
Model of 5 foot diameter "Zone Plate Antenna." The concentric rings are $\frac{1}{2}$ wavelength steps at \approx 12 GHz and the aperture forms a thin replacement for a parabolic reflector

Autocorrelation of white noise at the output of the antenna is a sinc function. Thus for a band-limited system of 400 MHz, for example, the correlation time is approx. 2.5 ns. Since the ZPA induces a delay of 0.27 ns per ring by design, partial correlation of white noise may be present, resulting in some destructive interference of the noise signal

Synthesized element values using Woodward-Lawson method ⁵ corresponding to the pattern at right

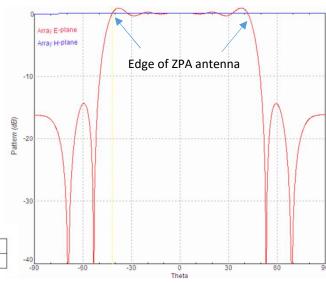
Element #
Amplitude
Phase (degrees)

1	2	3	4	5	6	7	8	9
0.026	0.086	0.156	0.219	0.756	0.219	0.156	0.086	0.026
180	0	180	0	0	0	180	0	180



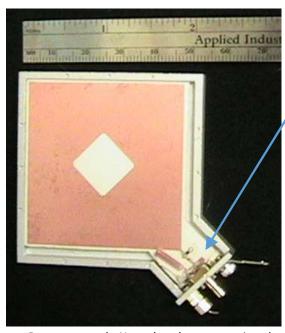
Typical attenuator location

12 cm Uniform Amplitude Taper Array Feed for 1.5 m diameter
Zone Plate Antenna

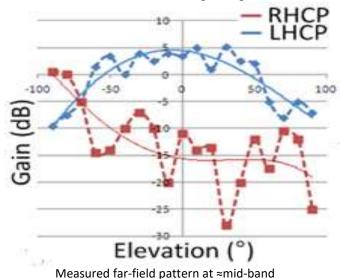


Modeled pattern at 11.7 GHz to uniformly illuminate 1.5 m ZPA

Voltage Tunable Low-Signature L-Band Antenna



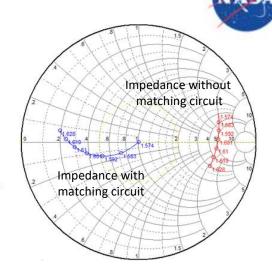
Resonant patch. Note that the antenna is only about ¼ wavelength long

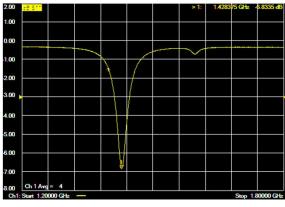


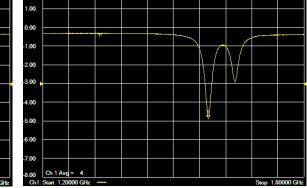
External Bias Tee connector Zo SMV1430 JB Z_L

tuner "patch"

Tuning/Matching Circuit. SMV1430 is a varactor







Measured return loss with 0 Volts Bias

Measured return loss with 8 Volts Bias

The antenna's center frequency tunes between ≈ 1.4 and ≈ 1.6 GHz and covers GPS L1 and the high end of the Iridium band.

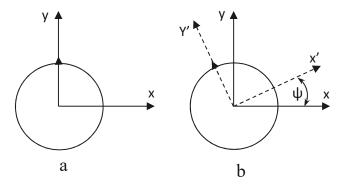
VHF Hybrid Spiral/Dipole Orientation Determining Antenna 7



A normalized RHCP wave propagating along the z axis.

$$E = (x - jy) e^{-j\beta z} e^{-j\omega t}$$

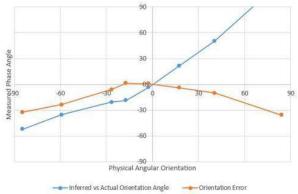
It is a property of a circularly polarized antenna that a physical rotation of Ψ degrees results in a far-field phase shift of Ψ degrees



When the antenna is rotated by angle ψ , the orthogonal field components can be determined by projecting the rotated axes onto the parent coordinate system at z=0. The resulting field is

$$\begin{aligned} \boldsymbol{E_{rot}} &= \left[\mathbf{x} \, \cos(\psi) - \mathbf{y} \, \sin(\psi) - \mathbf{j} (\mathbf{x} \, \sin(\psi) + \mathbf{y} \, \cos(\psi)) \right] \, \mathrm{e}^{-\mathrm{j}\beta z} \, \mathrm{e}^{-\mathrm{j}\omega t} \\ &= \left(\mathbf{x} \, \mathrm{e}^{-\mathrm{j}\psi} - \mathrm{j} \mathbf{y} \, \mathrm{e}^{-\mathrm{j}\psi} \right) \, \mathrm{e}^{-\mathrm{j}\beta z} \, \mathrm{e}^{-\mathrm{j}\omega t} \\ &= \left(\mathbf{x} - \mathrm{j} \mathbf{y} \right) \, \mathrm{e}^{-\mathrm{j}(\beta z + \psi)} \, \mathrm{e}^{-\mathrm{j}\omega t} \end{aligned}$$

thereby preserving the RHCP wave and illustrating an additional phase (delay) of $\boldsymbol{\psi}$ radians.





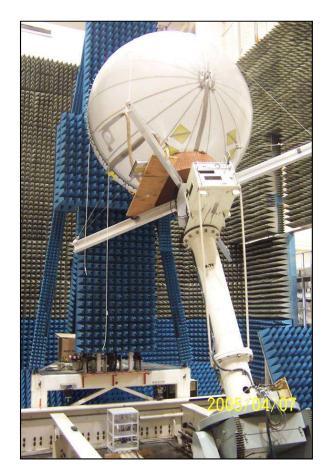
Long-Lived In-situ Solar System Explorer ⁶



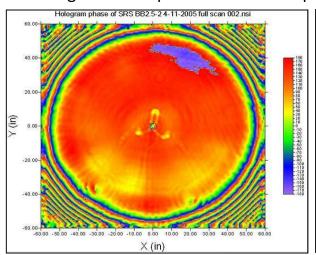
Logarithmic Spiral Low Axial Ratio Design. 24 cm spiral on high contrast substrate represents a factor of 11.4 reduction in physical size. The photograph shows the proof-of-concept integrated spiral and dipole (tuned to 640 MHz) at about a 90 degree rotation angle. Rotating the dipole causes essentially no phase shift variation. The standard deviation of the dipole phase shift as the dipole was rotated was only 0.9 degrees.

Inflatable Radome Antenna System 8

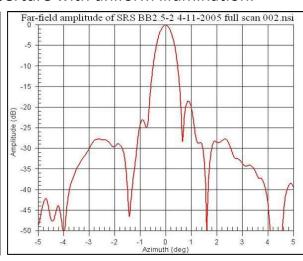
The 2.5 m terrestrial radome antenna was manufactured by GATR (Huntsville, AL) and initially exhibited a 6 dB gain anomaly. GRC performed pattern measurements, surface scans using a laser radar system, and materials measurements and diagnosed several causes of the anomaly. Characterization was at Ku-band. Ultimately, measured directivity corresponded to 75 % of the theoretical gain from a perfect 2.5 meter aperture with uniform illumination.



BB2.5 Radome Antenna on Pedestal Mount in the NASA GRC Near Field Range



BB2.5 Radome Antenna Phase Hologram



Measured far-field azimuth pattern

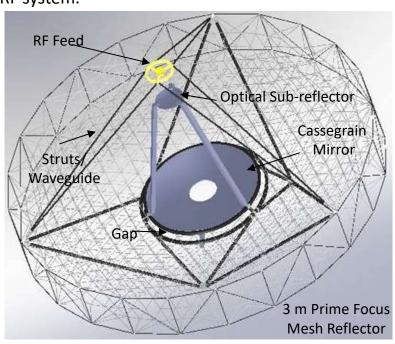


To date, GATR antennas have been deployed in six of the seven continents for humanitarian and disaster relief purposes. Here, The antenna provides communications in the search for a missing girl in San Diego, CA

Integrated Radio and Optical Communications "Teletenna 9"

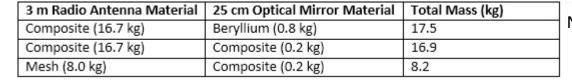


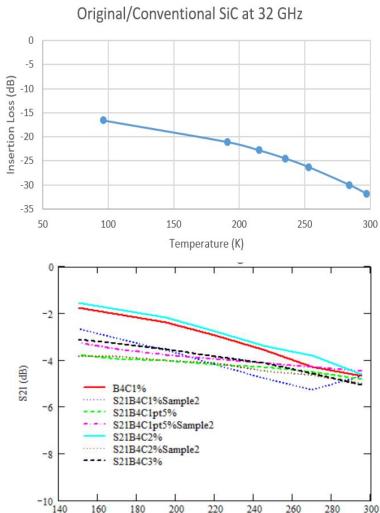
The goal of the iROC project is to integrate a 1550 nm optical terminal with a ≈3 m Ka-band antenna to form a resilient hybrid communications system for deep-space applications with the same mass as a conventional RF system.



iROC Teletenna system:

- 3 m Ka-Band mesh reflector,
- A nominal 25 cm 1550nm optical aperture and associated vibration isolation platform.
- 0.3 μradian star tracker accuracy (beacon-less pointing)
- 4 μradian optical pointing requirement.
- Instantaneous data rates ≈350 MBPS from Mars perigee





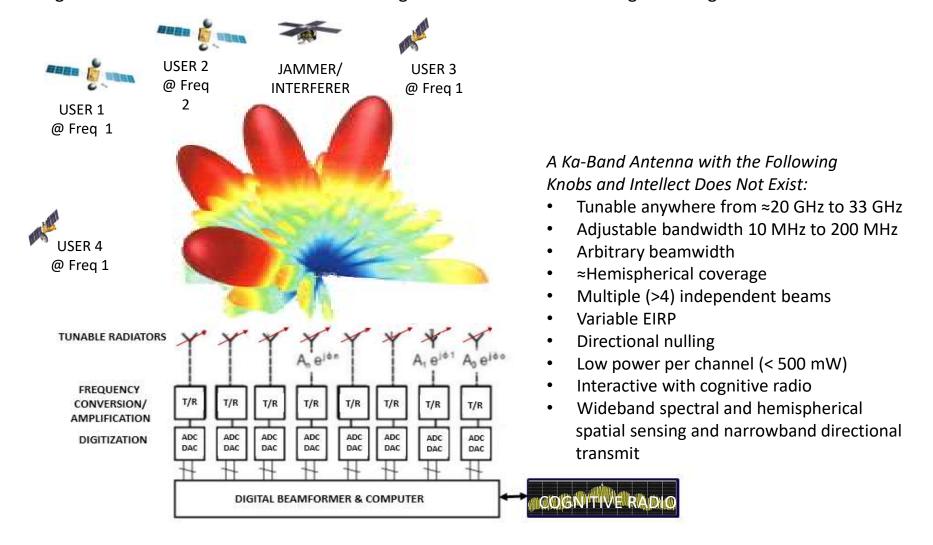
New type of SiC developed that retains all structural advantages but becomes translucent at Ka-band to enable novel hybrid teletenna systems, etc.

Temperature (K)

Cognitive Antennas



According to the FCC, a cognitive radio "can change its transmitter parameters based on interaction with the environment in which it operates." Hence we define a cognitive antenna as an environmentally perceptive antenna that can dynamically allocate bandwidth and/or adjust beam direction and directivity (beamwidth), EIRP, provide beam nulling, etc. to optimize spectral, spatial and temporal resources to complement cognitive radio technology. Intelligence is shared between the beam-forming controller and the radio cognitive engine.





References

- 1. "Advances in Scanning Reflectarray Antennas Based on Thin Ferroelectric Film Phase Shifters," R. Romanofsky, Proc. IEEE, Special Issue on Technical Advances in Deep Space Communications and Tracking, Vol. 95, No. 10, Oct. 2007, pp. 1968-1975.
- 2. "How to Ensure Reliable Connectivity for Aerial Vehicles Over Cellular Networks", H.C. Nguyen, et al., IEEE Wireless Communications, Applications, Control and Modeling, Vol. 6, March, 2018, pp. 12304-12316.
- 3. "Broadband Directive Antenna for Cellular Control of Unmanned Aerial Vehicles", R. Romanofsky, To Be Published.
- 4. "Top-Hat Array for Zone Plate Antenna Feed," R. Romanofsky, Unpublished
- 5. "The Theoretical Precision with Which an Arbitrary Radiation Pattern may be Obtained from a Source of Finite Size," P. M. Woodward and J. D. Lawson, IEE-Part III: Radio and Communication Engineering, vol. 95, pp. 363–370, September 1948.
- 6. "Long-life In-situ Solar System Explorer (LLISSE) Probe Concept And Enabling High Temperature Electronics," T. Kremic et al., Lunar and Planetary Science XLVIII, 2017, pp. 2986.
- 7. "Miniaturized Antenna System for Orientation Determination," R. Romanofsky, Subject of Invention Disclosure (NTR 1550775197), NASA Glenn Research Center, 2019.
- 8. "Technology Benefiting Disaster Relief Has Roots in the SBIR Program and Technology Transfer Efforts," L. Stauber, Technology Transfer and Partnership Office, NASA's Glenn Research Center, 2014
- 9. "Near Earth and Deep Space Communications System," R. Romanofsky, Patent Pending, LEW 19485-1, 2017.